NOTICE OF PUBLIC MEETING

Governmental Body: Van Meter Planning and Zoning Commission

Date of Meeting: Monday October 11th, 2021

Time/Location of Meeting: 5:30 PM – 910 Main Street

Agenda:

- 1. Call to Order/Roll Call
- 2. Approval of Agenda
- 3. Approval of Minutes 9-13-2021
- 4. Discussion and Action Regarding Hudson Heights Plat 2
 - a. Plat of Survey
 - b. Annexation and Rezoning Request
 - c. Preliminary Plat of Survey
- 5. Adjournment

Posted this 8th day of October 2021

Meeting Minutes

Governmental Body: Van Meter Planning and Zoning Commission

Date of Meeting: Monday, September 13th, 2021 Time/Location of Meeting: 5:30 PM – 310 Mill Street

Agenda:

1. Call to Order/Roll Call

Akers called the meeting to order at 5:31 PM Roll was called: Harrison, Hulse (via phone), Akers, DeVore, Feldman present. Staff present included City Administrator Kyle Michel

2. Approval of Agenda

Feldman moved, supported by Harrison, to approve the agenda as published. Motion carried unanimously.

- 3. Approval of Minutes 8-2-2021 Meeting Minutes Hulse moved, supported by Feldman, to approve the minutes. Motion carried unanimously.
- 4. Discussion and Action: Grand Ridge Estates Townhomes Preliminary Plat and Site Plan Paul Clausen, CEC, was present to provide an overview of the preliminary plat and site plan submittal. City Administrator Michel indicated that City Engineer Veenstra's comments were included in the packet and responses from CEC appeared to satisfy all outstanding comments. Discussion ensued regarding unit ownership, covenants, and sidewalk/trail systems. Harrison moved, supported by DeVore, to recommend approval to Council as submitted. Motion carried unanimously.
- 5. Discussion and Action: 36093 Tabor Road Plat of Survey
 City Administrator Michel provided an overview of the plat of survey submitted on behalf of
 Wayne and Marcia Lacox. Michel provided an overview of City Engineer Veenstra's comments.
 Discussion ensued regarding compliance with the future land use map of the City and future
 development of the properties included in the plat of survey.
 Akers move, supported by Harrison, to recommend approval of the Plat of Survey to the City
 Council subject to the following conditions: Future development of the parcel is subject to the
 City's site plan ordinance and/or subdivision ordinance whether the property is developed as a
 single parcel or further divided, the City reserves the right to require compliance with the
 subdivision ordinance as a part of future site plan or subdivision submittal, and that future
- 6. Adjournment

Motion by Feldman, supported by Devore, to adjourn the meeting. Motion carried unanimously. The meeting was adjourned at 6:05 pm.

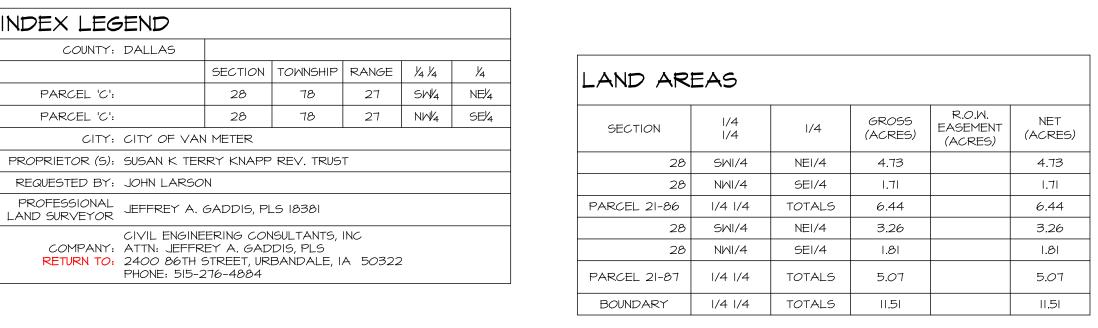
development shall occur in conformance with the future land use map or zoning map of the City

as applicable at the time of development. Motion carried unanimously.

PARCEL 21-86 \$ 21-87 OF PARCEL 'C'

SMI/4 NEI/4 & NMI/4 SEI/4 SEC. 28-78-27

VAN METER, IOMA



| | DESOTO ROAD - 352nd PLACE | |
|-----------------|--|------|
| | THIS SITE ARLINGTON AVENUE ARLINGTON AVENUE | |
| Old Portland Rd | LAKEVIEW DISTRICT OF THE PROPERTY OF THE PROPE | |
| Old Por | F90 - 360th STREET | est: |

SEGMENT #14 : LINE

NORTH: 556345.2328'

COURSE: S29°55'47"E

NORTH: 556230.2906'

SEGMENT #18 : CURVE

SEGMENT #19 : LINE

COURSE: N60°09'02"E LENGTH: 184.70'

COURSE: S43°41'04"E LENGTH: 227.03'

COURSE: S65°34'06"W LENGTH: 191.80'

LENGTH: 69.83' RADIUS: 266.42'

DELTA: 015°01'04" TANGENT: 35.12'

CHORD: 69.63' COURSE: SO7°14'47"E

NORTH: 555986.7828' EAST: 1514041.5626'

COURSE IN: S75°14'41"W COURSE OUT: S89°44'15"E

RP NORTH: 555918.9281' FAST: 1513783.9285'

END NORTH: 555917.7090' EAST: 1514050.3455'

NORTH: 556066.II28' EAST: I5I42I6.I879'

EAST: 1513993.2074

EAST: 1514059.38151

LENGTH: 132.631

| SHEET | LIST TABLE |
|-----------------|----------------|
| SHEET NUMBER | SHEET TITLE |
| I | COVER |
| 2 | DIMENSION PLAN |

AREA: 501415.28 SQ. FT.

0.0102 COURSE:

0.00503 EAST:

PROPERTY OWNERS:

HUDSON HEIGHTS LLC P.O.BOX 267 JOHNSTON IA 50131 CONTACT: JOHN LARSON

APPLICANT: HUDSON HEIGHTS LLC P.O.BOX 267 JOHNSTON IA 50131 CONTACT: JOHN LARSON

PROFESSIONAL LAND SURVEYOR: CIVIL ENGINEERING CONSULTANTS ATTN: JEFFREY A. GADDIS, PLS #18381 2400 86TH STREET, SUITE #12

URBANDALE, IA 50322

PHONE: 515-276-4884 EXT 221

EMAIL: GADDIS@CECLAC.COM

PARCEL ID: 1528251006 1528300009

PROPERTY ADDRESS: VAN BUREN DRIVE, ARLINGTON AVENUE & PARK STREET VAN METER, IA

Consultants, 1
Des Moines, Iowa

Civil Engineering

PROJECT MANAGER:

CIVIL ENGINEERING CONSULTANTS ATTN: PAUL CLAUSEN 2400 86TH STREET, SUITE #12 URBANDALE, IA 50322 515-276-4884 EMAIL: CLAUSEN@CECLAC.COM

ORIGINAL PROPERTY DESCRIPTION

WARRANTY DEED BOOK 2018, PAGE 3770 PARCEL 'C' OF THE SURVEY OF THE SEI/4 OF THE SEX, NEI/4 OF THE SWX, SEI/4 OF THE NWX, SWI/4 OF THE NEX, AND THE NWI/4 OF THE SEI/4 OF SECTION 28, TOWNSHIP 78 NORTH, RANGE 27 WEST OF THE 5TH P.M., DALLAS COUNTY, IOWA AS SHOWN IN BOOK 2001 PAGE 8585, IN THE OFFICE OF THE RECORDER OF DALLAS COUNTY,

IOMA EXCEPT VALLEY VIEW ACRES, AN OFFICIAL PLAT IN VAN METER, DALLAS COUNTY, IOMA.

LEGAL DESCRIPTION

A PARCEL OF LAND IN PARCEL 'C', AN OFFICIAL PARCEL RECORDED IN BOOK 2001, PAGE 8585 AT THE DALLAS COUNTY RECORDER'S AND PART OF THE SWI/4 NEI/4 AND NWI/4 SEI/4 OF SECTION 28, TOWNSHIP 78 NORTH, RANGE 27 WEST OF THE 5TH/ P.M., CITY OF VAN METER, DALLAS COUNTY, IOWA THAT IS MORE PARTICULARLY DESCRIBED AS FOLLOWS:

BEGINNING AT THE NW CORNER OF LOT I, VALLEY VIEW ACRES PLAT I, AN OFFICIAL PLAT RECORDED IN BOOK 2008, PAGE 148 AT THE DALLAS COUNTY RECORDER'S OFFICE; THENCE S29°47'51"E, 146.64 FEET ALONG THE WEST LINE OF SAID VALLEY VIEW ACRES PLAT I TO THE SW CORNER OF SAID LOT I, SAID SW CORNER ALSO BEING ON THE NORTH RIGHT-OF-WAY LINE OF VAN BUREN STREET AS IS IT PRESENTLY ESTABLISHED; THENCE 530°08'37"E, 195.09 FEET ALONG SAID WEST LINE OF SAID VALLEY VIEW ACRES PLAT I TO THE SW CORNER OF LOT 2 OF SAID VALLEY VIEW ACRES PLAT I: THENCE S46°19'15"W. 88.40 FEET TO A POINT: THENCE S40°31'02"W. 58.10 FEET TO A POINT; THENCE S30°06'00"W, 58.10 FEET TO A POINT; THENCE S19°40'57"W, 58.10 FEET TO A POINT; THENCE SO9°15'54"W, 58.10 FEET TO A POINT; THENCE SO0°51'48"W, 65.67 FEET TO A POINT; THENCE 500°14'46"W, 210.00 FEET TO A POINT ON THE NORTH LINE OF PARKVIEW ESTATES PLAT I, AN OFFICIAL PLAT RECORDED IN BOOK 187, PAGE 904 AT THE DALLAS COUNTY RECORDER'S OFFICE; THENCE N89°45'14"W, 360.00 FEET ALONG SAID NORTH LINE OF PARKVIEW ESTATES PLAT I TO A POINT; THENCE NOO°14'46"E, 300.00 FEET TO A POINT; THENCE NIO°13'37"E, 129.88 FEET TO A POINT; THENCE NI8°48'02"E, 89.44 FEET TO A POINT; THENCE N26°20'31"E, 89.44 FEET TO A POINT; THENCE N33°53'00"E, 89.44 FEET TO A POINT; THENCE N41°25'29"E, 89.44 FEET TO A POINT; THENCE N48°57'59"E, 89.44 FEET TO A POINT; THENCE N61°54'13"E, 38.49 FEET TO A POINT ON THE NORTH LINE OF SAID PARCEL 'C'; THENCE N60°32'OI"E, 54.52 FEET ALONG SAID NORTH LINE TO THE POINT OF BEGINNING AND CONTAINING 6.44 ACRES MORE OR LESS

LEGAL DESCRIPTION

PARCEL 21-87

A PARCEL OF LAND IN PARCEL 'C', AN OFFICIAL PARCEL RECORDED IN BOOK 2001, PAGE 8585 AT THE DALLAS COUNTY RECORDER'S AND PART OF THE SWI/4 NEI/4 AND NWI/4 SEI/4 OF SECTION 28, TOWNSHIP 78 NORTH, RANGE 27 WEST OF THE 5TH/ P.M., CITY OF VAN METER, DALLAS COUNTY, IOWA THAT IS MORE PARTICULARLY DESCRIBED AS FOLLOWS:

BEGINNING AT THE SE CORNER OF VAN BUREN HEIGHTS PLAT 4, AN OFFICIAL PLAT RECORDED IN BOOK 4. PAGE 375 AT THE DALLAS COUNTY RECORDER'S OFFICE, SAID SE CORNER ALSO BEING ON THE NORTH LINE OF WEIGEL ADDITION PLAT NO. 2, AN OFFICIAL PLAT RECORDED IN BOOK 5, PAGE 489 AT THE DALLAS COUNTY RECORDER'S OFFICE; THENCE N89°43'02"W, 235.05 FEET ALONG SAID NORTH LINE TO THE NW CORNER OF LOT 5 OF SAID WEIGEL ADDITION PLAT NO. 2; THENCE N89°45'14"W , 141.81 FEET ALONG A LINE THAT COINCIDES WITH SAID NORTH LINE OF WEIGEL ADDITION PLAT NO. 2 AND THE NORTH LINE OF PARKVIEW ESTATES PLAT I, AN OFFICIAL PLAT RECORDED IN BOOK 187, PAGE 904 AT THE DALLAS COUNTY RECORDER'S OFFICE, TO A POINT; THENCE NOO°14'46"E, 210.00 FEET TO A POINT; THENCE NOO°51'48"E, 65.67 FEET TO A POINT; THENCE NO9°15'54"E, 58.10 FEET TO A POINT; THENCE NI9°40'57"E, 58.10 FEET TO A POINT; THENCE N30°06'00"E, 58.10 FEET TO A POINT; THENCE N40°31'02"E, 58.10 FEET TO A POINT; THENCE N46°19"15"E, 88.40 TO THE SW CORNER OF LOT 2, VALLEY VIEW ACRES PLAT I, AN OFFICIAL PLAT RECORDED IN BOOK 2008, PAGE 148 AT THE DALLAS COUNTY RECORDER'S OFFICE; THENCE N60°09'02"E, 184.70 FEET ALONG THE SOUTH LINE OF SAID LOT 2 TO THE SE CORNER OF SAID LOT 2, SAID SE CORNER ALSO BEING ON THE WEST LINE OF VAN BUREN HEIGHTS PLAT 2, AN OFFICIAL PLAT RECORDED IN BOOK 4. PAGE 15 AT THE DALLAS COUNTY RECORDER'S OFFICE AND THE EAST LINE OF SAID PARCEL 'C'; THENCE S29°55'47"E, I32.63 FEET ALONG SAID WEST LINE AND SAID EAST LINE OF PARCEL 'C' TO A POINT; THENCE S43°41'04"E, 227.03 FEET ALONG SAID WEST LINE AND SAID EAST LINE OF PARCEL 'C' TO A POINT ON THE NORTH LINE OF SAID VAN BUREN HEIGHTS PLAT 4; THENCE 565°34'06"W, 191.80 FEET ALONG SAID NORTH LINE OF VAN BUREN HEIGHTS PLAT 4 AND SAID EAST LINE OF PARCEL 'C' TO THE NU CORNER OF SAID VAN BUREN HEIGHTS PLAT 4; THENCE SOUTHEASTERLY ALONG A NON-TANGENT CURVE THE TO RIGHT HAVING A RADIUS OF 266.42 FEET AND A CHORD BEARING SOT°14'47"E, AN ARC LENGTH OF 69.83 FEET ALONG THE WEST LINE OF SAID VAN BUREN HEIGHTS PLAT 4 AND SAID EAST LINE OF PARCEL 'C' TO THE SW CORNER OF LOT 8 OF SAID VAN BUREN HEIGHTS PLAT 4, SAID SW CORNER ALSO BEING ON THE NORTH RIGHT-OF-WAY LINE OF ARLINGTON AVENUE AS IT IS PRESENTLY ESTABLISHED; THENCE SOO°34'47"W, 209.38 FEET ALONG SAID WEST LINE OF VAN BUREN HEIGHTS PLAT 4 AND SAID EAST LINE OF PARCEL 'C' TO THE POINT OF BEGINNING AND CONTAINING 5.07 ACRES MORE OR LESS.

CERTIFICATION



HEREBY CERTIFY THAT THIS LAND SURVEYING DOCUMENT WAS PREPARED AND THE RELATED SURVEY WORK WAS PERFORMED BY ME OR UNDER MY DIRECT PERSONAL SUPERVISION AND THAT I AM A DULY ICENSED PROFESSIONAL LAND SURVEYOR UNDER THE LAWS OF THE STATE OF IOWA JEFFREY A. GADDIS, IOWA LICENSE NO. 18381 DATE MY LICENSE RENEWAL DATE IS DECEMBER 31, 2022

BASIS OF BEARINGS:

THE NORTH LINE OF WEIGEL ADDITION PLAT NO. 2 WAS MEASURED AS HAVING A BEARING OF N89°43'02"W. THIS BEARING WAS DETERMINED FROM THE IOWA DEPARTMENT OF TRANSPORTATION REAL-TIME NETWORK CONVERTED TO IOMA STATE PLANE NADI983(2011) SOUTH ZONE GRID NORTH.

THIS PARCEL MAY BE SUBJECT TO EASEMENTS OF RECORD. NO TITLE WORK WAS PROVIDED TO THIS LAND SURVEYOR.

THE UNADJUSTED ERROR OF CLOSURE IS NOT GREATER THAN I:10000 FOR SUBDIVISION BOUNDARIES AND IS NOT GREATER THAN I:5000 FOR INDIVIDUAL LOTS. MONUMENTS TO BE SET WITHIN THIRTY DAYS OF THE PLAT OF SURVEY RECORDING DATE.

PARCEL NOTES:

NO DEVELOPMENT SHALL OCCUR ON ANY PARCEL WITHOUT THE FORMAL DEVELOPMENT APPLICATION PROCEDURES AS REQUIRED BY THE APPROPRIATE JURISDICTION.

R-I SINGLE FAMILY RESIDENTIAL DISTRICT FRONT - 35'

SIDE - 8' MINIMUM

FLOOD ZONE

FEMA FIRM FLOOD INSURANCE RATE MAP NUMBER 19049C0340F, REVISED 12-7-2018.

LEGEND

| Δ | SET SECTION CORNER (5/8" I.R. W/BLUE CAP #18381 UNLESS OTHERWISE NOTED) |
|------------------|---|
| H | FOUND RIGHT-OF-WAY RAIL |
| • | FOUND CORNERS |
| | FOUND ½" I.R. WYELLOW CAP #7056 |
| 0 | SET PROPERTY CORNER (5/8" I.R. W/BLUE CAP #18381 UNLESS OTHERWISE NOTED) |
| | PARCEL BOUNDARY LINES |
| | PROPOSED PARCEL LINES |
| | EXISTING PROPERTY LINES |
| | SECTION LINES |
| | EASEMENT LINES |
| | CENTERLINE STREET |
| D. | DEEDED BEARING & DISTANCE |
| P. | PREVIOUSLY RECORDED BEARING & DISTANCE |
| M. | MEASURED BEARING & DISTANCE |
| I.R. | IRON ROD |
| I.P. | IRON PIPE |
| BK. XXX, PG. XXX | COUNTY RECORDER'S INDEXING BOOK & PAGE |
| R.O.W. | RIGHT-OF-WAY |
| P.O.B | POINT OF BEGINNING |
| P.U.E. | PUBLIC UTILITY EASEMENT |

+ - EXISTING PIPE FENCE

FOUND SECTION CORNERS

BOUNDARY CLOSURE REPORT

NORTH: 555708.3347' EAST: 1514048.2360' SEGMENT #1 : LINE COURSE: N89°43'02"W LENGTH: 235.05' NORTH: 555709.4947' EAST: 1513813.1888' COURSE: N89°45'14"W LENGTH: 501.81' NORTH: 5557II.6502' EAST: I5I33II.3834' SEGMENT #3 : LINE NORTH: 556011.6475' EAST: 1513312.6721'

SEGMENT #4 : LINE COURSE: NIO°13'37"E LENGTH: 129.88' NORTH: 556|39.4640' EAST: |5|3335.7320'

SEGMENT #5 : LINE COURSE: NI8°48'02"E LENGTH: 89.44' NORTH: 556224.1320' EAST: 1513364.5562' SEGMENT#6 : LINE COURSE: N26°20'31"E LENGTH: 89.44' NORTH: 556304.2847' EAST: 1513404.2432'

PARCEL 21-86

CLOSURE REPORT NORTH: 556549,2586' EAST: 1513662,1750' SEGMENT #1 : LINE COURSE: S29°47'51"E LENGTH: 146.64' NORTH: 556422.0063' EAST: I5I3735.0457' COURSE: 530°08'37"E LENGTH: 195.09' NORTH: 556253.2985' EAST: 1513833.01391 SEGMENT #3 : LINE COURSE: S46°19'15"W LENGTH: 88.40' NORTH: 556192.2477' EAST: 1513769.0814' SEGMENT #4 : LINE COURSE: S40°31'02"W LENGTH: 58.10'

PARCEL 21-87 CLOSURE REPORT NORTH: 555708.3347' EAST: 1514048.2360' SEGMENT #1 : LINE COURSE: N89°43'02"W LENGTH: 235.05 NORTH: 555709.4947' EAST: 1513813.1888' SEGMENT #2 : LINE COURSE: N89°45'|4"W LENGTH: |4|.8|' NORTH: 555710.1039' EAST: 1513671.3801' SEGMENT #3 : LINE COURSE: NOO°14'46"E LENGTH: 210.00' NORTH: 555920.1019' EAST: 1513672.2822' SEGMENT #4 : LINE COURSE: NOO°51'48"E LENGTH: 65.67' NORTH: 555985.7645' EAST: 1513673.2716'

NORTH: 556148.0795' EAST: 1513731.3352'

SEGMENT #7 : LINE COURSE: N33°53'00"E LENGTH: 89.44' NORTH: 556378.5355' EAST: 1513454.1063'

VICINITY SKETCH

SEGMENT #8 : LINE COURSE: N41°25'29"E LENGTH: 89.44' NORTH: 556445.5999' EAST: 1513513.2830' COURSE: N48°57'59"F I FNGTH: 89 44' NORTH: 556504.3174' EAST: 1513580.7498' SEGMENT #10 : LINE NORTH: 556522.4445' EAST: 1513614.7040'

COURSE: N61°54'13"E LENGTH: 38.49' SEGMENT #II : LINE COURSE: N60°32'01"E LENGTH: 54.52' NORTH: 556549.2636' EAST: 1513662.1715' SEGMENT #12 : LINE COURSE: S29°47'51"E LENGTH: 146.64' NORTH: 556422.0113' EAST: 1513735.0422' COURSE: S30°08'37"E LENGTH: 195.09'

NORTH: 556253.3034' EAST: I5I3833.0I04'

SEGMENT #5 : LINE COURSE: S30°06'00"W LENGTH: 58.10' COURSE: NOO°14'46"E LENGTH: 300.00' NORTH: 556097.8142' EAST: 1513702.1974' NORTH: 556011.6497' EAST: 1513312.6751' COURSE: SI9°40'57"W LENGTH: 58.10' COURSE: NIO°13'37"E NORTH: 556139.4662' NORTH: 556043.1088' EAST: 1513682.6289' COURSE: SO9°15'54"W LENGTH: 58.10' COURSE: NI8°48'02"E NORTH: 555985.7667' EAST: 1513673.2747' NORTH: 556224.1342' SEGMENT #8 : LINE SEGMENT #14 : LINE COURSE: SOO°51'48"W LENGTH: 65.67' COURSE: N26°20'31"E NORTH: 555920.1042' EAST: 1513672.2852' NORTH: 556304.2869' COURSE: 500°14'46"W LENGTH: 210.00' COURSE: N33°53'00"E

NORTH: 555710.1061' EAST: 1513671.3832' COURSE: N89°45'14"W LENGTH: 360.00' COURSE: N41°25'29"E LENGTH: 89.44' NORTH: 555711.6525' EAST: 1513311.3865' NORTH: 556445.6021' EAST: 1513513.2861' SEGMENT #5 : LINE SEGMENT #II : LINE COURSE: NO9°15'54"E LENGTH: 58.10' COURSE: S29°55'47"E LENGTH: 132.63' NORTH: 556043.1065' EAST: 1513682.6258' COURSE: 543°41'04"E LENGTH: 227.03' COURSE: NI9°40'57"E LENGTH: 58.10' NORTH: 556097.8119' EAST: 1513702.1943' NORTH: 556066.1056' SEGMENT #7 : LINE COURSE: N30°06'00"E LENGTH: 58.10' COURSE: S65°34'06"W LENGTH: 191.80' NORTH: 556148.0772' EAST: 1513731.3321' NORTH: 555986.7756' EAST: 1514041.5630'

COURSE: N40°31'02"E LENGTH: 58.10' NORTH: 556192.2455' EAST: 1513769.0783' COURSE: N46°19'15"E LENGTH: 88.40' NORTH: 556253.2962' EAST: 1513833.0108' COURSE: N60°09'02"E LENGTH: 184.70' COURSE: SOO°34'47"W LENGTH: 209.38'

NORTH: 556345.2256' EAST: 1513993.2078'

COURSE: SOO°34'47"W LENGTH: 209.38' NORTH: 555708.3397' EAST: 1514048.2270' SEGMENT #17 : LINE COURSE: N48°57'59"E LENGTH: 89.44' NORTH: 556504.3197' EAST: 1513580.7529' LENGTH: 129.881 EAST: 1513335,73501 LENGTH: 89.44' EAST: 1513364.55931 LENGTH: 89.44' ERROR CLOSURE: NO3°12'03"W ERROR NORTH: -0.00040

ERROR CLOSURE:

PRECISION 1: 300377.45

N60°34'47"W

-0.00892

ERROR NORTH:

EAST: 1513404.2463' LENGTH: 89.44' NORTH: 556378.5377' EAST: 1513454.1094' NORTH: 556230.2834' EAST: 1514059.3819'

ERROR NORTH: EAST: 1514216.1883'

SEGMENT #14 : CURVE LENGTH: 69.83' RADIUS: 266.42' DELTA: 015°01'04" TANGENT: 35.12' CHORD: 69.63' COURSE: SO7°14'47"E COURSE IN: S75°14'41"W COURSE OUT: S89°44'15"E RP NORTH: 555918.9209' FAST: 1513783.9289' END NORTH: 555917.7018' EAST: 1514050.3459'

NORTH: 555708.3325' EAST: 1514048.2274'

COURSE: N61°54'13"E LENGTH: 38.49' NORTH: 556522.4468' EAST: 1513614.7071' COURSE: N60°32'01"E LENGTH: 54.52' NORTH: 556549.2659' EAST: 1513662.1746' PERIMETER: 2268.29' AREA: 280611.05 SQ. FT. 0.0072 COURSE:

0.00720 EAST: PRECISION 1: 315040.28

PERIMETER: 1988.69' AREA: 220804.24 SQ. FT. ERROR CLOSURE: 0.0088 COURSE: -0.00217 EAST: -0.00852

PRECISION 1: 225965.91

S75°40'|7"W



September 8, 2021

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SHEET

*O*F 2

q:\E-FILES\E-8000\E8686_C3D Drawings\Plat\POS\E8686 POS DIM.dwg, 9/8/2021 3:17:03 PM, lhook, 1:



September 27, 2021

ATTN: Kyle Michel City Administrator 310 Miller Street P.O. Box 160 Van Meter, IA 50261

RE: Hudson Heights Plat 2 - Annexation Request

Dear Kyle,

On behalf of Susan K Terry Knapp Revocable Trust, we are submitting this letter of requesting the annexation of a portion of the Dallas County Parcel ID 1528300009 located in Section 28, Township 78N, Range 27W of the 5th P.M., City of Van Meter, Dallas County, Iowa as generally depicted on the attached schematic. The property is located south of Desoto Road and west of Hazel Street.

Please review this information at your earliest convenience. Would you please place us on the earliest Planning and Zoning Commission and City Council Agenda? Do not hesitate to contact us if you have any questions or concerns.

Sincerely,

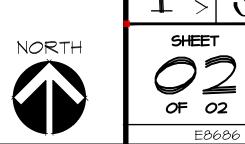
Civil Engineering Consultants, Inc.

Paul Clausen, P.E.

CC: Susan Knapp, Stuart Ruddy, Tom Wittman, Bob Veenstra, and John Larson

E8686





Civil Engineering Consultants, Inc. 2400 86th Street. Unit 12. Des Moines, Iowa 50322 515.276.4884. mail@ceclac.com

CEC



September 27, 2021

ATTN: Kyle Michel City Administrator 310 Miller Street P.O. Box 160 Van Meter, IA 50261

RE: Hudson Heights Plat 2 – Rezoning Request

Dear Kyle,

On behalf of Susan K Terry Knapp Revocable Trust, we are submitting this letter of request for rezoning Parcel 2021-86 and Parcel 2021-87, official parcels located in the City of Van Meter, Dallas County, Iowa. The property is located south of Desoto Road and west of Hazel Street.

The property is currently zoned A – Agricultural. We are proposing to rezone the property to R-2 – Two-Family Residence District. We have created a preliminary plat for this area including: single family lots, street lots; adjacent lot information; utilities and grading for your review.

Please review this information at your earliest convenience. Would you please place us on the earliest Planning and Zoning Commission and City Council Agenda? Do not hesitate to contact us if you have any questions or concerns.

Sincerely,

Civil Engineering Consultants, Inc.

CC: Susan Knapp, Tom Wittman, Bob Veenstra, and John Larson

SHEET

OF 04

E8686

HUDSON HEIGHTS PLAT 2 VAN METER, IONA

VAN METER PUBLIC WORKS ADDRESS: 310 MILL STREET VAN METER, IOWA 50261 PHONE: (515) 996-2644

SANITARY SEWER - CITY OF VAN METER STORM SEWER - CITY OF VAN METER WATER - CITY OF VAN METER

ELECTRIC AND NATURAL GAS UTILITY

MIDAMERICAN ENERGY CORPORATION 666 GRAND AVENUE DES MOINES, IA 50309 CONTACT: MATT REINHARDT PHONE: 515-515-252-6413 EMAIL: MJREINHARDT@MIDAMERICAN.COM

TELEPHONE

CENTURY LINK 4201 KINGMAN BLVD. 2nd FLOOR DES MOINES, IA 50311 CONTACT: CINDY CARTER PHONE: 515-554-3316

BUILDING DEPARTMENT

CITY OF VAN METER ADDRESS: 310 MILL STREET VAN METER, IOWA 50261 PHONE: (515) 996-2644

HEALTH DEPARTMENT

DALLAS COUNTY PUBLIC HEALTH DEPARTMENT ADDRESS: 25747 N AVENUE, ADEL, IA 50003 PHONE: (515) 993-3750

FIRE DEPARTMENT

505 GRANT ST, VAN METER, IA 50261 DIRECTOR DAGGETT: 515-202-4154 STATION PHONE NUMBER -515-993-4567

GENERAL LEGEND

FRANCHISE UTILITIES

WATER VALVE

SAN SANITARY SEWER WITH SIZE

----SAN--- SANITARY SERVICE

----ST---- STORM SERVICE

/X SILT FENCE

(1234)

STORM SEWER WITH SIZE

PROPOSED CONTOUR

RIP RAP

ADDRESS

SET CORNER 5/8" I.R.

M. MEASURED DISTANCE

WORANGE CAP #12265

PREVIOUSLY RECORDED DISTANCE

FOUND CORNER

FIRE HYDRANT ASSEMBLY

DETECTABLE WARNING PANEL

BLOW-OFF HYDRANT

I. CONTRACT FOR STREET LIGHTING SHALL BE EXECUTED WITH FINAL PLAT. CONTRACT FOR ELECTRIC DISTRIBUTION SYSTEM SHALL BE EXECUTED

3. NATURAL GAS, TELEPHONE, CABLE OR OTHER UTILITIES SHALL BE INSTALLED AFTER COMPLETION OF PLAT IMPROVEMENTS.

| Sheet List Table | | | | | |
|------------------|-----------------|--|--|--|--|
| Sheet Number | Sheet Title | | | | |
| 01 | COVER SHEET | | | | |
| 02 | DIMENSION SHEET | | | | |
| 03 | UTILITY SHEET | | | | |
| | | | | | |

| | SUBMITTAL TABLE |
|-------------------|-------------------|
| SUBMITTAL DATE | SUBMITTAL NOTES |
| 2021-09-28 | INITIAL SUBMITTAL |
| | |
| | |
| | |
| | |
| | |
| | |
| · | |

GRADING SHEET

| | PROPOSED | |
|---|------------------------------|--|
| _ | PLAT BOUNDARY | |
| | SECTION LINE | |
| _ | LOT LINE | |
| | CENTERLINE | 0 |
| 1 | EASEMENT LINE | M |
| | FLARED END SECTION | |
| | TYPE SW-501 STORM INTAKE | |
| | TYPE SW-502 STORM INTAKE | ₩ |
| | TYPE SW-503 STORM INTAKE | |
| | TYPE SW-504 STORM INTAKE | |
| | TYPE SW-505 STORM INTAKE | The state of the s |
| | TYPE SM-506 STORM INTAKE | |
| | TYPE SM-511 STORM INTAKE | <u>.</u> |
| | TYPE SM-512 STORM INTAKE | р ∳- × - |
| | TYPE SM-513 STORM INTAKE | , > |
| | TYPE SM-401 STORM MANHOLE | E G |
| | TYPE SW-402 STORM MANHOLE | \bigcirc |
| | TYPE SW-403 STORM MANHOLE | þ |
| | TYPE SW-403 STORM MANHOLE | -CATV UGE |
| | TYPE SW-301 SANITARY MANHOLE | <u> </u> |
| | TYPE SW-302 SANITARY MANHOLE | -UGFO |
| | TYPE SW-304 SANITARY MANHOLE | —UGT— — —они— — |
| | STORM/SANITARY CLEANOUT | —SAN ^{8"} — |
| | | c_12" |

| ——— ○ X □ ———— | LOT LINE SANITARY/STORM MANHOLE WATER VALVE FIRE HYDRANT STORM SEWER SINGLE INTAKE STORM SEWER DOUBLE INTAKE STORM SEWER ROUND INTAKE FLARED END SECTION |
|--|--|
| | DECIDUOUS TREE |
| | CONIFEROUS TREE |
| 0 | SHRUB |
| ø | POWER POLE |
| <i>,</i> / | STREET LIGHT |
| > | GUY ANCHOR |
| E | ELECTRIC TRANSFORMER |
| 6 | GAS METER |
| \bigcirc | TELEPHONE RISER |
| d | SIGN |
| | UNDERGROUND TELEVISION |
| — —UGE— — | UNDERGROUND ELECTRIC |
| — 6 — — | UNDERGROUND GAS |
| — -UGFO | UNDERGROUND FIBER OPTIC |
| — —UGT— — | UNDERGROUND TELEPHONE |
| <u> — они — </u> | OVERHEAD ELECTRIC |
| — — SAN 8" — | SANITARY SEWER WITH SIZE |
| - · · · · · · · · · · · · · · · · · · · | STORM SEWER WITH SIZE |
| <u> — м^в </u> | WATER MAIN WITH SIZE |
| 926 | EXISTING CONTOUR |
| | TREELINE |
| B.S.L. | BUILDING SETBACK LINE |

PUBLIC UTILITY EASEMENT

TREES TO BE REMOVED

MINIMUM OPENING ELEVATION

P.U.E.

M.O.E.

| | LOT LINE |
|---|---------------------------|
| | SANITARY/STORM MANHOLE |
| | MATER VALVE |
| | FIRE HYDRANT |
| | STORM SEWER SINGLE INTAKE |
| | STORM SEWER DOUBLE INTAKE |
| | STORM SEWER ROUND INTAKE |
| | FLARED END SECTION |
| | DECIDUOUS TREE |
| | CONIFEROUS TREE |
| | SHRUB |
| | POWER POLE |
| | STREET LIGHT |
| | GUY ANCHOR |
| | ELECTRIC TRANSFORMER |
| | GAS METER |
| | TELEPHONE RISER |
| | SIGN |
| - | UNDERGROUND TELEVISION |
| - | UNDERGROUND ELECTRIC |
| - | UNDERGROUND GAS |
| - | UNDERGROUND FIBER OPTIC |
| - | UNDERGROUND TELEPHONE |
| _ | OVERHEAD ELECTRIC |
| - | SANITARY SEWER WITH SIZE |
| - | STORM SEWER WITH SIZE |
| _ | WATER MAIN WITH SIZE |
| | EXISTING CONTOUR |
| | TREELINE |
| | |

| EXISTING | | | | | | |
|---------------------------|---------------------------|--|--|--|--|--|
| LOT LINE | | | | | | |
| SANITARY/STORM | 1 MANHOLE | | | | | |
| WATER VALVE | | | | | | |
| FIRE HYDRANT | FIRE HYDRANT | | | | | |
| STORM SEWER SINGLE INTAKE | | | | | | |
| STORM SEWER DO | STORM SEWER DOUBLE INTAKE | | | | | |
| STORM SEWER RO | OUND INTAKE | | | | | |
| FLARED END SECTION | | | | | | |
| DECIDUOUS TREE | | | | | | |
| CONIFEROUS TREE | | | | | | |
| SHRUB | | | | | | |
| POWER POLE | | | | | | |
| STREET LIGHT | | | | | | |

I. PARCEL MAY BE SUBJECT TO EASEMENTS, LICENSES, OR AGREEMENTS OF RECORD. NO TITLE WORK WAS PERFORMED BY SURVEYOR 2. ALLOWABLE ERROR OF CLOSURE FOR BOUNDARY IS 1:10,000 AND ALLOWABLE ERROR OF CLOSURE FOR EACH LOT IS 1:5,000.

4. LOTS 'A', 'B' & 'C' ARE TO BE DEDICATED TO CITY OF VAN METER. 5. SOME LOTS ACCEPT DRAINAGE FROM ADJACENT PROPERTY. BUILDING ON THESE LOTS MUST TAKE INTO ACCOUNT UPSTREAM DRAINAGE

6. ALL UTILITIES INDICATED ON PLAT ARE PUBLIC UNLESS OTHERWISE NOTED. 7. WATER SERVICES TO BE I-INCH PVC AND SHALL BE BORED WHEN FEASIBLE, STOP BOXES TO BE FORD BALL VALVE TYPE CURB STOPS.

PARKLAND WITHIN ORDINANCE 2021-02: 26 LOTS * 2.8 PEOPLE PER LOT * 0.005 AC = 0.364 ACRES OR 15,856 S.F. MINIMUM DEDICATION REQUIRED FOR ANY DEVELOPMENT: 20,000 SF.



VICINITY SKETCH

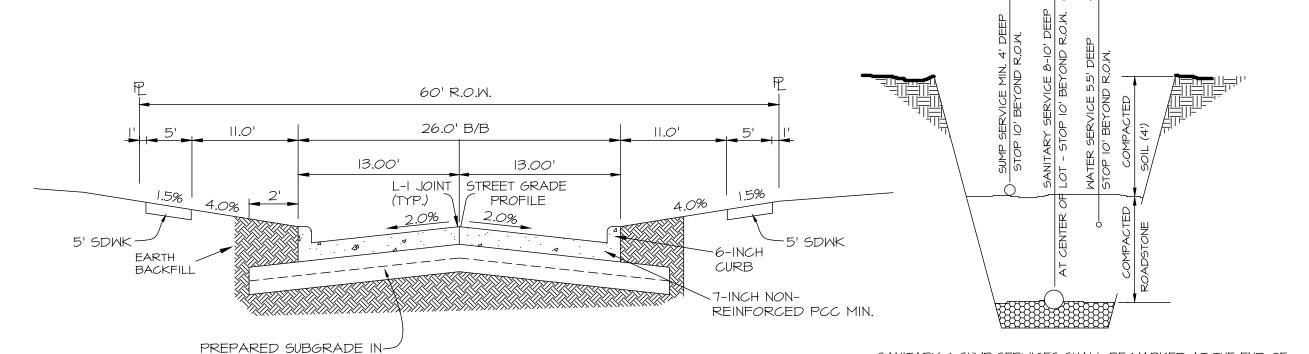


3. MONUMENTS TO BE SET WITHIN ONE YEAR OF FINAL PLAT'S RECORDING DATE.

8. AN HOA SHALL BE ESTABLISHED AND RESPONSIBLE FOR THE OPERATION AND MAINTENANCE OF THE STORMWATER DETENTION BASIN.

PARKLAND DEDICATION:

CALCULATION FOR PARKLAND DEDICATION IS PER CHAPTER 173 - DEDICATION OF



2-6" LIFTS TO 95% MIN. DENSITY (SEE PAVING NOTE 4.)

TYPICAL 26' B/B CROSS SECTION

NO SCALE

SANITARY, GREEN FOR SUMPS AND BLUE FOR WATER. SERVICE LOCATION DETAIL

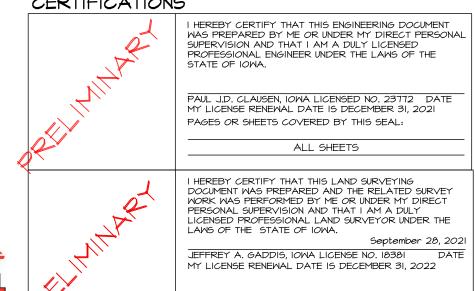
BOX. COLOR MARKING OF SERVICES SHALL BE RED FOR

PIPE WITH A 2X4 TO THE SURFACE & A STEEL FENCE POST.

PLACE ONE 6 FT. STEEL POST BURIED 3 FT. AT WATER CURB

SANITARY & SUMP SERVICES SHALL BE MARKED AT THE END OF

CERTIFICATIONS



PROPERTY OWNER / DEVELOPER / APPLICANT:

PARCEL 2I-86 & PARCEL 2I-87, OFFICIAL PARCELS RECORDED IN BOOK XXXX,

FEMA FIRM FLOOD INSURANCE RATE MAP NUMBER 19049C0340F, REVISED 12-7-2018.

I. IMPROVEMENTS SHALL BE CONSTRUCTED USING 2021 S.U.D.A.S. SPECIFICATIONS

HUDSON HEIGHTS LLC

JOHNSTON IA 50131 CONTACT: JOHN LARSON

PAUL CLAUSEN, PE,

2400 86TH STREET, #12

DES MOINES, IOWA 50322 PH. 515-276-4884 EXT. #217 EMAIL: CLAUSEN@CECLAC.COM

PROJECT MANAGER:

CIVIL ENGINEERING CONSULTANTS

CIVIL ENGINEERING CONSULTANTS, INC.

MUNICIPALITY PLANNER:

EMAIL: KMICHEL@VANMETERIA.GOV

LEGAL DESCRIPTION

TOTAL LAND AREA:

EXISTING ZONING:

PROPOSED ZONING:

R-2 SINGLE FAMILY RESIDENTIAL DISTRICT

- 35'

- 30'

CONSTRUCTION SCHEDULE

GRADING ACTIVITIES - AUGUST, 2021

PUNCH LIST ITEMS - MAY, 2022

UTILITY PLACEMENT - OCTOBER, 2021

APRIL, 2022

- 8' MINIMUM

PH: JEFFERY A. GADDIS, PLS

2400 86TH STREET, SUITE 12

PH. 515-276-4884 EXT. 221 EMAIL: GADDIS@CECLAC.COM

CITY OF VAN METER, IOWA PHONE: (515) 996-2644

URBANDALE, IA 50322

CITY ADMINISTRATOR

KYLE MICHEL

501,415 SQ. FT

A AGRICULTURAL

SETBACKS:

PAVING -

FRONT

SIDE

REAR

FLOOD ZONE

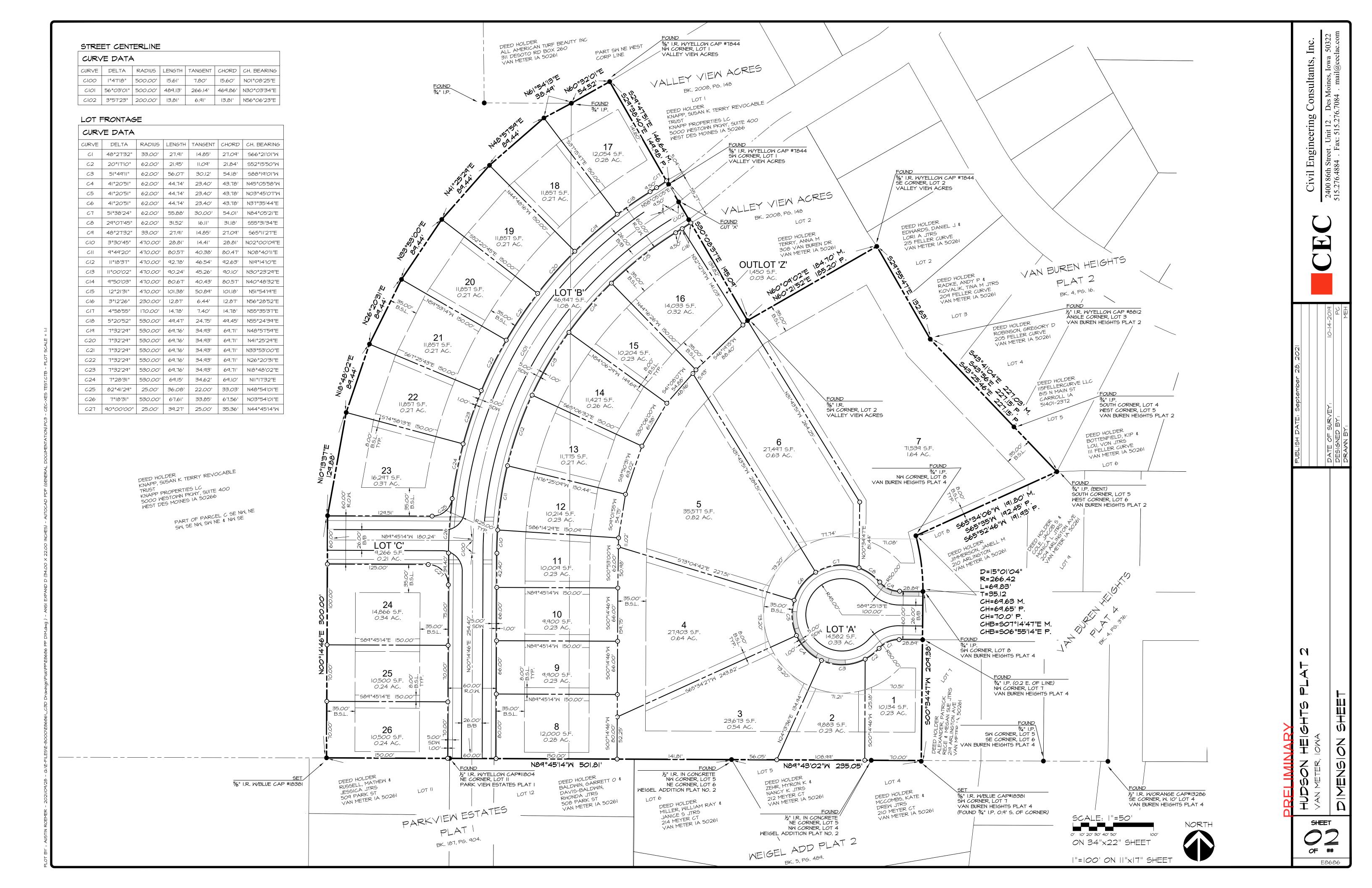
ZONE 'X' & ZONE 'A'

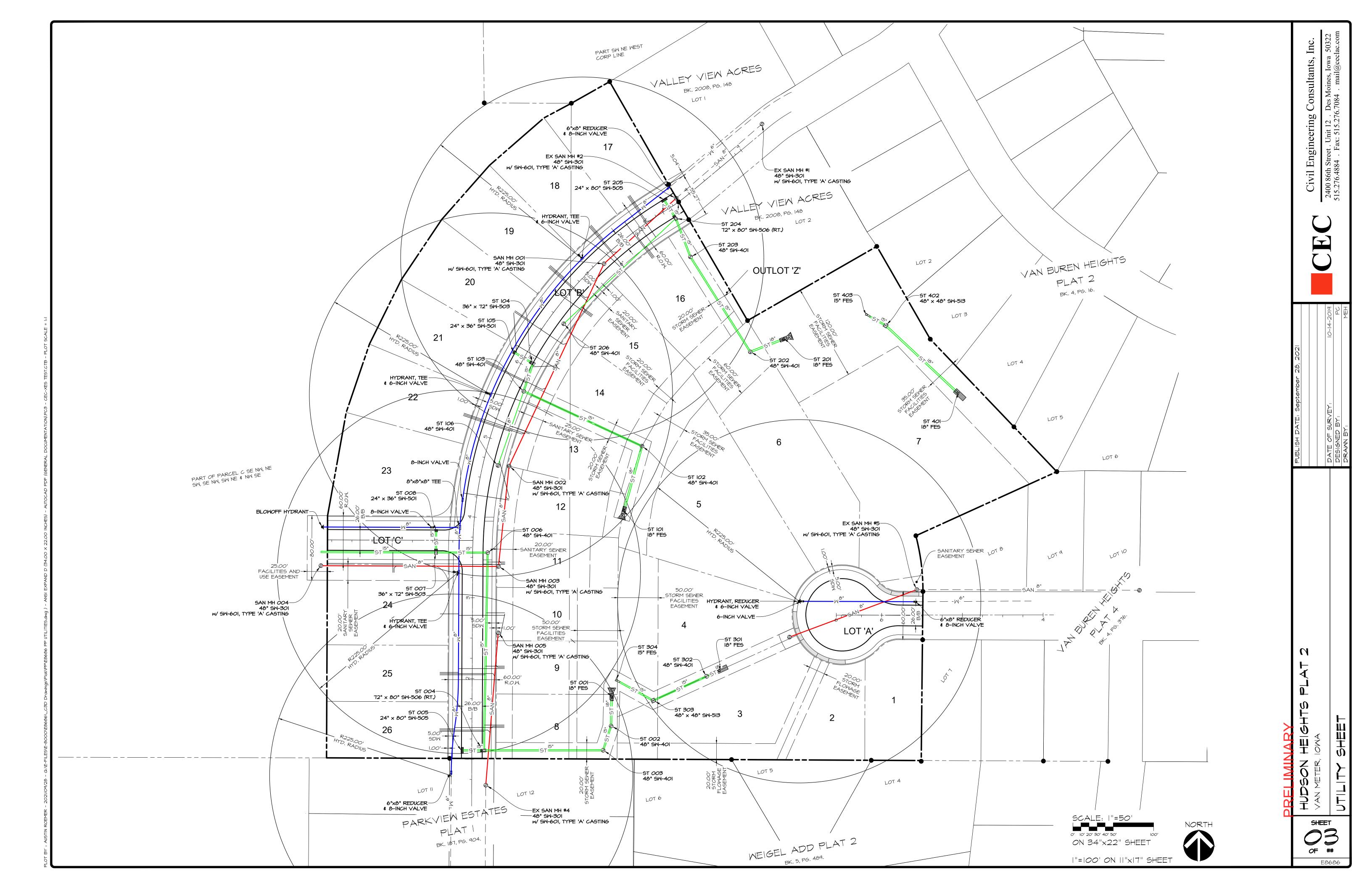
PROFESSIONAL LAND SURVEYOR:

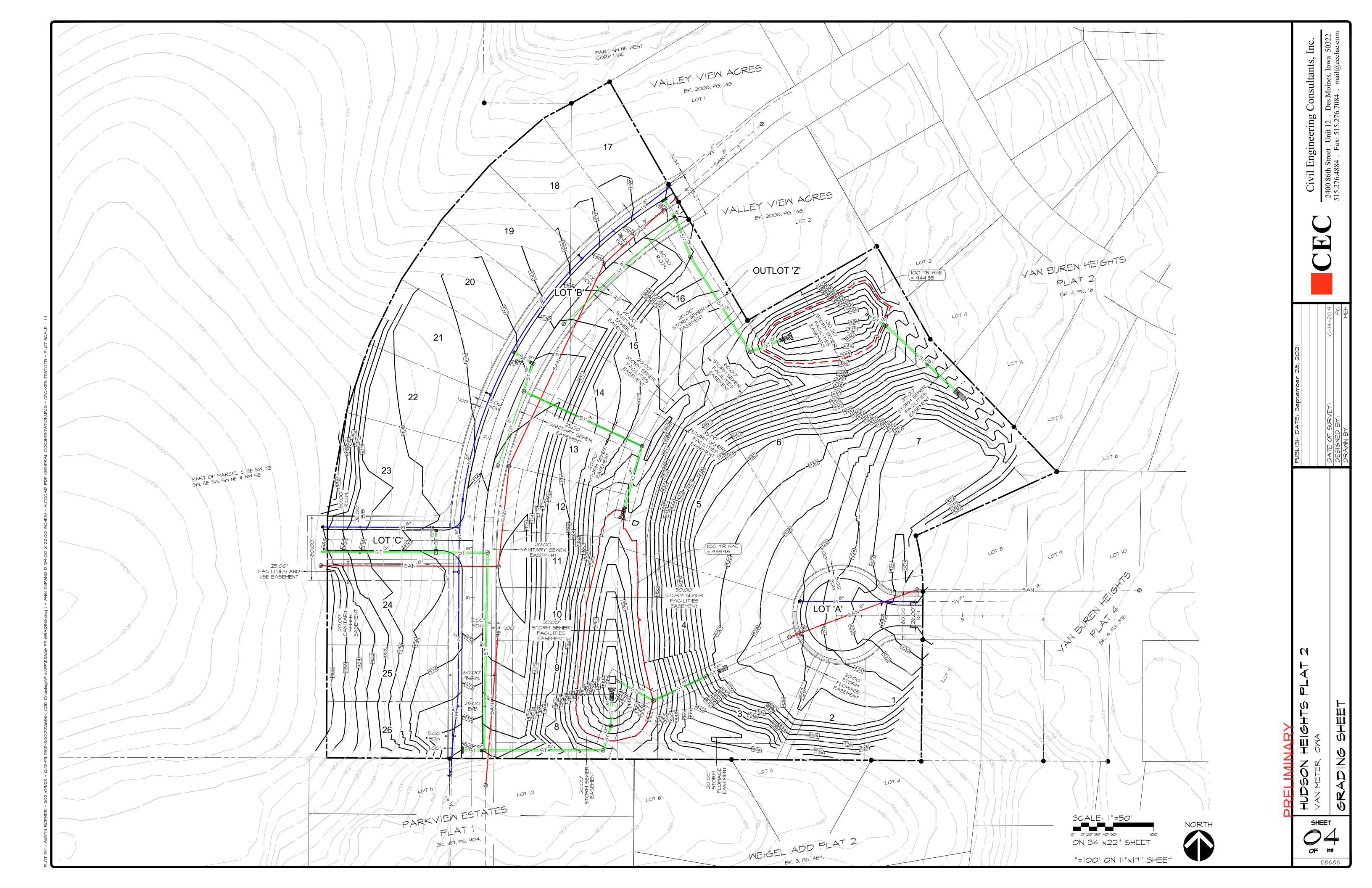
PAGE XXXXX, CITY OF VAN METER, DALLAS COUNTY, IOWA.

SAID PARCELS CONTAIN II.51 ACRES MORE OR LESS.

⊗IOWA 1-800-292-8989







STORMWATER MANAGEMENT REPORT

Project: Hudson Heights Plat 2 Prepared By: Paul Clausen, P.E. Austin Roemer, E.I.T.



Civil Engineering Consultants, Inc.

Date: September 27, 2021 Revised: Project No: E8686

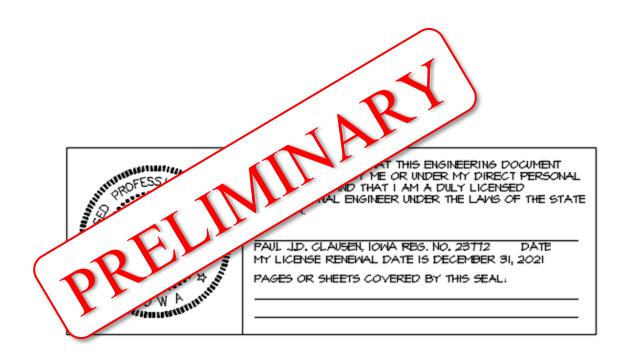


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1. Site Characteristics

a. Pre-developed Conditions

Hudson Heights Plat 2 is a 11.51-acre site located adjacent to and north of Park Street, west of Arlington Avenue, and south of Van Buren Drive in Van Meter, Iowa. The entire site will be disturbed during improvements. Stormwater runoff drains towards the east into unnamed ditches and streams, ending in the North Raccoon River.

The soils predominantly consist of Ladoga silty clay loam with slopes between 9% to 14%; Van Meter silt loam with slopes between 14% to 30%; and Colo, occasionally flooded-Ely silty clay loams, dissected till plain with slopes between 1% to 3%. Ladoga silty clay loam is classified as Hydrologic Soils Group C. Van Meter silt loam is classified as Hydrologic Soils Group D. Colo, occasionally flooded-Ely silty clay loams, dissected till plain is classified as Hydrologic Soils Group C/D. Hydrologic soils group C/D soils have a low infiltration rate when thoroughly wet with a slow rate of water transmission. The USDA Hydrologic Soils Report may be found in the Appendix.

b. Post-development Conditions

Hudson Heights Plat 2 project will consist of the development of twenty-six single-family residential lots and a 0.03-arce outlot. The entire site will be disturbed during improvements. Three detention basins will provide stormwater detention for the site. Two detention basins will be located on the northeast side of the site; the other basin will be centrally located on the south side of the site. The detention basins will release stormwater runoff into unnamed ditches and streams before ultimately draining to the North Raccoon River. The proposed conditions are assumed to have soils classified as Hydrologic Soils Group C.

c. Peak Stormwater Runoff Table

| Stormwater Runoff Rate Summary | | | | | | | |
|--------------------------------|---------|------------------|--------|---------|---------|---------|----------|
| A was Description | Area | Runoff Rate, cfs | | | | | |
| Area Description | (Acres) | 2-year | 5-year | 10-year | 25-year | 50-year | 100-year |
| EXISTING DA | 11.56 | 15.45 | 23.99 | 32.15 | 45.37 | 56.83 | 69.10 |
| OFFSITE WEST (DET) | 1.76 | 2.35 | 3.65 | 4.90 | 6.91 | 8.65 | 10.52 |
| OFFSITE SOUTH (UNDET) | 0.54 | 1.38 | 1.92 | 2.42 | 3.18 | 3.82 | 4.49 |
| OFFSITE CENTRAL (PASS-THRU) | 0.10 | 0.26 | 0.36 | 0.45 | 0.59 | 0.71 | 0.83 |
| OFFSITE NORTH (PASS-THRU) | 0.24 | 0.61 | 0.85 | 1.08 | 1.41 | 1.70 | 2.00 |
| DEV CENTRAL DA | 4.36 | 9.50 | 13.36 | 16.88 | 22.27 | 26.80 | 31.57 |
| DEV NORTH DA | 3.06 | 6.67 | 9.37 | 11.85 | 15.63 | 18.81 | 22.16 |
| DEVELOPED UNDETAINED | 4.14 | 7.37 | 10.79 | 14.01 | 19.00 | 23.25 | 27.75 |
| CENTRAL POND | | 0.63 | 0.67 | 0.69 | 0.72 | 0.74 | 0.76 |
| NORTH POND | | 0.24 | 0.26 | 0.28 | 0.30 | 0.32 | 0.33 |
| TOTAL SITE | | 8.24 | 11.72 | 14.98 | 20.02 | 24.31 | 28.84 |
| CENTRAL POND + PASS-THRU | | 0.63 | 0.67 | 0.69 | 0.72 | 0.74 | 0.76 |
| NORTH POND + PASS-THRU | | 0.24 | 0.27 | 0.29 | 0.31 | 0.33 | 0.34 |
| TOTAL SITE + OFFSITE RELEASE | | 9.22 | 13.13 | 16.76 | 22.36 | 27.12 | 32.15 |

d. Contributing Off-site Drainage

Approximately 2.40 acres of offsite area will drain onto the Hudson Heights Plat 2 site.

Offsite West consists of 1.76 acres of pasture and will be detained for on-site.

Offsite North consists of 0.24 acres of single-family residential, Offsite South consists of 0.54 acres of single-family residential, and Offsite Central consists of 0.10 acres of single-family residential. Offsite North, Offsite South, and Offsite Central will be treated as pass-thru. Refer to the drainage maps found in the Appendix.

e. Floodways, Floodplains and Wetlands

See Appendix for the Wetlands map and FIRM Panel Number 19049C0340F, effective date December 7, 2018.

2. Drainage Basin

a. Pre-developed Analysis

1) Pre-developed Land Use

All CN Values are from Section 2B-4

| Sub-Area | | Hydrologic | | Curve |
|-------------|------------------------|------------|-------|--------|
| Identifier | Land Use | Soil | Area | Number |
| | | Group | (ac) | |
| | | ~ | | |
| Existing DA | Pasture, grassland, or | С | 11.56 | 74 |
| 70.4.1 | Range – good condition | NT 1 | 11.50 | 74 |
| Total | Area / Weighted Curve | Number | 11.56 | 74 |
| | | | ===== | == |

2) Precipitation Model

Rainfall Intensity Duration Frequency (IDF) Curve.

| 1-Yr | 2-Yr | 5-Yr | 10-Yr | 25-Yr | 50-Yr | 100-Yr |
|------|------|------|-------|-------|-------|--------|
| | | | | | | |
| 2.67 | 3.08 | 3.81 | 4.46 | 5.44 | 6.26 | 7.12 |

3) Time of Concentration

| | | TIME OF CONCENTRATION |
|--------------|--------------------------------------|-----------------------|
| | | SUBAREA |
| | | Existing DA |
| | n (Manning's "n") | 0.15 |
| | L (length of flow) | 100.0 |
| SHEET FLOW | P2 (two year, 24 hr rainfall) | 3.08 |
| | S (slope in ft/ft) | 5.44% |
| | T _{SF} (MINUTES) | 6.69 |
| | | |
| | L (length of flow in feet) | 726.1 |
| CHALLOW | S (slope in ft/ft) | 8.73% |
| SHALLOW | Ground Cover | SHORT-GRASS |
| CONCENTRATED | Velocity Coefficent (TABLE 2-B-3.02) | 6.96 |
| FLOW | V (ft/sec) | 2.06 |
| | T _{CF} (MINUTES) | 5.88 |
| | | |
| | n (mannings "n") | N/A |
| | A (cross sectional area) | N/A |
| | P (wetted perimter) | N/A |
| CHANNEL FLOW | S (slope ft/ft) | N/A |
| | V (velocity ft/sec) | N/A |
| | L (Length of flow in feet) | N/A |
| | T _{CF} (MINUTES) | N/A |
| TIME OF | CONCENTRATION (MINUTES) | 12.58 |

4) Summary of Pre-Developed Runoff

Hydrograph Peak/Peak Time Table

| Sub-Area or Reach Identifier | | | 10-Yr (cfs) | | 50-Yr | eturn Period 100-Yr (cfs) (hr) |
|------------------------------------|-------|-------|-------------|-------|-------|---|
| SUBAREAS Existing DA | 15.45 | 23.99 | 32.15 | 45.37 | 56.83 | 69.10 |
| | 12.03 | 12.03 | 12.00 | 12.00 | 12.00 | 12.00 |

b. Offsite Runoff Analysis

1) Watershed Area

All CN Values are from Section 2B-4

| Sub-Area | | Hydrologi | c | Curve |
|-----------------|---|---------------|-----------|--------|
| Identifier | Land Use | Soil Group | Area (ac) | Number |
| Offsite West | Pasture, grassland, or Range – good condition | С | 1.76 | 74 |
| Offsite South | Residential district by average lot size – ½ acre | С | 0.54 | 83 |
| Offsite Central | Residential district by average lot size – ½ acre | С | 0.10 | 83 |
| Offsite North | Residential district by average lot size – ½ acre | С | 0.24 | 83 |

2) Time of Concentration

| | | TIME OF CONCENTRATION | | | | | |
|-------------------------|--------------------------------------|-----------------------|--|--|--|--|--|
| | | SUBAREA | | | | | |
| | | OFFSITE WEST | | | | | |
| | n (Manning's "n") | 0.15 | | | | | |
| | L (length of flow) | 100.0 | | | | | |
| SHEET FLOW | P2 (two year, 24 hr rainfall) | 3.08 | | | | | |
| | S (slope in ft/ft) | 3.29% | | | | | |
| | T _{SF} (MINUTES) | 8.18 | | | | | |
| | | | | | | | |
| | L (length of flow in feet) | 209.5 | | | | | |
| CHALLOW | S (slope in ft/ft) | 7.08% | | | | | |
| SHALLOW CONCENTRATED | Ground Cover | SHORT-GRASS | | | | | |
| FLOW | Velocity Coefficent (TABLE 2-B-3.02) | 6.96 | | | | | |
| FLOW | V (ft/sec) | 1.85 | | | | | |
| | T _{CF} (MINUTES) | 1.89 | | | | | |
| | | | | | | | |
| | n (mannings "n") | N/A | | | | | |
| | A (cross sectional area) | N/A | | | | | |
| | P (wetted perimter) | N/A | | | | | |
| CHANNEL FLOW | S (slope ft/ft) | N/A | | | | | |
| | V (velocity ft/sec) | N/A | | | | | |
| | L (Length of flow in feet) | N/A | | | | | |
| | T _{CF} (MINUTES) | N/A | | | | | |
| TIME OF | CONCENTRATION (MINUTES) | 10.07 | | | | | |

^{*}Min ToC of 5 minutes used for Offsite North, Offsite South, and Offsite Central.

3) Precipitation Model

Rainfall Intensity Duration Frequency (IDF) Curve.

| 1-Yr | 2-Yr | 5-Yr | 10-Yr | 25-Yr | 50-Yr | 100-Y | r |
|------|------|------|-------|-------|-------|-------|---|
| | | | | | | | |
| 2.67 | 3.08 | 3.81 | 4.46 | 5.44 | 6.26 | 7.12 | |

4) Summary of Offsite Runoff

Hydrograph Peak/Peak Time Table

| Sub-Area or Reach Identifier | Peak Flow a 2-Yr (cfs) (hr) | and Peak 5-Yr (cfs) (hr) | Time (h 10-Yr (cfs) (hr) | , , | | eturn Period 100-Yr (cfs) (hr) |
|------------------------------------|--------------------------------------|-----------------------------------|-----------------------------------|-------|-------|---|
| SUBAREAS | | | | | | |
| Offsite West | 2.35 | 3.65 | 4.90 | 6.91 | 8.65 | 10.52 |
| (Detained) | 12.03 | 12.03 | 12.00 | 12.00 | 12.00 | 12.00 |
| Offsite South | 1.38 | 1.92 | 2.42 | 3.18 | 3.82 | 4.49 |
| (Undetained) | 11.93 | 11.93 | 11.93 | 11.93 | 11.93 | 11.93 |
| Offsite Central | 0.26 | 0.36 | 0.45 | 0.59 | 0.71 | 0.83 |
| (Pass-Thru) | 11.93 | 11.93 | 11.93 | 11.93 | 11.93 | 11.93 |
| Offsite North | 0.61 | 0.85 | 1.08 | 1.41 | 1.70 | 2.00 |
| (Pass-Thru) | 11.93 | 11.93 | 11.93 | 11.93 | 11.93 | 11.93 |

c. Post-development Runoff Analysis

1) Developed Drainage Area

| Sub-Area Identifier | Land Use | Hydrologic Soil Group | Sub-Area Area (ac) | Curve Number |
|------------------------|---|-----------------------------|--------------------------|-----------------|
| Central DA | Residential districts by average lot size – ½ acre | С | 4.36 | 83 |
| North DA | Residential districts by average lot size – ¼ acre | С | 3.06 | 83 |
| DEV UNDET | Residential districts by average lot size – ½ acre – 1 acre | C C | 2.46 1.68 | 79 80 |
| | Total | C | 4.14 | 79 |

Total Area: 11.56

=====

2) Time of Concentration

The time of concentration for the Central DA, North DA, East DA, and DEV UNDET is assumed to be 10 minutes.

3) Summary of Developed Runoff

Hydrograph Peak/Peak Time Table

| Sub-Area or Reach Identifier | Peak Flow a 2-Yr (cfs) (hr) | 5-Yr (cfs) (hr) | | 25-Yr (cfs) (hr) | | eturn Period 100-Yr (cfs) (hr) |
|------------------------------------|--------------------------------------|-----------------------|----------------|------------------------|----------------|---|
| SUBAREAS Central DA | 9.50 12.00 | 13.36 12.00 | 16.88 12.00 | 22.27 12.00 | 26.80 12.00 | 31.57 12.00 |
| North DA | 6.67 12.00 | 9.37 12.00 | 11.85 12.00 | 15.63 12.00 | 18.81 12.00 | 22.16 12.00 |
| DEV UNDET | 7.37 12.03 | 10.79 12.00 | 14.01 12.00 | 19.00 12.00 | 23.25 12.00 | 27.75 12.00 |

d. Stormwater Conveyance Design

1) Design Information References

- i. The Rational Method was used to determine design flows. Manning's Equation was used to determine pipe capacities.
- ii. Intakes were located to provide bypass flows below the maximum 50% bypass flow for the 5-year event. (See Figure 5.1 Storm Sewer Intake Calculations)
- iii. Low point intakes were designed to intercept the 100-year storm event. Pipes downstream from low point intakes were designed to convey 100-year flows.
- iv. Cleansing velocities within storm sewer pipes were calculated using ½ full pipes. All cleansing velocities were between 3 fps and 15 fps.

2) Storm Sewer

- 1. Storm Sewer System
 - a. Intake Calculations

| Storm Sewer Calcu | lations f | for Huds | on Heial | nts Plat 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-----------------------|-----------|----------|----------|------------|------|------|-------|-------|--------|---------|-------------|----------|----------|----|------|---------|---------|-------|-----------------|-------------------------|-------------------|------|------|------|-------|-------|-------|----------|----------|----------|----------|
| * LP or CG= intake is | | | | | | | | | LP=0 | CG=1 | AREA=3 | 3 | | | | | | | | | | | | | | | | | | | |
| | | | | | | n = | 0.016 | Broom | Finish | Concret | te (typical | for most | streets) | | | | | | | | | | | | | | | | | | |
| Α | В | D | Е | F | G | Н | I | J | K | L | М | N | 0 | 0 | Р | R | | S | Р | Q | R | S | Т | U | V | W | Χ | Υ | Z | AA | AB |
| DRAINAGE AREA | Area | 15 | I10 | I100 | с5 | c10 | c100 | Q5 | Q10 | Q100 | q5 + | q10 + | q100 + | * | INT. | Slope | Street | Road | Q _{i5} | Q _{i10} | Q _{i100} | d5 | d10 | d100 | Qb5 | Qb10 | Qb100 | %Capture | %Capture | %Capture | Bypasses |
| IDENTIFIER | | (in/hr) | (in/hr) | (in/hr) | | | | (cfs) | (cfs) | (cfs) | bypass | bypass | bypass | CG | Туре | (ft/ft) | X-Slope | Width | (cfs) | (cfs) | (cfs) | ft | ft | (ft) | (cfs) | (cfs) | (cfs) | 5Yr | 10Yr | 100Yr | То |
| | (ac) | | | | | | | | | | | | | LP | SW- | | | (ft) | | | | | | | | | | | | | Intake |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ST 206 | 0.00 | 4.12 | 4.82 | 7.44 | 0.45 | 0.50 | 0.65 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0 | 501 | 4.00% | 2.00% | 13.0 | 0.06 | 0.06 | 0.06 | 0.03 | 0.03 | 0.03 | 0.00 | 0.00 | 0.00 | 100% | 100% | 100% | MANHOLE |
| 07.005 | 4.50 | 4.40 | 4.00 | 7.44 | 0.45 | 0.50 | 0.05 | 0.70 | 0.00 | 7.05 | 0.47 | 4.50 | 0.74 | | 505 | 4.0007 | 0.0007 | 40.0 | 0.00 | 0.04 | 7.05 | 0.40 | 0.40 | 0.40 | 0.44 | 0.57 | 0.00 | 070/ | 070/ | 700/ | OFFOITE |
| ST 205 | 1.50 | 4.12 | 4.82 | 7.44 | 0.45 | 0.50 | 0.65 | 2.78 | 3.62 | 7.25 | 3.47 | 4.52 | 9.74 | 1 | 505 | 4.00% | 2.00% | 13.0 | 3.03 | 3.94 | 7.65 | 0.13 | 0.13 | 0.13 | 0.44 | 0.57 | 2.09 | 87% | 87% | 79% | OFFSITE |
| ST 204 | 0.39 | 4.12 | 4.82 | 7.44 | 0.45 | 0.50 | 0.65 | 0.72 | 0.94 | 1.89 | 0.84 | 1.12 | 2.48 | 1 | 505 | 4.00% | 2.00% | 13.0 | 0.77 | 1.01 | 1.95 | 0.10 | 0.12 | 0.13 | 0.07 | 0.11 | 0.53 | 92% | 90% | 79% | OFFSITE |
| 31 204 | 0.59 | 4.12 | 4.02 | 7.44 | 0.43 | 0.50 | 0.03 | 0.12 | 0.94 | 1.03 | 0.04 | 1.12 | 2.40 | ' | 303 | 4.00 /6 | 2.0078 | 13.0 | 0.77 | 1.01 | 1.95 | 0.10 | 0.12 | 0.15 | 0.07 | 0.11 | 0.00 | 32 /0 | 3070 | 1370 | OFFORE |
| ST 106 | 0.00 | 4.12 | 4.82 | 7.44 | 0.45 | 0.50 | 0.65 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | 0 | 501 | 1.00% | 2.00% | 13.0 | 0.04 | 0.04 | 0.04 | 0.02 | 0.02 | 0.02 | 0.00 | 0.00 | 0.00 | 100% | 100% | 100% | MANHOLE |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ST 105 | 1.31 | 4.12 | 4.82 | 7.44 | 0.45 | 0.50 | 0.65 | 2.43 | 3.16 | 6.34 | 2.77 | 3.64 | 7.70 | 1 | 501 | 3.00% | 2.00% | 13.0 | 2.09 | 2.74 | 5.21 | 0.13 | 0.13 | 0.13 | 0.69 | 0.90 | 2.49 | 75% | 75% | 68% | ST 205 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ST 104 | 0.38 | 4.12 | 4.82 | 7.44 | 0.45 | 0.50 | 0.65 | 0.70 | 0.92 | 1.84 | 0.70 | 0.92 | 1.84 | 1 | 501 | 3.00% | 2.00% | 13.0 | 0.59 | 0.74 | 1.24 | 0.10 | 0.11 | 0.13 | 0.11 | 0.18 | 0.59 | 84% | 80% | 68% | ST 204 |
| ST 008 | 0.40 | 4.40 | 4.00 | 7.44 | 0.45 | 0.50 | 0.05 | 0.74 | 0.96 | 1.93 | 0.74 | 0.00 | 1.93 | 4 | 501 | 2.00% | 0.000/ | 40.0 | 0.60 | 0.77 | 1.37 | 0.44 | 0.42 | 0.13 | 0.40 | 0.20 | 0.57 | 83% | 80% | 71% | ST 105 |
| 31 008 | 0.40 | 4.12 | 4.82 | 7.44 | 0.45 | 0.50 | 0.65 | 0.74 | 0.96 | 1.93 | 0.74 | 0.96 | 1.93 | 1 | 501 | 2.00% | 2.00% | 13.0 | 0.62 | 0.77 | 1.37 | 0.11 | 0.13 | 0.13 | 0.12 | 0.20 | 0.57 | 03% | 00% | 11% | 31 105 |
| ST 007 | 0.56 | 4.12 | 4.82 | 7.44 | 0.45 | 0.50 | 0.65 | 1.04 | 1.35 | 2.71 | 1.04 | 1.35 | 2.71 | 1 | 501 | 2.00% | 2.00% | 13.0 | 0.82 | 1.06 | 1.91 | 0.13 | 0.13 | 0.13 | 0.22 | 0.29 | 0.80 | 79% | 78% | 71% | ST 105 |
| 3.00. | 0.00 | 1 | 1.02 | | 0.10 | 0.00 | 0.00 | 1.01 | 1.00 | ,, | 1.0 1 | 1.00 | | | | 2.0070 | 2.0070 | 10.0 | 0.02 | 1.00 | 1.01 | 3.10 | 5.10 | 3.10 | 3.22 | 0.23 | 0.00 | 1070 | 1070 | 7 1 70 | 0.100 |
| ST 005 | 1.61 | 4.12 | 4.82 | 7.44 | 0.45 | 0.50 | 0.65 | 2.98 | 3.88 | 7.79 | 2.98 | 3.88 | 7.79 | 1 | 505 | 6.25% | 2.00% | 13.0 | 2.50 | 3.25 | 5.87 | 0.13 | 0.13 | 0.13 | 0.48 | 0.63 | 1.92 | 84% | 84% | 75% | OFFSITE |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ST 004 | 0.34 | 4.12 | 4.82 | 7.44 | 0.45 | 0.50 | 0.65 | 0.63 | 0.82 | 1.64 | 0.63 | 0.82 | 1.64 | 1 | 505 | 6.25% | 2.00% | 13.0 | 0.59 | 0.75 | 1.26 | 0.09 | 0.10 | 0.12 | 0.04 | 0.07 | 0.38 | 94% | 92% | 77% | OFFSITE |

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b. Pipe Calculations

| | All Minimum Pipe Slopes are based on using RCP | | | | | | | | | | | | | |
|--------|--|--------|------------|--------------------------|---------------------------|---------------|---------|---------|---------|---------|---------|--------|-----------|-------|
| | | | N | lo Pipe Slopes les | ss than 0.40% | shall be used | | | | | | | | |
| Struc | to | Struc | Cumm | Cumm | Cumm | DESIGN | Min 24" | Min 21" | Min 18" | Min 15" | Min 12" | Min 8" | DIDE D | FOLON |
| | | | Q₅pipe cfs | Q ₁₀ pipe cfs | Q ₁₀₀ pipe cfs | STORM | | | | | | | PIPE DI | ESIGN |
| | | | | | | | 24 | 21 | 18 | 15 | 12 | 8 | PIPE SIZE | SLOPE |
| ST 206 | to | ST 204 | 0.06 | 0.06 | 0.06 | Q5pipe cfs | 0.00% | 0.00% | 0.00% | 0.00% | 0.00% | 0.00% | 8 | 4.75% |
| ST 205 | to | ST 204 | 3.03 | 3.94 | 7.65 | Q5pipe cfs | 0.02% | 0.04% | 0.08% | 0.22% | 0.72% | 2.99% | 15 | 1.00% |
| ST 204 | to | ST 203 | 3.86 | 5.01 | 9.66 | Q5pipe cfs | 0.03% | 0.06% | 0.13% | 0.36% | 1.17% | 4.86% | 15 | 3.50% |
| ST 203 | to | ST 202 | 3.86 | 5.01 | 9.66 | Q100pipe cfs | 0.18% | 0.37% | 0.84% | 2.22% | 7.31% | 30.47% | 15 | 8.00% |
| ST 202 | to | ST 201 | 3.86 | 5.01 | 9.66 | Q100pipe cfs | 0.18% | 0.37% | 0.84% | 2.22% | 7.31% | 30.47% | 18 | 2.00% |
| ST 106 | to | ST 103 | 0.04 | 0.04 | 0.04 | Q5pipe cfs | 0.00% | 0.00% | 0.00% | 0.00% | 0.00% | 0.00% | 8 | 2.75% |
| ST 105 | to | ST 104 | 2.09 | 2.74 | 5.21 | Q5pipe cfs | 0.01% | 0.02% | 0.04% | 0.10% | 0.34% | 1.42% | 15 | 1.00% |
| ST 104 | to | ST 103 | 2.68 | 3.48 | 6.46 | Q100pipe cfs | 0.08% | 0.17% | 0.38% | 0.99% | 3.27% | 13.62% | 15 | 1.00% |
| ST 103 | to | ST 102 | 2.72 | 3.52 | 6.50 | Q100pipe cfs | 0.08% | 0.17% | 0.38% | 1.01% | 3.31% | 13.79% | 15 | 7.50% |
| ST 102 | to | ST 101 | 2.72 | 3.52 | 6.50 | Q100pipe cfs | 0.08% | 0.17% | 0.38% | 1.01% | 3.31% | 13.79% | 18 | 0.50% |
| ST 008 | to | ST 007 | 0.62 | 0.77 | 1.37 | Q5pipe cfs | 0.00% | 0.00% | 0.00% | 0.01% | 0.03% | 0.12% | 15 | 1.00% |
| ST 007 | to | ST 006 | 1.43 | 1.83 | 3.28 | Q5pipe cfs | 0.00% | 0.01% | 0.02% | 0.05% | 0.16% | 0.67% | 15 | 1.00% |
| ST 006 | to | ST 004 | 1.43 | 1.83 | 3.28 | Q5pipe cfs | 0.00% | 0.01% | 0.02% | 0.05% | 0.16% | 0.67% | 15 | 3.00% |
| ST 005 | to | ST 004 | 2.50 | 3.25 | 5.87 | Q5pipe cfs | 0.01% | 0.02% | 0.06% | 0.15% | 0.49% | 2.04% | 15 | 1.00% |
| ST 004 | to | ST 003 | 4.53 | 5.83 | 10.41 | Q100pipe cfs | 0.21% | 0.43% | 0.98% | 2.58% | 8.49% | 35.37% | 15 | 8.00% |
| ST 003 | to | ST 002 | 4.53 | 5.83 | 10.41 | Q100pipe cfs | 0.21% | 0.43% | 0.98% | 2.58% | 8.49% | 35.37% | 15 | 8.00% |
| ST 002 | to | ST 001 | 4.53 | 5.83 | 10.41 | Q100pipe cfs | 0.21% | 0.43% | 0.98% | 2.58% | 8.49% | 35.37% | 18 | 2.50% |

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c. TR-55 Design Limitations

TR-55 includes a method for estimating required storage volume based upon peak inflow, peak outflow, and total runoff volume. This method may result in storage errors of 25% and should not be used in final design. The detention basin size in final design should be based upon actual hydrograph routing utilizing methods such as WINTR-55 or TR-20.

e. Stormwater Facilities Design – Onsite

1) Release Rate

The allowed release rate of the Hudson Heights Plat 2 site during the developed 100-year rain event will be limited to the peak stormwater runoff rate of the 5-year rain event with pre-developed conditions plus the release rate of 5-year storm for the detained offsite.

 $Q_{ALLOWABLE}$ release = Q_{5-YEAR} onsite predeveloped + Q_{5-YEAR} offsite west

 $Q_{ALLOWABLE RELEASE} = 23.99 \text{ cfs} + 3.65 \text{ cfs} = 27.64 \text{ cfs}$

 Q_{100} developed= Q_{100} central pond + Q_{100} north pond + Q_{100} dev undet

 $Q_{100 \text{ DEVELOPED}} = 0.76 \text{ cfs} + 0.33 \text{ cfs} + 27.75 \text{ cfs} = 28.84 \text{ cfs}$

2) Central Detention Basin Performance

The Hydraflow Hydrographs (see Appendix) show the detention basin performance for the developed Central Drainage Area + Offsite Central Pass-Thru. There will be a two-stage outlet structure for the detention pond. The outlet will consist of a 4" orifice set at an elevation of 942.00. The proposed detention basin will release 0.76 cfs from the site during the 100-year rain event with a high-water elevation of 953.98 and volume of 97,450 cubic feet.

The 2nd stage outlet weir will consist of an SW-513 area intake weir structure with openings on 3 sides set at an elevation of 954.00. This structure will allow for catastrophic flow events and offsite pass-thru flow to be conveyed downstream. There is a 20' emergency overflow at an elevation of 954.50 should the outlet structure fail. The top of pond is set at an elevation of 955.00 providing approximately 1.0' of freeboard during the 100-year rain event.

3) North Detention Basin Performance

The Hydraflow Hydrographs (see Appendix) show the detention basin performance for the developed North Drainage Area + Offsite North Pass-Thru. There will be a two-stage outlet structure for the detention pond. The outlet will consist of a 3" orifice set at an elevation of 935.00. The proposed detention basin will release 0.34 cfs from the site during the 100-year rain event with a highwater elevation of 944.85 and volume of 58,545 cubic feet.

The 2nd stage outlet weir will consist of an SW-513 area intake weir structure with openings on 3 sides set at an elevation of 945.00. This structure will allow for catastrophic flow events to be conveyed downstream. There is a 20' emergency overflow at an elevation of 945.50 should the outlet structure fail. The top of pond is set at an elevation of 946.00 providing approximately 1.1' of freeboard during the 100-year rain event.

3. Energy Dissipation Design

The soils predominantly consist of Ladoga silty clay loam with slopes between 9% to 14%; Vanmeter silt loam with slopes between 14% to 30%; and Colo, occasionally flooded-Ely silty clay loams, dissected till plain with slopes between 1% to 3%. Ladoga silty clay loam is classified as Hydrologic Soils Group C. Vanmeter silt loam is classified as Hydrologic Soils Group D. Colo, occasionally flooded-Ely silty clay loams, dissected till plain is classified as Hydrologic Soils Group C/D. Hydrologic soils group C/D soils have a low infiltration rate when thoroughly wet with a slow rate of water transmission. Flared end section discharging stormwater will have rip rap to dissipate the energy of the water flowing into adjacent waterways.

ST 001:

Release
$$Q_{100} = 10.41 \text{ cfs}$$

Pipe
$$V_{100} = 9.91 \text{ ft/s}$$

A 10' long x 18" deep apron (7.5 tons) of class 'E' riprap will be placed to prevent erosion. Refer to **Figure 7E-10.04:** Design of Outlet Protection, Maximum Tailwater Condition, see appendix.

ST 101:

Release
$$Q_{100} = 6.50 \text{ cfs}$$

Pipe
$$V_{100} = 4.71 \text{ ft/s}$$

A 10' long x 18" deep apron (7.5 tons) of class 'E' riprap will be placed to prevent erosion. Refer to **Figure 7E-10.04:** Design of Outlet Protection, Maximum Tailwater Condition, see appendix.

ST 201:

Release
$$Q_{100} = 9.66 \text{ cfs}$$

Pipe
$$V_{100} = 8.92 \text{ ft/s}$$

A 10' long x 18" deep apron (7.5 tons) of class 'E' riprap will be placed to prevent erosion. Refer to **Figure 7E-10.04:** Design of Outlet Protection, Maximum Tailwater Condition, see appendix.

ST 301:

Release
$$Q_{100} = 0.72 \text{ cfs}$$

Pipe
$$V_{100} = 4.14 \text{ ft/s}$$

A 10' long turf reinforcement mat (11 SY) will be placed at the end of ST 301 to prevent erosion.

ST 401:

Use 18" RCP @
$$0.50\%$$
, Release $Q_{100} = 0.21$ cfs

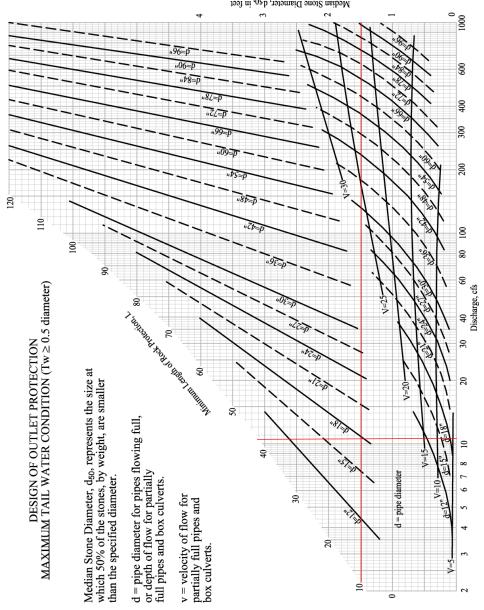
Release
$$O_{100} = 0.21 \text{ cfs}$$

Pipe
$$V_{100} = 2.08 \text{ ft/s}$$

A 10' long turf reinforcement mat (11 SY) will be placed at the end of ST 401 to prevent erosion.

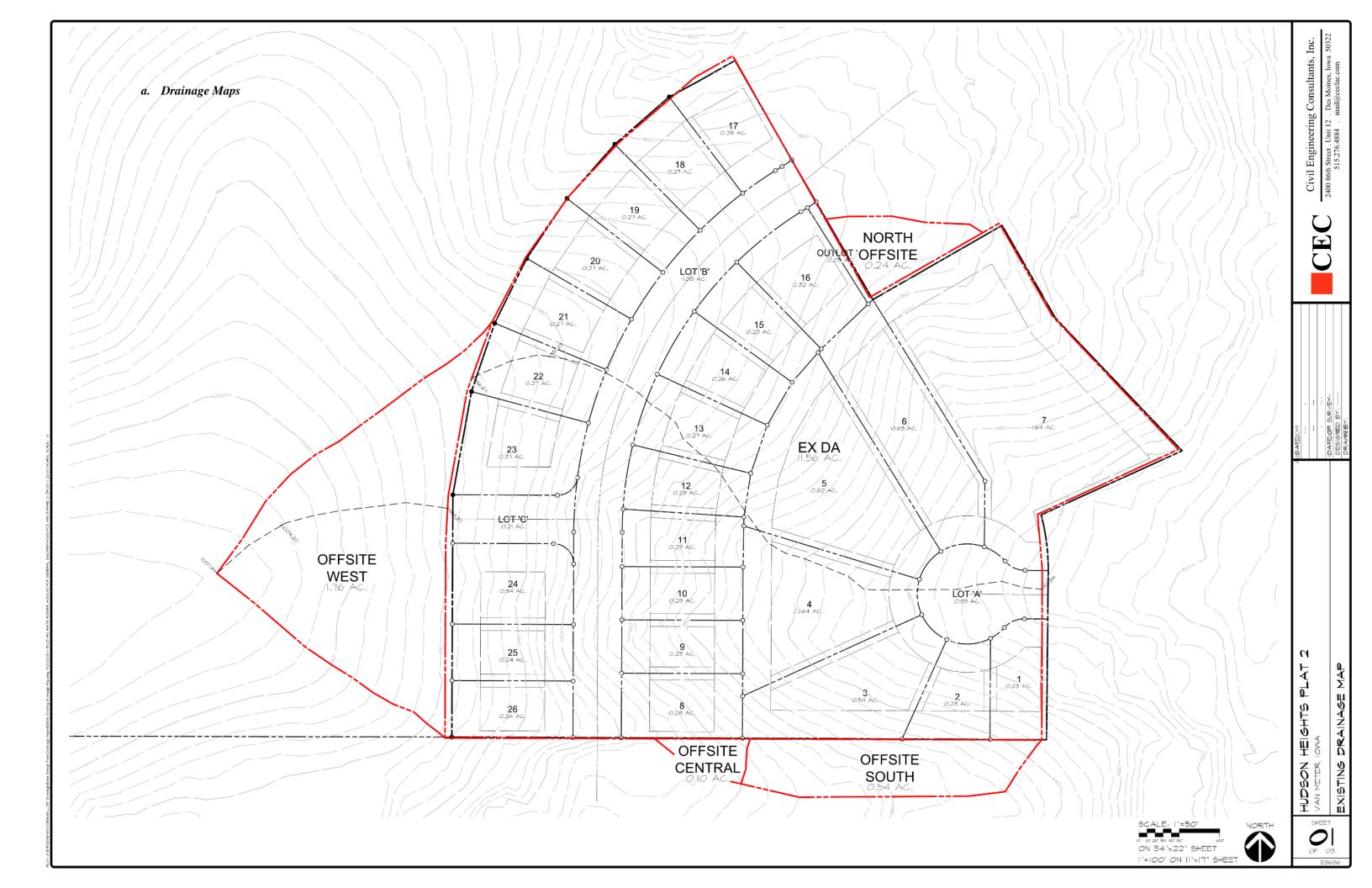
Chapter 7 - Erosion and Sediment Control Section 7E-10 - Rip Rap Revised: 2013 Edition

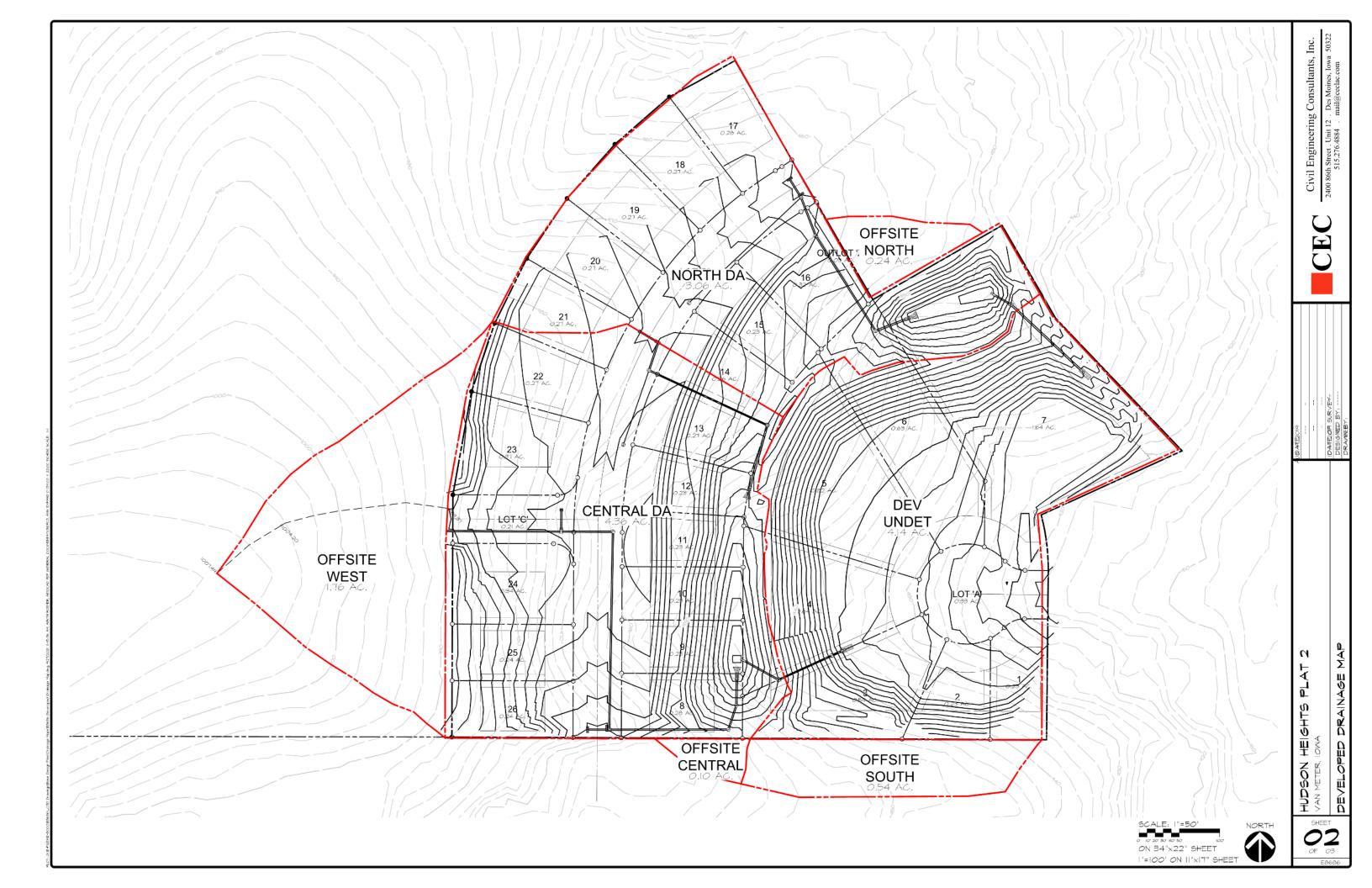
Figure 7E-10.04: Design of Outlet Protection, Maximum Tailwater Condition

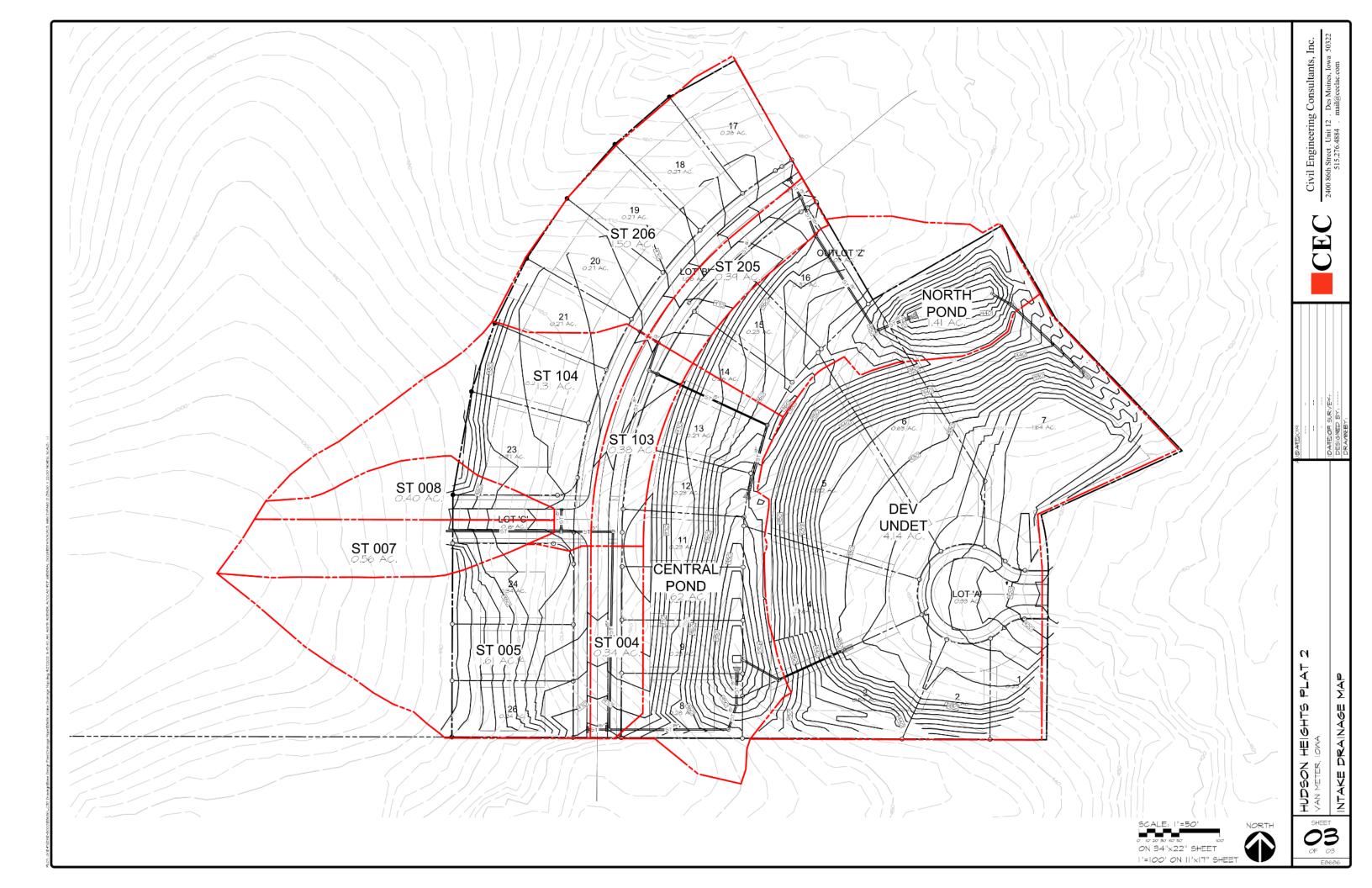


4. Permits

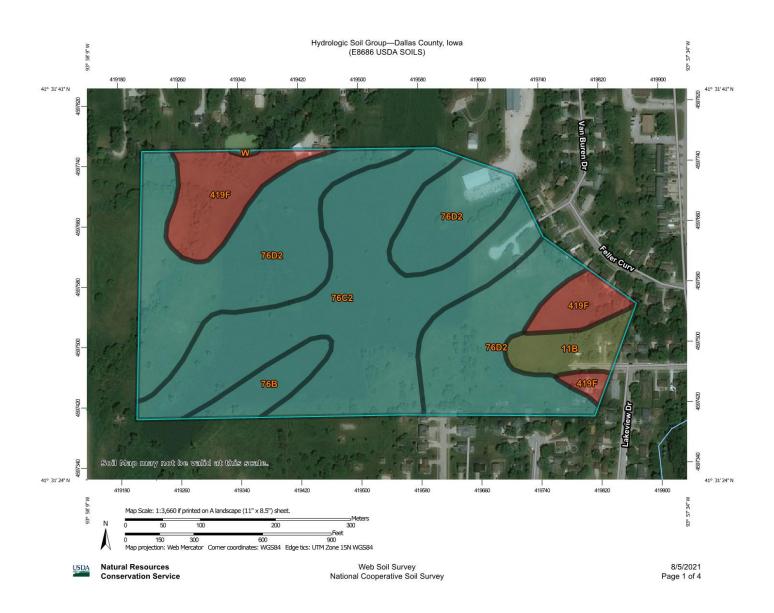
5. Appendix



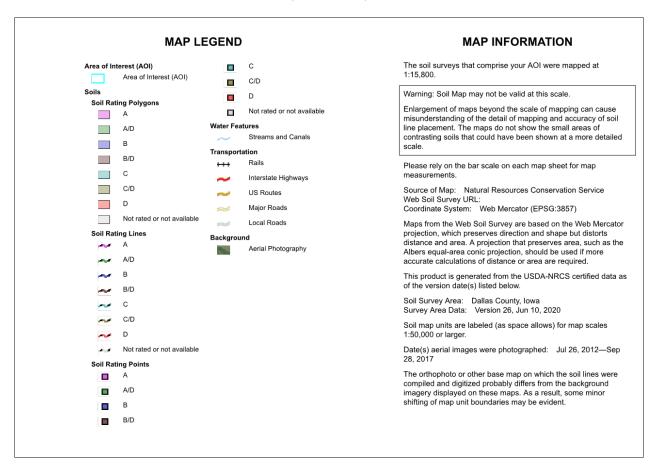


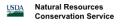


b. Web Soils Soil Report



Hydrologic Soil Group—Dallas County, Iowa (E8686 USDA SOILS)





Web Soil Survey National Cooperative Soil Survey 8/5/2021 Page 2 of 4

Hydrologic Soil Group

| | | | 1 | |
|--------------------------|--|--------|--------------|----------------|
| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
| 11B | Colo, occasionally flooded-Ely silty clay loams, dissected till plain, 2 to 5 percent slopes | C/D | 2.2 | 4.4% |
| 76B | Ladoga silt loam, 2 to 5 percent slopes | С | 2.0 | 3.9% |
| 76C2 | Ladoga silty clay loam, dissected till plain, 5 to 9 percent slopes, eroded | С | 17.9 | 35.1% |
| 76D2 | Ladoga silty clay loam, 9 to 14 percent slopes, eroded | С | 22.8 | 44.6% |
| 419F | Vanmeter silt loam, 14 to 30 percent slopes | D | 6.0 | 11.8% |
| W | Water | | 0.0 | 0.1% |
| Totals for Area of Inter | est | | 51.1 | 100.0% |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

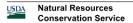
Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

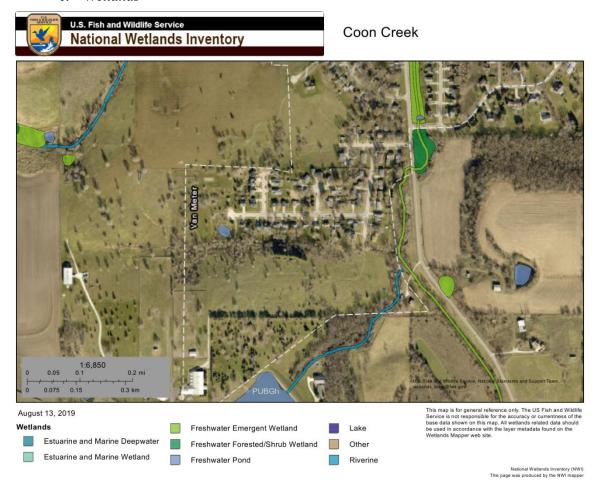
Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified

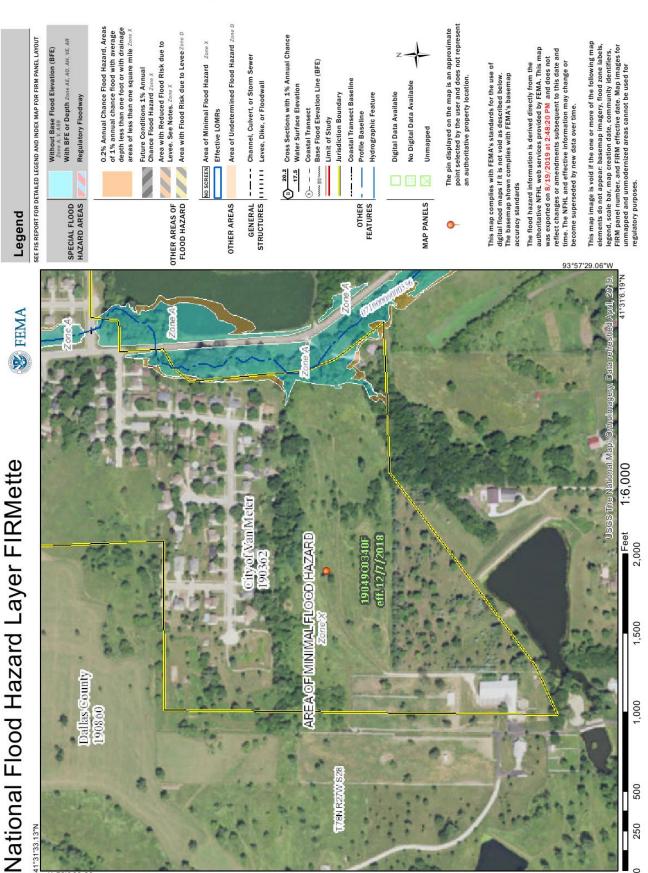
Tie-break Rule: Higher



c. Wetlands

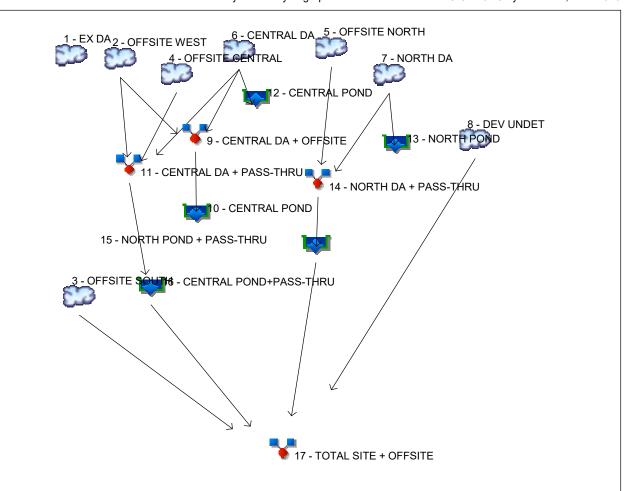


d. FEMA Flood Map



e. Hydrographs Report

Watershed Model Schematic



Legend

| <u>Hyd</u> | <u>l. Origin</u> | <u>Description</u> |
|------------|------------------|------------------------|
| 1 | SCS Runoff | EX DA |
| 2 | SCS Runoff | OFFSITE WEST |
| 3 | SCS Runoff | OFFSITE SOUTH |
| 4 | SCS Runoff | OFFSITE CENTRAL |
| 5 | SCS Runoff | OFFSITE NORTH |
| 6 | SCS Runoff | CENTRAL DA |
| 7 | SCS Runoff | NORTH DA |
| 8 | SCS Runoff | DEV UNDET |
| 9 | Combine | CENTRAL DA + OFFSITE |
| 10 | Reservoir | CENTRAL POND |
| 11 | Combine | CENTRAL DA + PASS-THRU |
| 12 | Reservoir | CENTRAL POND |
| 13 | Reservoir | NORTH POND |
| 14 | Combine | NORTH DA + PASS-THRU |
| 15 | Reservoir | NORTH POND + PASS-THRU |
| 16 | Reservoir | CENTRAL POND+PASS-THRU |
| 17 | Combine | TOTAL SITE + OFFSITE |
| | | |

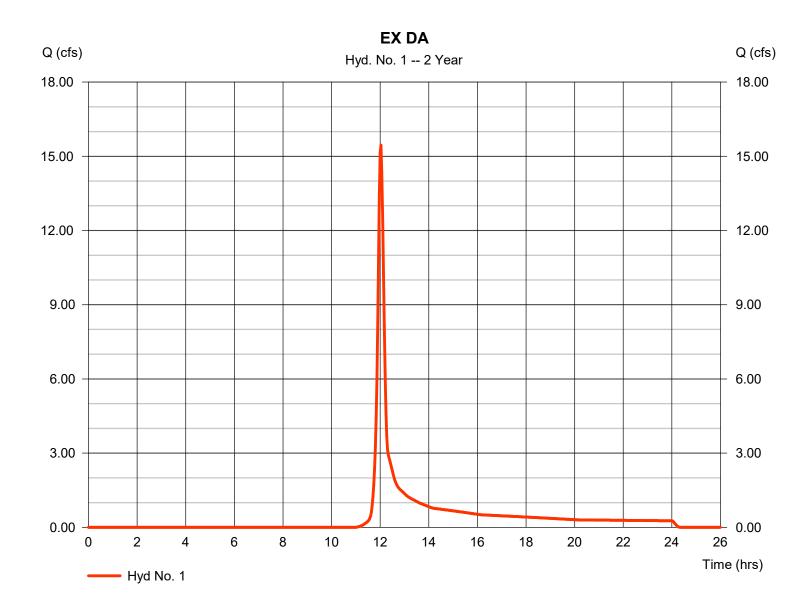
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Hyd. No. 1

EX DA

Hydrograph type = SCS Runoff Peak discharge = 15.45 cfsStorm frequency = 2 yrsTime to peak $= 12.03 \, hrs$ Time interval = 2 min Hyd. volume = 41,516 cuft Drainage area = 11.560 ac Curve number = 74 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) = 12.60 min = User Total precip. = 3.08 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



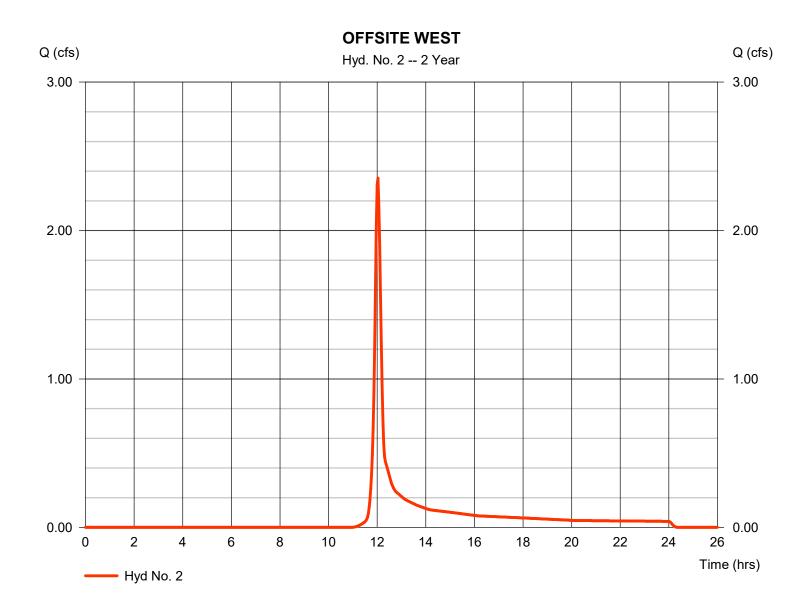
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Hyd. No. 2

OFFSITE WEST

Hydrograph type = SCS Runoff Peak discharge = 2.352 cfsStorm frequency = 2 yrsTime to peak $= 12.03 \, hrs$ Time interval = 2 min Hyd. volume = 6.321 cuftDrainage area = 1.760 acCurve number = 74 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 10.10 min = User Total precip. = 3.08 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



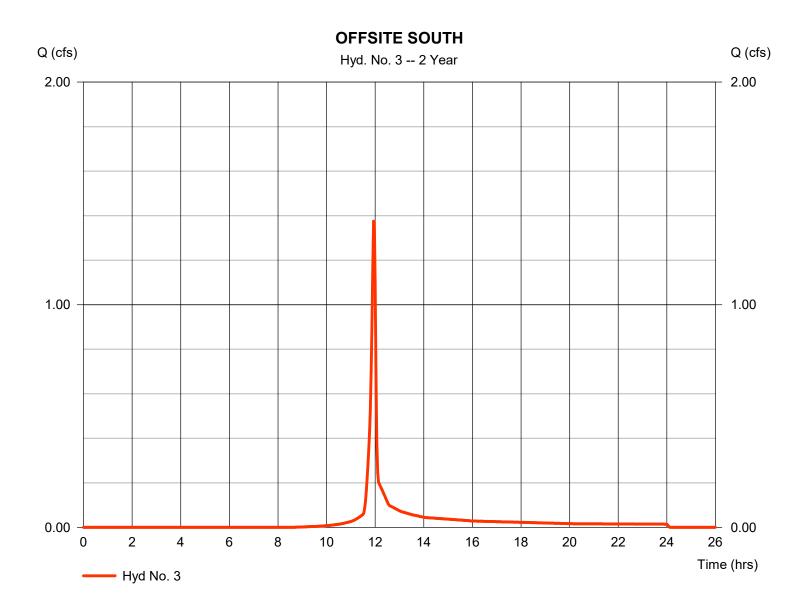
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Hyd. No. 3

OFFSITE SOUTH

= SCS Runoff Hydrograph type Peak discharge = 1.375 cfsStorm frequency = 2 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 2,777 cuftDrainage area = 0.540 acCurve number = 83 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.08 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



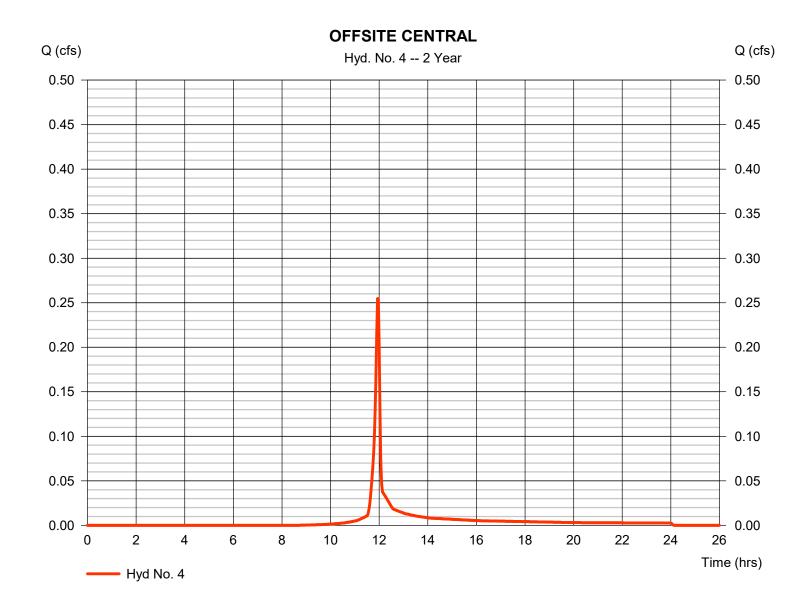
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Hyd. No. 4

OFFSITE CENTRAL

Hydrograph type = SCS Runoff Peak discharge = 0.255 cfsStorm frequency Time to peak = 2 yrs $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 514 cuft Drainage area Curve number = 0.100 ac= 83 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.08 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



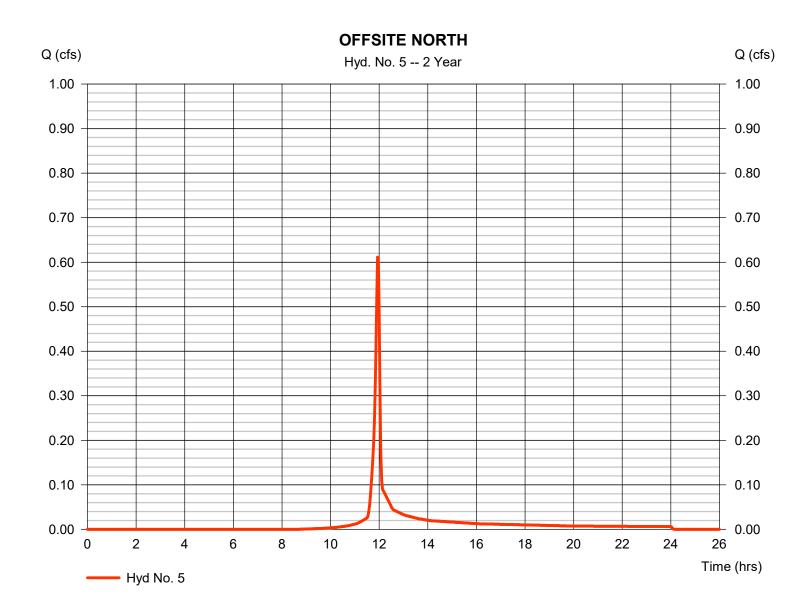
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Hyd. No. 5

OFFSITE NORTH

Hydrograph type = SCS Runoff Peak discharge = 0.611 cfsStorm frequency = 2 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 1.234 cuft Drainage area = 0.240 acCurve number = 83 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.08 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



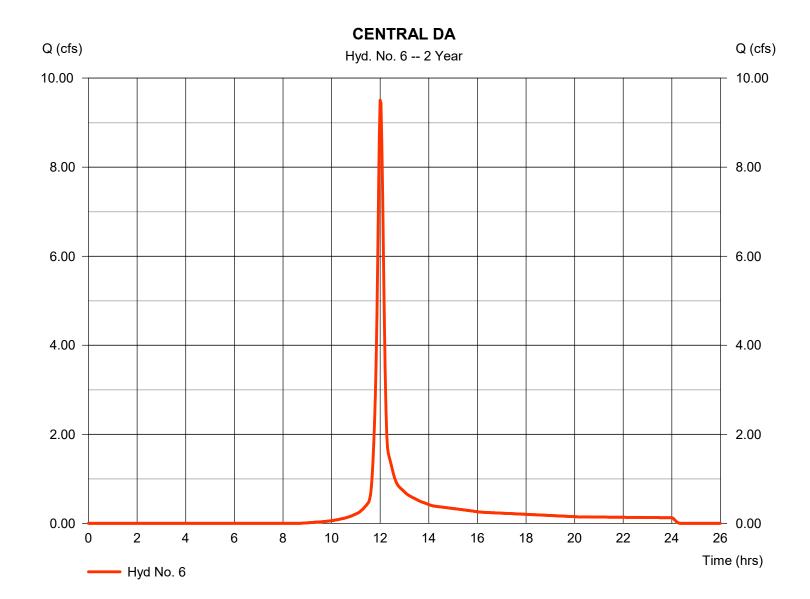
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Hyd. No. 6

CENTRAL DA

Hydrograph type = SCS Runoff Peak discharge = 9.501 cfsStorm frequency = 2 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 24,665 cuft Drainage area = 4.360 acCurve number = 83 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 3.08 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



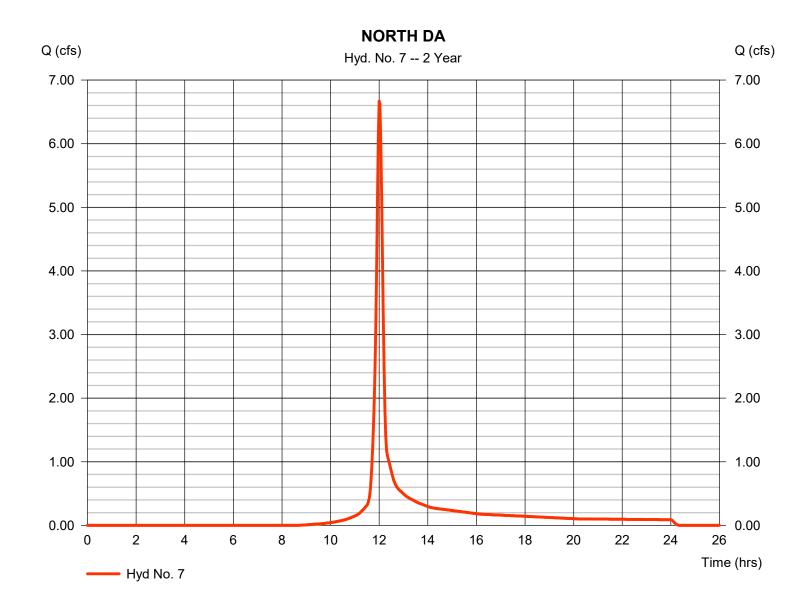
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Hyd. No. 7

NORTH DA

Hydrograph type = SCS Runoff Peak discharge = 6.668 cfsStorm frequency = 2 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 17,311 cuft Drainage area = 3.060 acCurve number = 83 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 10.00 min = User Total precip. = 3.08 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

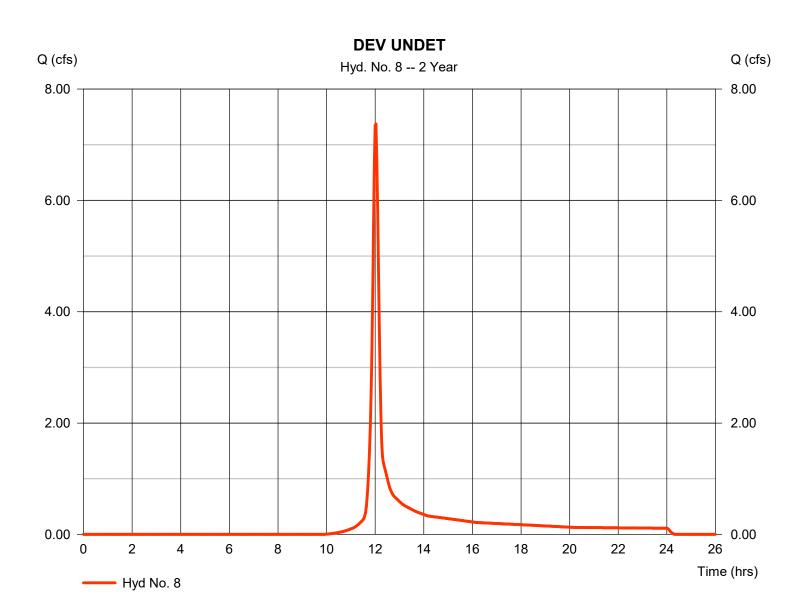
Monday, 09 / 27 / 2021

Hyd. No. 8

DEV UNDET

Hydrograph type = SCS Runoff Peak discharge = 7.372 cfsStorm frequency = 2 yrsTime to peak $= 12.03 \, hrs$ Time interval = 2 min Hyd. volume = 19,330 cuftDrainage area = 4.140 acCurve number = 79* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 3.08 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(2.460 x 79) + (1.680 x 80)] / 4.140



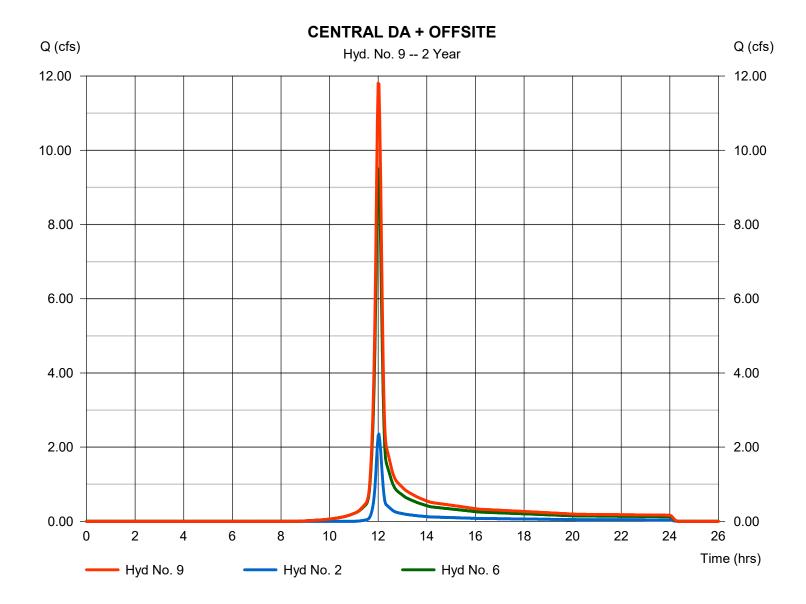
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Hyd. No. 9

CENTRAL DA + OFFSITE

Hydrograph type = Combine Peak discharge = 11.81 cfsStorm frequency Time to peak = 2 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 30,986 cuft Inflow hyds. = 2,6 Contrib. drain. area = 6.120 ac



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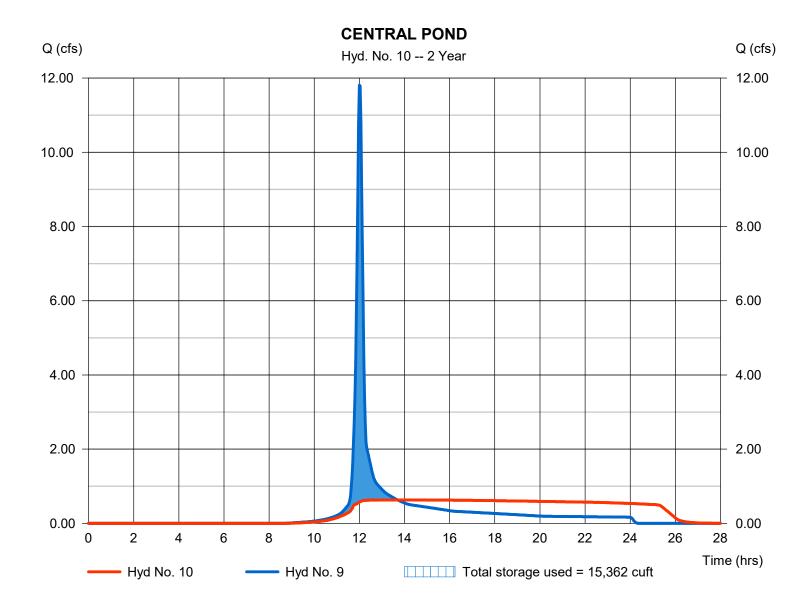
Monday, 09 / 27 / 2021

Hyd. No. 10

CENTRAL POND

Hydrograph type Peak discharge = 0.630 cfs= Reservoir Storm frequency = 2 yrsTime to peak $= 13.70 \, hrs$ Time interval = 2 min Hyd. volume = 30,985 cuftInflow hyd. No. = 9 - CENTRAL DA + OFFSITE Max. Elevation = 948.37 ft= CENTRAL POND Reservoir name Max. Storage = 15,362 cuft

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Pond No. 2 - CENTRAL POND

Pond Data

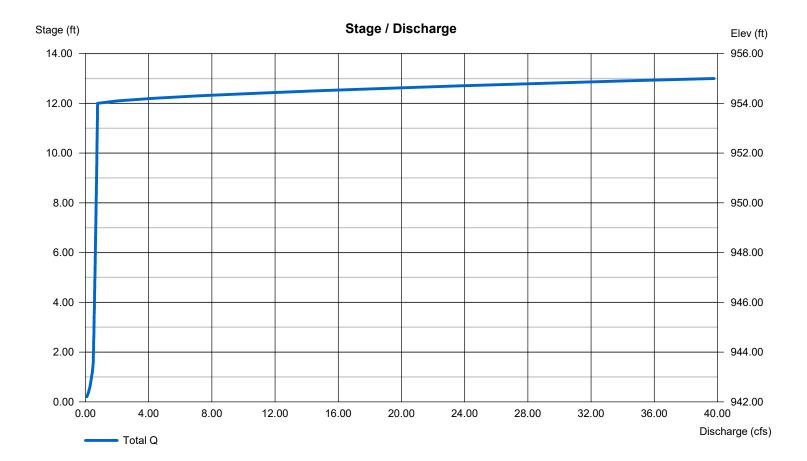
Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 942.00 ft

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 942.00 | 90 | 0 | 0 |
| 2.00 | 944.00 | 1,190 | 1,280 | 1,280 |
| 4.00 | 946.00 | 2,760 | 3,950 | 5,230 |
| 6.00 | 948.00 | 4,970 | 7,730 | 12,960 |
| 8.00 | 950.00 | 8,020 | 12,990 | 25,950 |
| 10.00 | 952.00 | 12,470 | 20,490 | 46,440 |
| 12.00 | 954.00 | 18,250 | 30,720 | 77,160 |
| 13.00 | 955.00 | 22,330 | 20,290 | 97,450 |

Weir Structures Culvert / Orifice Structures [B] [C] [PrfRsr] [A] [B] [C] [D] [A] = 4.00 0.00 0.00 0.00 = 15.00 0.00 0.00 0.00 Rise (in) Crest Len (ft) Span (in) = 4.000.00 0.00 0.00 Crest El. (ft) = 954.00 0.00 0.00 0.00 No. Barrels 0 Weir Coeff. = 2.60 3.33 3.33 3.33 Invert El. (ft) = 942.00 0.00 0.00 0.00 Weir Type = Broad Length (ft) = 100.00 0.00 0.00 0.00 Multi-Stage = No No No No Slope (%) = 6.00 0.00 0.00 n/a N-Value = .013 .013 .013 n/a = 0.60 0.60 0.60 0.60 = 0.000 (by Wet area) Orifice Coeff. Exfil.(in/hr) Multi-Stage = n/aNo No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



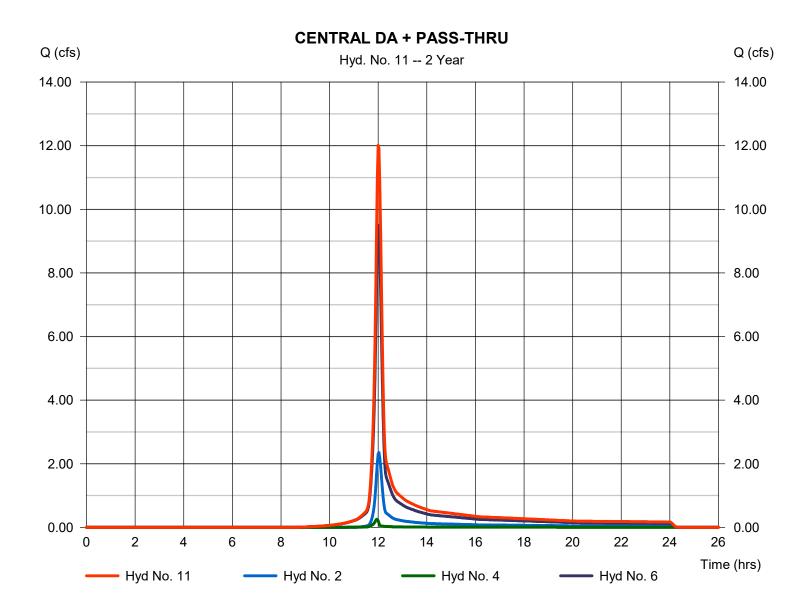
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Monday, 09 / 27 / 2021

Hyd. No. 11

CENTRAL DA + PASS-THRU

Hydrograph type = Combine Peak discharge = 12.01 cfsStorm frequency Time to peak = 2 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 31,501 cuft Inflow hyds. = 2, 4, 6Contrib. drain. area = 6.220 ac



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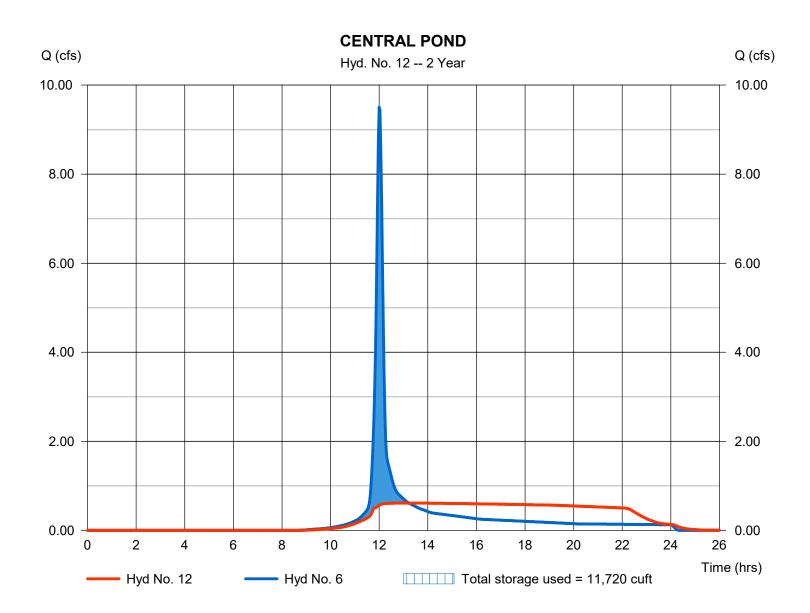
Monday, 09 / 27 / 2021

Hyd. No. 12

CENTRAL POND

Hydrograph type = Reservoir Peak discharge = 0.612 cfsStorm frequency = 2 yrsTime to peak $= 13.23 \, hrs$ Time interval = 2 min Hyd. volume = 24,664 cuft Inflow hyd. No. Max. Elevation = 6 - CENTRAL DA = 947.68 ft= CENTRAL POND Reservoir name Max. Storage = 11,720 cuft

Storage Indication method used.



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Monday, 09 / 27 / 2021

Pond No. 2 - CENTRAL POND

Pond Data

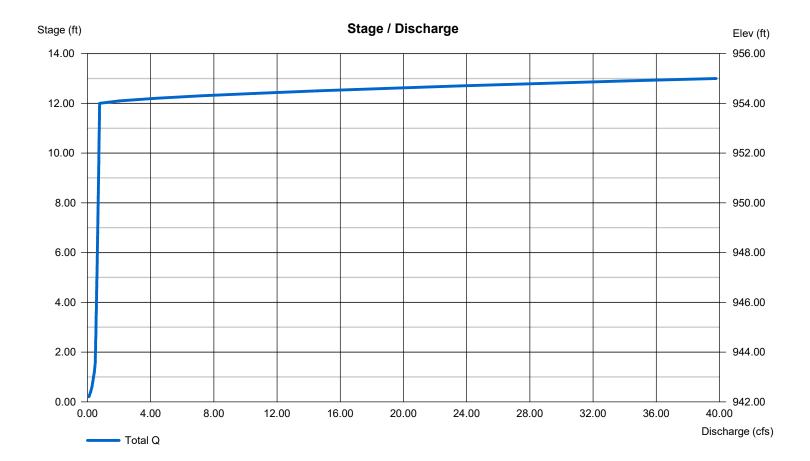
Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 942.00 ft

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 942.00 | 90 | 0 | 0 |
| 2.00 | 944.00 | 1,190 | 1,280 | 1,280 |
| 4.00 | 946.00 | 2,760 | 3,950 | 5,230 |
| 6.00 | 948.00 | 4,970 | 7,730 | 12,960 |
| 8.00 | 950.00 | 8,020 | 12,990 | 25,950 |
| 10.00 | 952.00 | 12,470 | 20,490 | 46,440 |
| 12.00 | 954.00 | 18,250 | 30,720 | 77,160 |
| 13.00 | 955.00 | 22,330 | 20,290 | 97,450 |

Weir Structures Culvert / Orifice Structures [B] [C] [PrfRsr] [A] [B] [C] [D] [A] = 4.00 0.00 0.00 0.00 = 15.00 0.00 0.00 0.00 Rise (in) Crest Len (ft) Span (in) = 4.000.00 0.00 0.00 Crest El. (ft) = 954.00 0.00 0.00 0.00 No. Barrels 0 Weir Coeff. = 2.60 3.33 3.33 3.33 Invert El. (ft) = 942.00 0.00 0.00 0.00 Weir Type = Broad Length (ft) = 100.00 0.00 0.00 0.00 Multi-Stage = No No No No Slope (%) = 6.00 0.00 0.00 n/a N-Value = .013 .013 .013 n/a = 0.60 0.60 0.60 0.60 = 0.000 (by Wet area) Orifice Coeff. Exfil.(in/hr) Multi-Stage = n/aNo No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

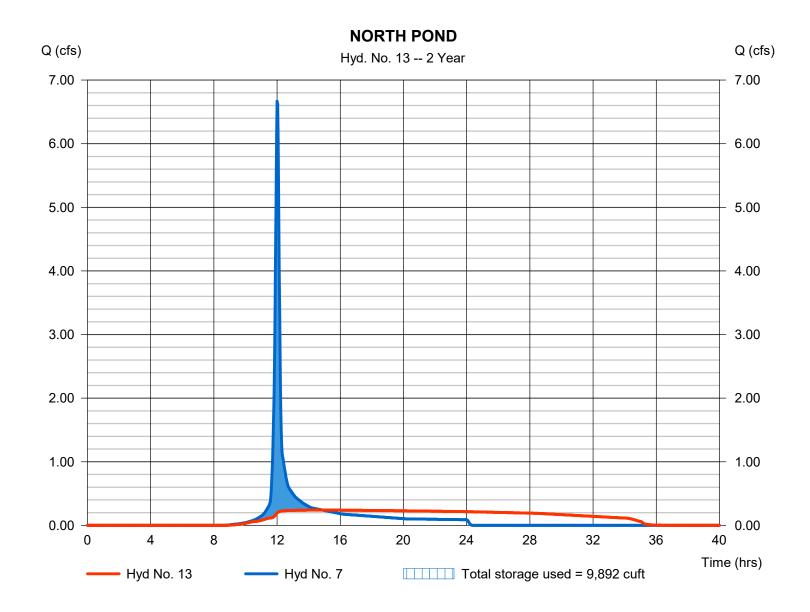
Monday, 09 / 27 / 2021

Hyd. No. 13

NORTH POND

Hydrograph type = Reservoir Peak discharge = 0.239 cfsStorm frequency = 2 yrsTime to peak $= 14.90 \, hrs$ Time interval = 2 min Hyd. volume = 17,310 cuftInflow hyd. No. = 7 - NORTH DA Max. Elevation = 939.83 ft= NORTH POND Reservoir name Max. Storage = 9,892 cuft

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Pond No. 1 - NORTH POND

Pond Data

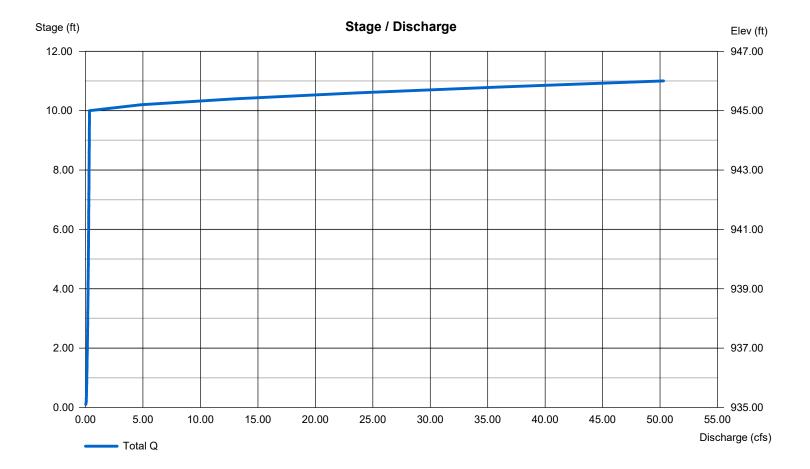
Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 935.00 ft

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 935.00 | 10 | 0 | 0 |
| 1.00 | 936.00 | 580 | 295 | 295 |
| 3.00 | 938.00 | 2,560 | 3,140 | 3,435 |
| 5.00 | 940.00 | 4,510 | 7,070 | 10,505 |
| 7.00 | 942.00 | 6,700 | 11,210 | 21,715 |
| 9.00 | 944.00 | 9,140 | 15,840 | 37,555 |
| 11.00 | 946.00 | 11,850 | 20,990 | 58,545 |

Culvert / Orifice Structures Weir Structures [A] [B] [C] [PrfRsr] [A] [B] [C] [D] 0.00 = 3.000.00 0.00 0.00 = 15.00 0.00 0.00 Rise (in) Crest Len (ft) = 3.000.00 0.00 0.00 Crest El. (ft) = 945.00 0.00 0.00 0.00 Span (in) Weir Coeff. 3.33 No. Barrels = 1 0 = 3.333.33 3.33 0.00 Invert El. (ft) = 935.00 0.00 0.00 Weir Type = Broad = 60.00 0.00 0.00 0.00 Multi-Stage = No No No No Length (ft) 0.00 0.00 Slope (%) = 0.50n/a N-Value = .013 .013 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 0.000 (by Wet area) Multi-Stage = n/aNo No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



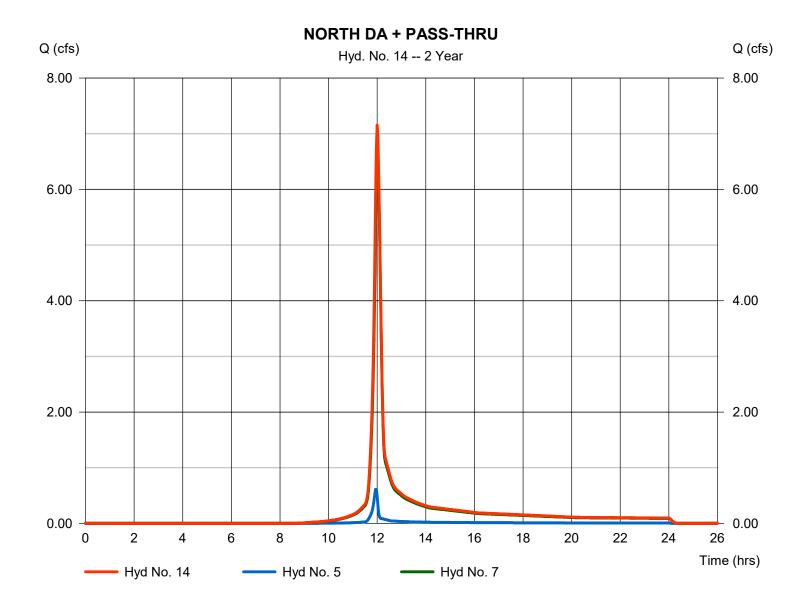
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Monday, 09 / 27 / 2021

Hyd. No. 14

NORTH DA + PASS-THRU

Hydrograph type = Combine Peak discharge = 7.158 cfsStorm frequency = 2 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 18,545 cuft Inflow hyds. = 5, 7Contrib. drain. area = 3.300 ac



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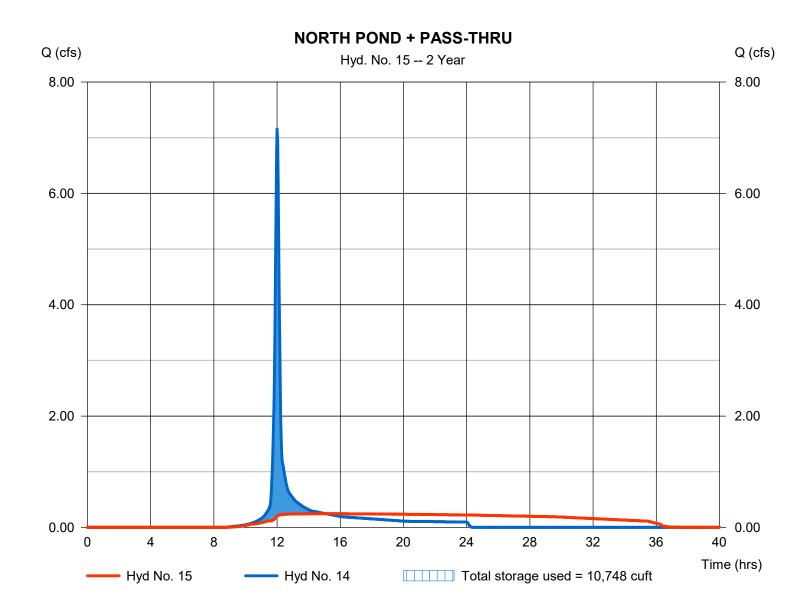
Monday, 09 / 27 / 2021

Hyd. No. 15

NORTH POND + PASS-THRU

Hydrograph type Peak discharge = 0.244 cfs= Reservoir Storm frequency = 2 yrsTime to peak $= 15.10 \, hrs$ Time interval = 2 min Hyd. volume = 18,544 cuft Inflow hyd. No. = 14 - NORTH DA + PASS-THR Max. Elevation = 940.04 ft= NORTH POND Reservoir name Max. Storage = 10,748 cuft

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

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Pond No. 1 - NORTH POND

Pond Data

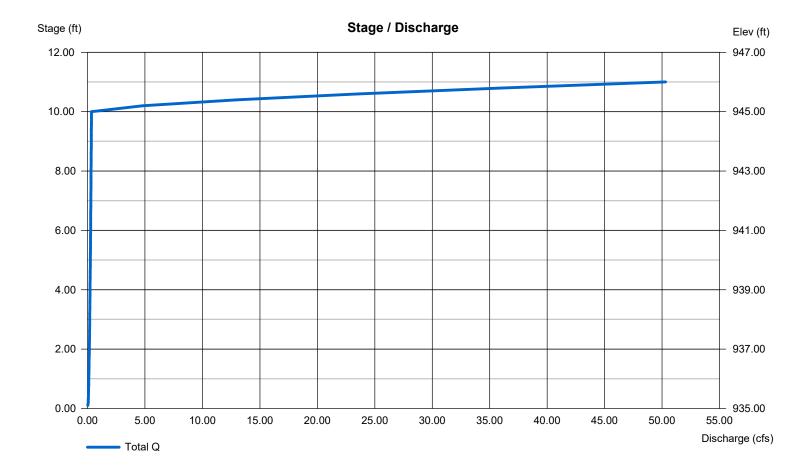
Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 935.00 ft

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 935.00 | 10 | 0 | 0 |
| 1.00 | 936.00 | 580 | 295 | 295 |
| 3.00 | 938.00 | 2,560 | 3,140 | 3,435 |
| 5.00 | 940.00 | 4,510 | 7,070 | 10,505 |
| 7.00 | 942.00 | 6,700 | 11,210 | 21,715 |
| 9.00 | 944.00 | 9,140 | 15,840 | 37,555 |
| 11.00 | 946.00 | 11,850 | 20,990 | 58,545 |

Culvert / Orifice Structures Weir Structures [A] [B] [C] [PrfRsr] [A] [B] [C] [D] 0.00 = 3.000.00 0.00 0.00 = 15.00 0.00 0.00 Rise (in) Crest Len (ft) = 3.000.00 0.00 0.00 Crest El. (ft) = 945.00 0.00 0.00 0.00 Span (in) Weir Coeff. 3.33 No. Barrels = 1 0 = 3.333.33 3.33 0.00 Invert El. (ft) = 935.00 0.00 0.00 Weir Type = Broad = 60.00 0.00 0.00 0.00 = No No No No Length (ft) Multi-Stage 0.00 0.00 Slope (%) = 0.50n/a N-Value = .013 .013 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 0.000 (by Wet area) Multi-Stage = n/aNo No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



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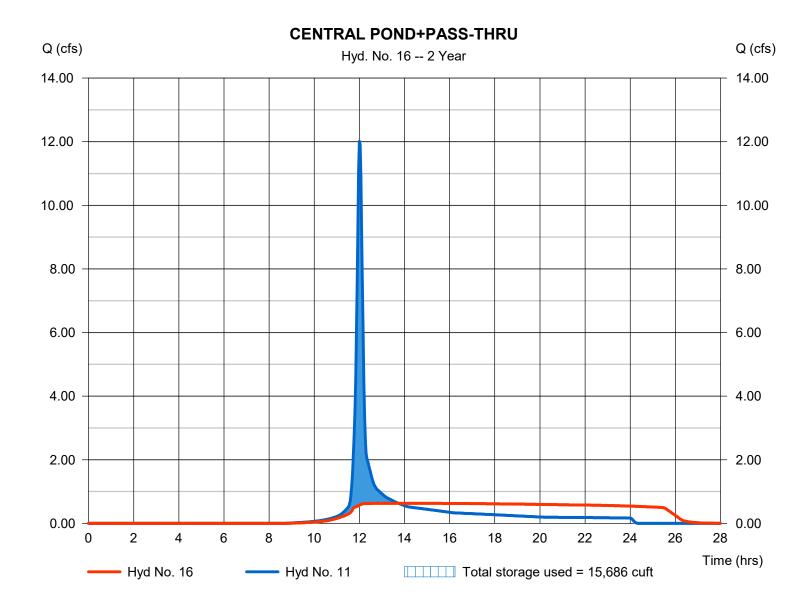
Monday, 09 / 27 / 2021

Hyd. No. 16

CENTRAL POND+PASS-THRU

Hydrograph type Peak discharge = 0.632 cfs= Reservoir Storm frequency = 2 yrsTime to peak $= 13.73 \, hrs$ Time interval = 2 min Hyd. volume = 31,499 cuftInflow hyd. No. = 11 - CENTRAL DA + PASS-THARAUX. Elevation = 948.42 ft= CENTRAL POND Reservoir name Max. Storage = 15,686 cuft

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Pond No. 2 - CENTRAL POND

Pond Data

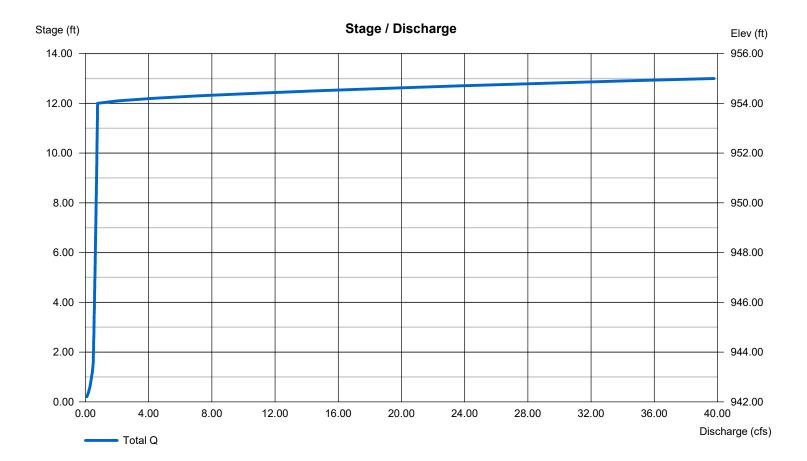
Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 942.00 ft

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 942.00 | 90 | 0 | 0 |
| 2.00 | 944.00 | 1,190 | 1,280 | 1,280 |
| 4.00 | 946.00 | 2,760 | 3,950 | 5,230 |
| 6.00 | 948.00 | 4,970 | 7,730 | 12,960 |
| 8.00 | 950.00 | 8,020 | 12,990 | 25,950 |
| 10.00 | 952.00 | 12,470 | 20,490 | 46,440 |
| 12.00 | 954.00 | 18,250 | 30,720 | 77,160 |
| 13.00 | 955.00 | 22,330 | 20,290 | 97,450 |

Weir Structures Culvert / Orifice Structures [B] [C] [PrfRsr] [A] [B] [C] [D] [A] = 4.00 0.00 0.00 0.00 = 15.00 0.00 0.00 0.00 Rise (in) Crest Len (ft) Span (in) = 4.000.00 0.00 0.00 Crest El. (ft) = 954.00 0.00 0.00 0.00 No. Barrels 0 Weir Coeff. = 2.60 3.33 3.33 3.33 Invert El. (ft) = 942.00 0.00 0.00 0.00 Weir Type = Broad Length (ft) = 100.00 0.00 0.00 0.00 Multi-Stage = No No No No Slope (%) = 6.00 0.00 0.00 n/a N-Value = .013 .013 .013 n/a = 0.60 0.60 0.60 0.60 = 0.000 (by Wet area) Orifice Coeff. Exfil.(in/hr) Multi-Stage = n/aNo No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



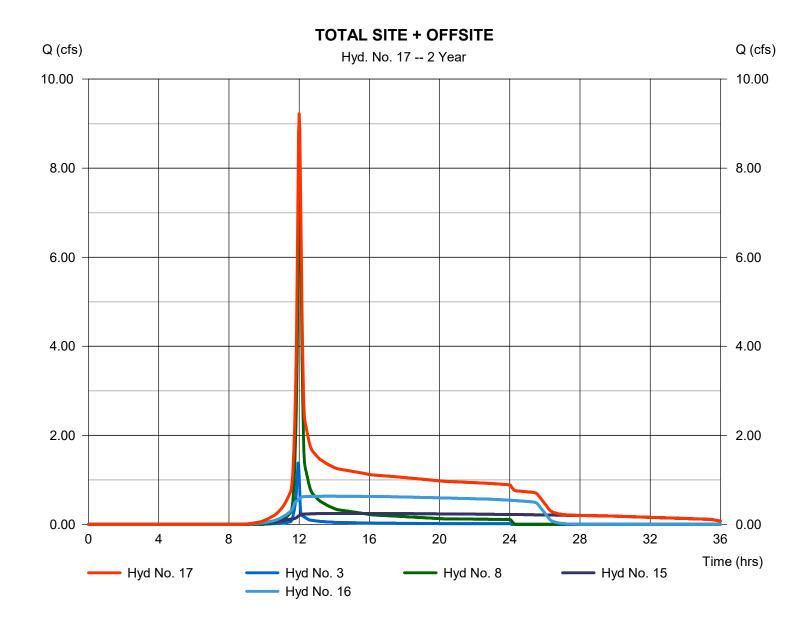
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Monday, 09 / 27 / 2021

Hyd. No. 17

TOTAL SITE + OFFSITE

Hydrograph type = Combine Peak discharge = 9.222 cfsStorm frequency Time to peak = 2 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 72,150 cuftInflow hyds. = 3, 8, 15, 16 Contrib. drain. area = 4.680 ac



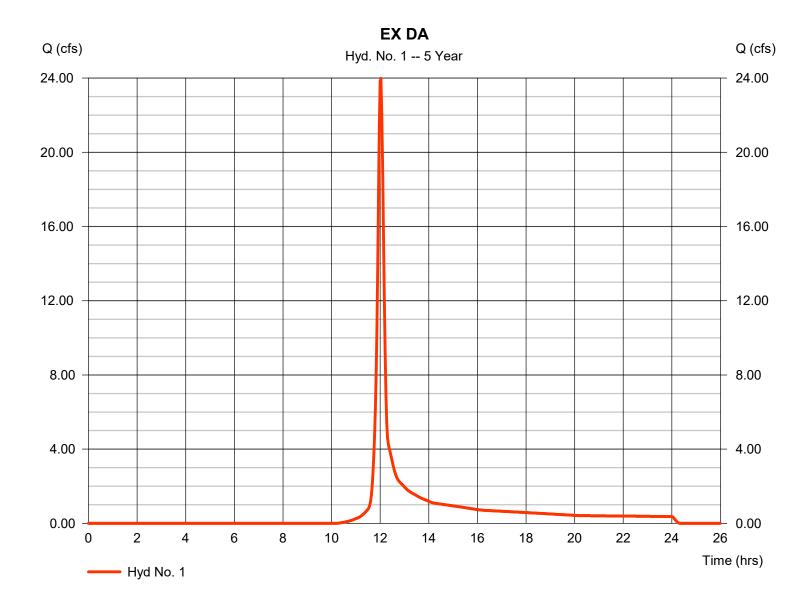
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Monday, 09 / 27 / 2021

Hyd. No. 1

EX DA

Hydrograph type = SCS Runoff Peak discharge = 23.99 cfsStorm frequency = 5 yrsTime to peak $= 12.03 \, hrs$ Time interval = 2 min Hyd. volume = 63,108 cuft Drainage area = 11.560 ac Curve number = 74 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 12.60 min = User Total precip. = 3.81 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



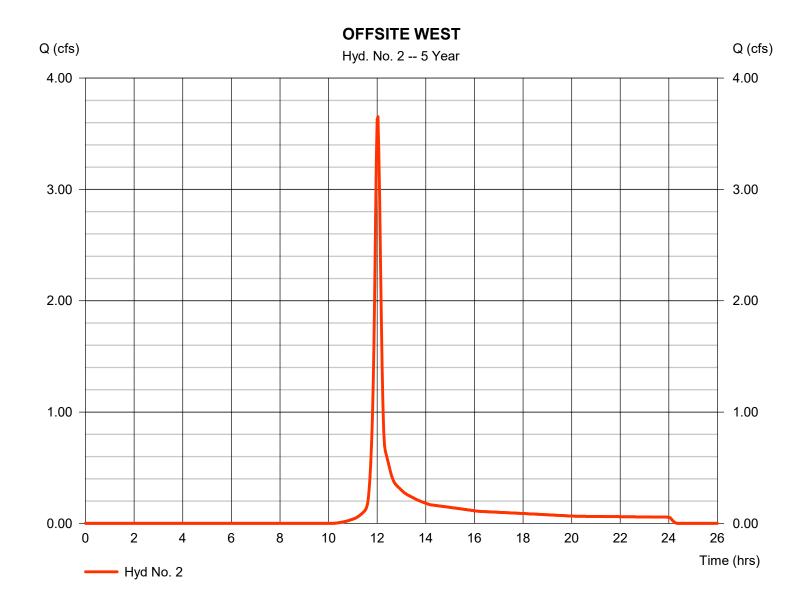
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Monday, 09 / 27 / 2021

Hyd. No. 2

OFFSITE WEST

Hydrograph type = SCS Runoff Peak discharge = 3.652 cfsStorm frequency = 5 yrsTime to peak $= 12.03 \, hrs$ Time interval = 2 min Hyd. volume = 9,608 cuftDrainage area = 1.760 acCurve number = 74 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) = 10.10 min = User Total precip. = 3.81 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



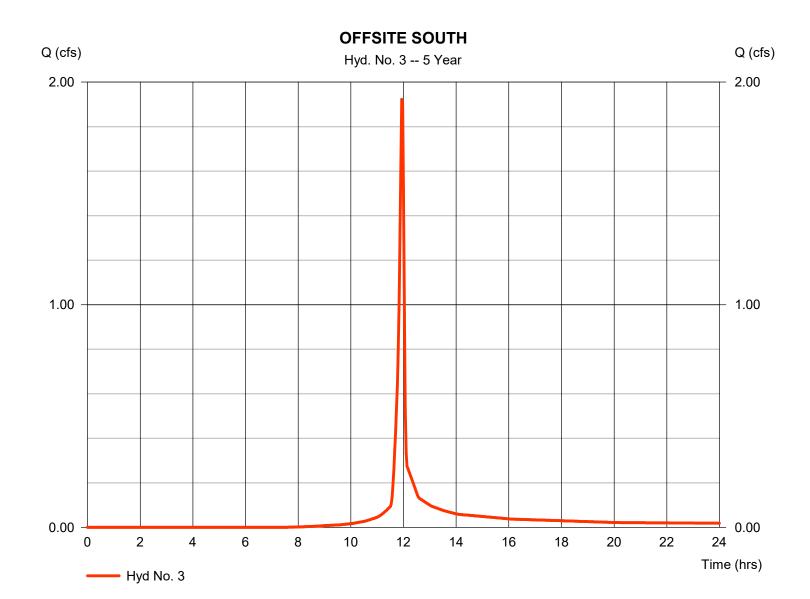
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Monday, 09 / 27 / 2021

Hyd. No. 3

OFFSITE SOUTH

= SCS Runoff Hydrograph type Peak discharge = 1.922 cfsStorm frequency = 5 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 3,900 cuftDrainage area = 0.540 acCurve number = 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.81 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



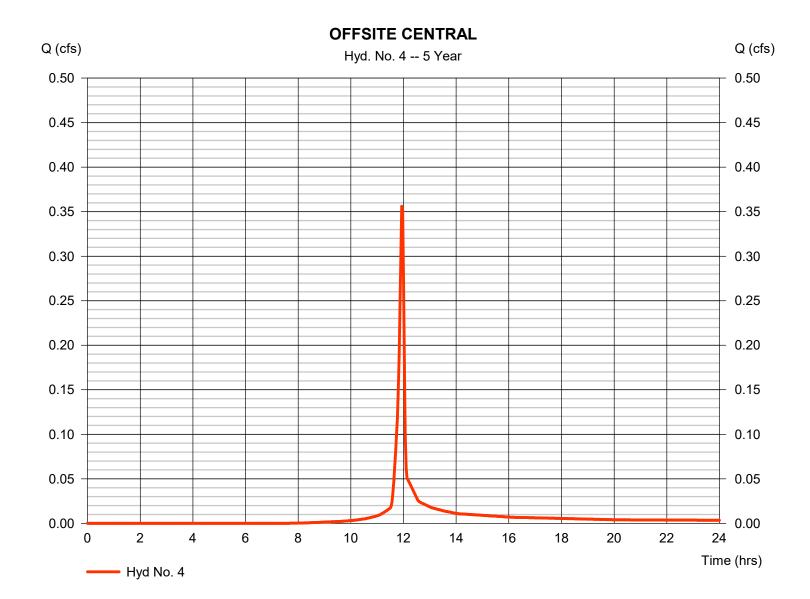
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Monday, 09 / 27 / 2021

Hyd. No. 4

OFFSITE CENTRAL

Hydrograph type = SCS Runoff Peak discharge = 0.356 cfsStorm frequency = 5 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 722 cuft Drainage area Curve number = 0.100 ac= 83 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.81 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



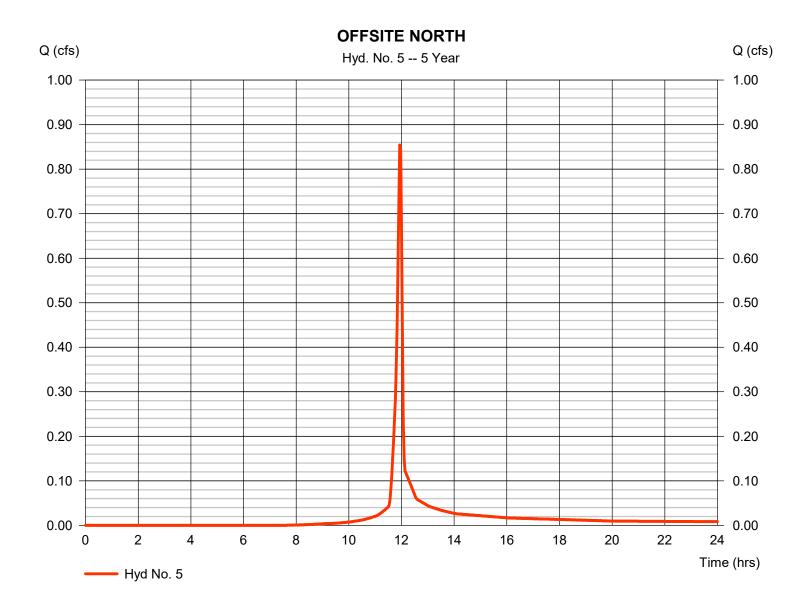
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Hyd. No. 5

OFFSITE NORTH

Hydrograph type = SCS Runoff Peak discharge = 0.854 cfsStorm frequency = 5 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 1,733 cuftDrainage area = 0.240 acCurve number = 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.81 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



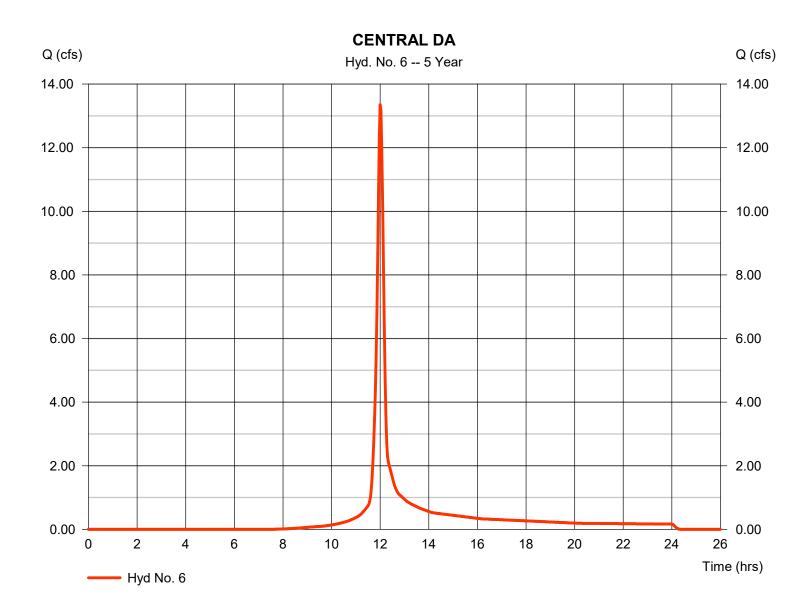
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Monday, 09 / 27 / 2021

Hyd. No. 6

CENTRAL DA

Hydrograph type = SCS Runoff Peak discharge = 13.36 cfsStorm frequency = 5 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 34,636 cuft Drainage area = 4.360 acCurve number = 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 3.81 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



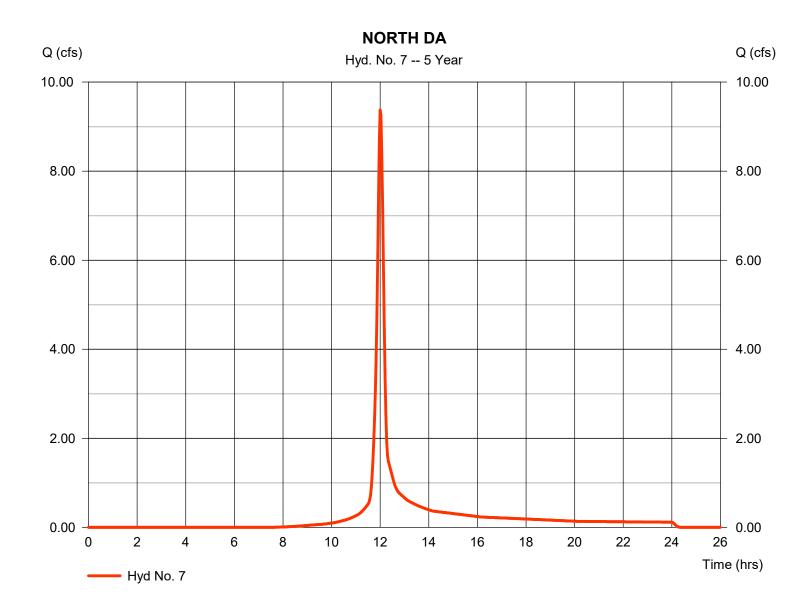
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Monday, 09 / 27 / 2021

Hyd. No. 7

NORTH DA

Hydrograph type = SCS Runoff Peak discharge = 9.373 cfsStorm frequency = 5 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 24,309 cuftDrainage area = 3.060 acCurve number = 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 3.81 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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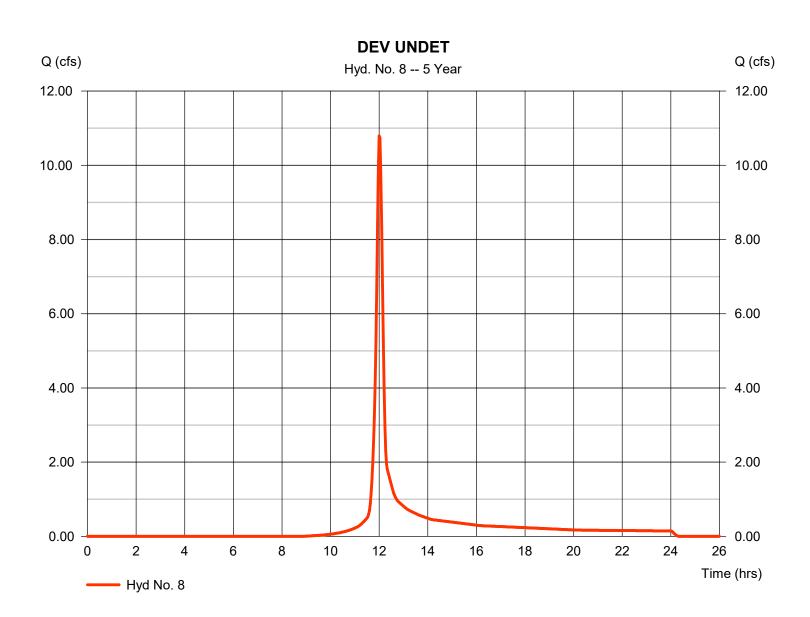
Monday, 09 / 27 / 2021

Hyd. No. 8

DEV UNDET

Hydrograph type = SCS Runoff Peak discharge = 10.79 cfsStorm frequency = 5 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 28,057 cuftDrainage area = 4.140 ac Curve number = 79* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 3.81 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(2.460 x 79) + (1.680 x 80)] / 4.140



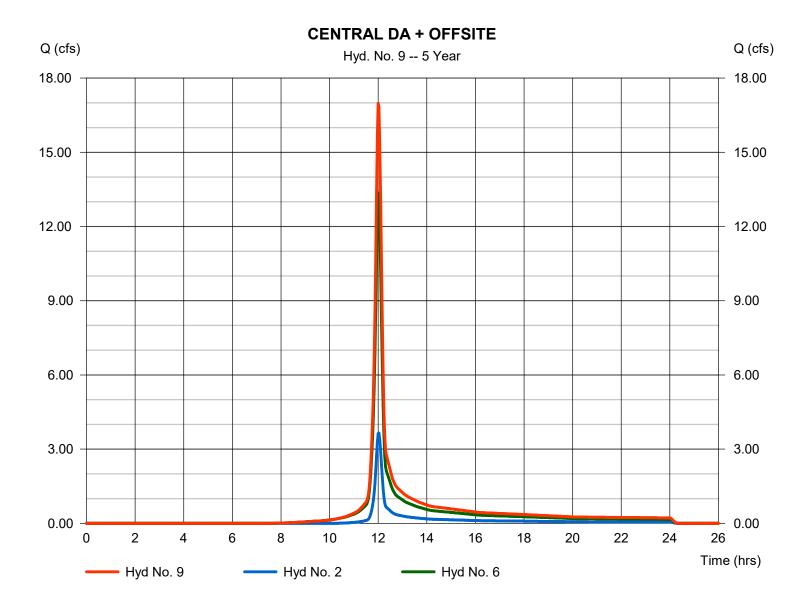
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Monday, 09 / 27 / 2021

Hyd. No. 9

CENTRAL DA + OFFSITE

Hydrograph type = Combine Peak discharge = 16.98 cfsStorm frequency Time to peak = 5 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 44,244 cuft Inflow hyds. = 2,6 Contrib. drain. area = 6.120 ac



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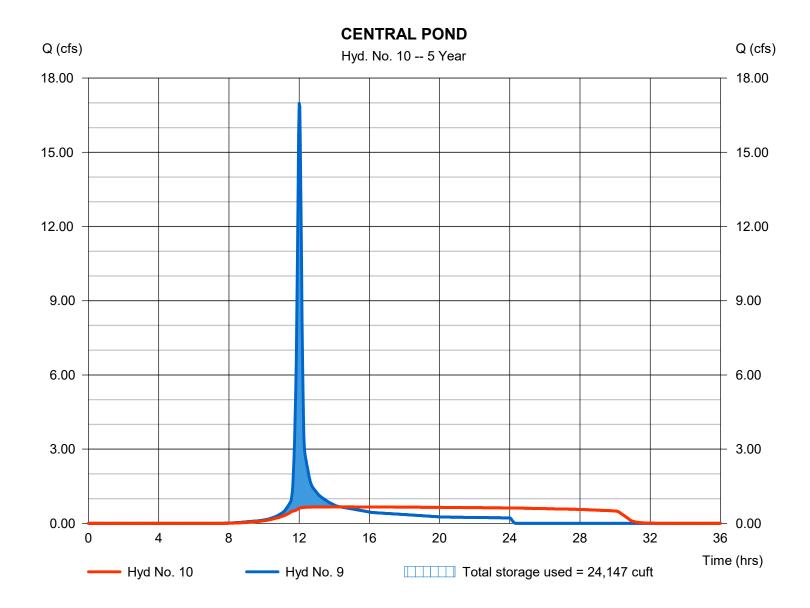
Monday, 09 / 27 / 2021

Hyd. No. 10

CENTRAL POND

Hydrograph type = Reservoir Peak discharge = 0.665 cfsStorm frequency = 5 yrsTime to peak $= 14.33 \, hrs$ Time interval = 2 min Hyd. volume = 44,242 cuft Inflow hyd. No. = 9 - CENTRAL DA + OFFSITE Max. Elevation = 949.72 ft= CENTRAL POND Reservoir name Max. Storage = 24,147 cuft

Storage Indication method used.



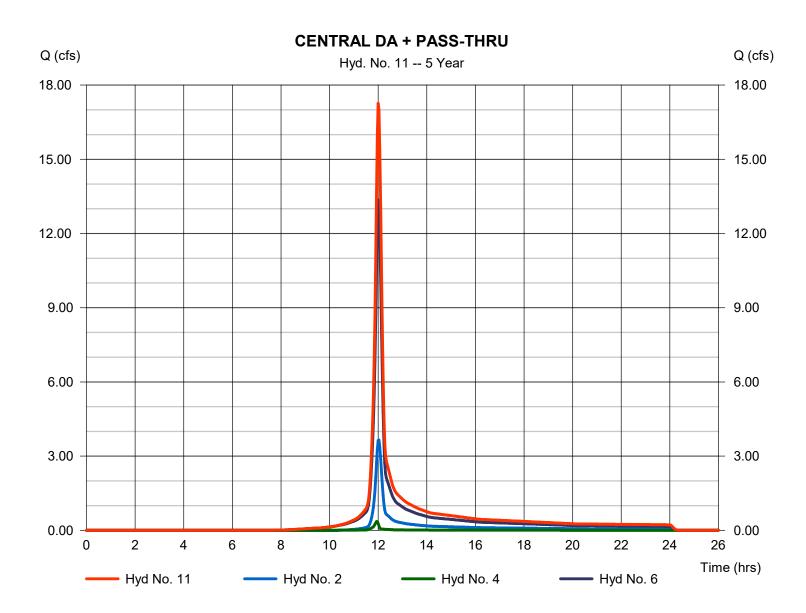
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Monday, 09 / 27 / 2021

Hyd. No. 11

CENTRAL DA + PASS-THRU

= 17.26 cfsHydrograph type = Combine Peak discharge Storm frequency = 5 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 44,966 cuft Inflow hyds. = 2, 4, 6Contrib. drain. area = 6.220 ac



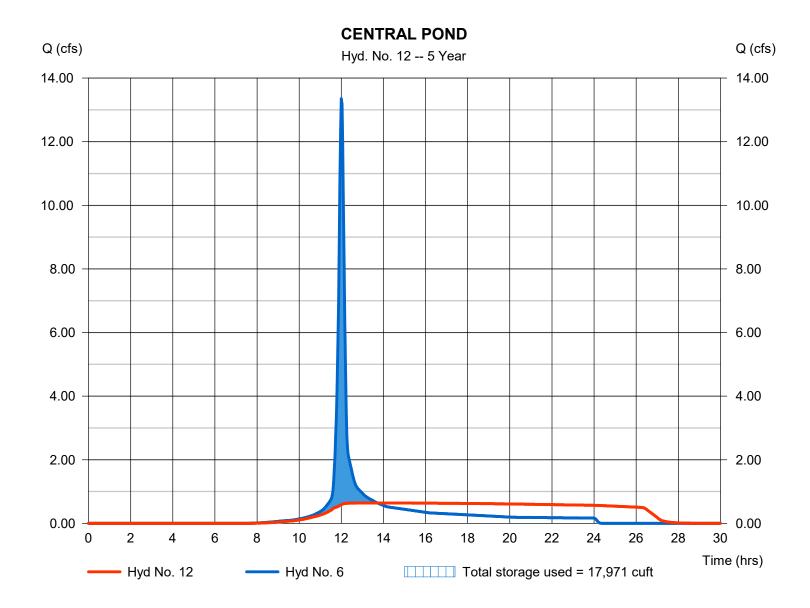
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Monday, 09 / 27 / 2021

Hyd. No. 12

CENTRAL POND

Hydrograph type Peak discharge = 0.641 cfs= Reservoir Storm frequency = 5 yrsTime to peak $= 13.70 \, hrs$ Time interval = 2 min Hyd. volume = 34,634 cuft Inflow hyd. No. Max. Elevation = 6 - CENTRAL DA = 948.77 ft = CENTRAL POND Reservoir name Max. Storage = 17,971 cuft



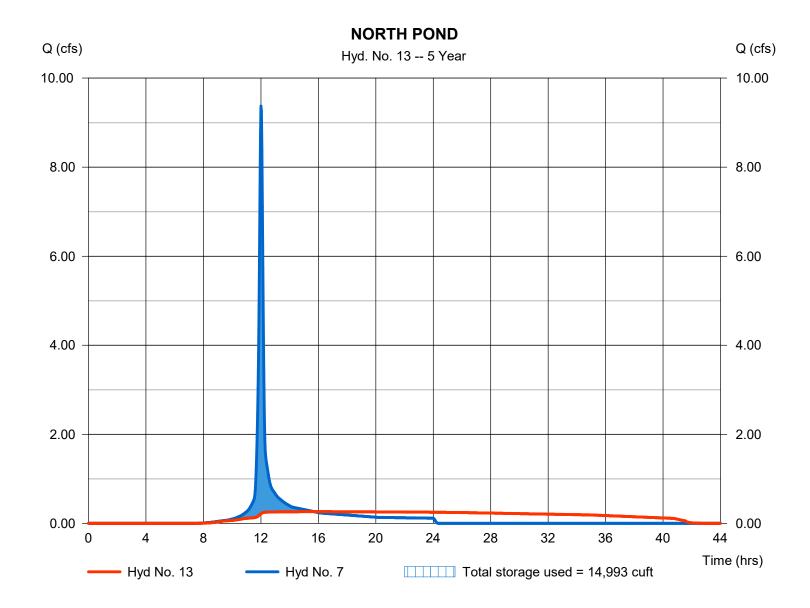
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Monday, 09 / 27 / 2021

Hyd. No. 13

NORTH POND

Hydrograph type = Reservoir Peak discharge = 0.262 cfsStorm frequency = 5 yrsTime to peak $= 15.70 \, hrs$ Time interval = 2 min Hyd. volume = 24,307 cuftInflow hyd. No. = 7 - NORTH DA Max. Elevation $= 940.80 \, \text{ft}$ = NORTH POND Reservoir name Max. Storage = 14,993 cuft



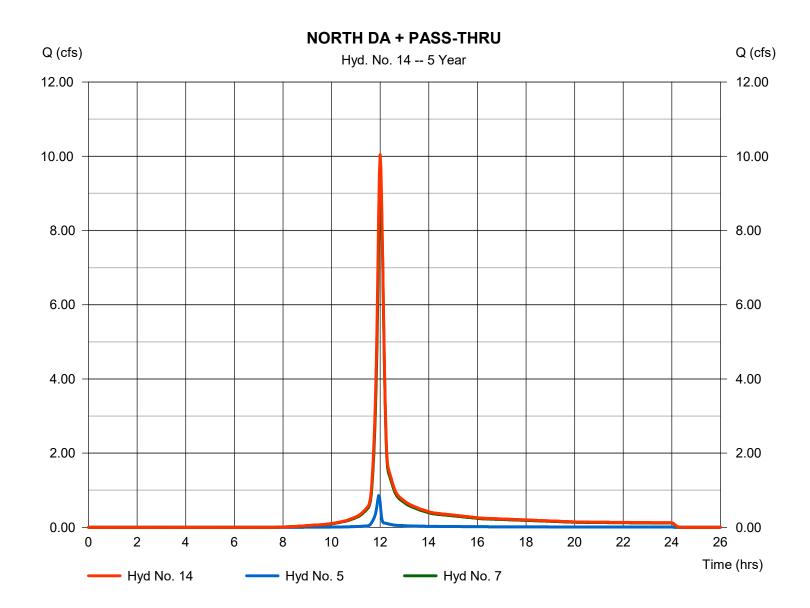
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Monday, 09 / 27 / 2021

Hyd. No. 14

NORTH DA + PASS-THRU

Hydrograph type = Combine Peak discharge = 10.05 cfsStorm frequency Time to peak = 5 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 26,042 cuft Inflow hyds. = 5, 7Contrib. drain. area = 3.300 ac



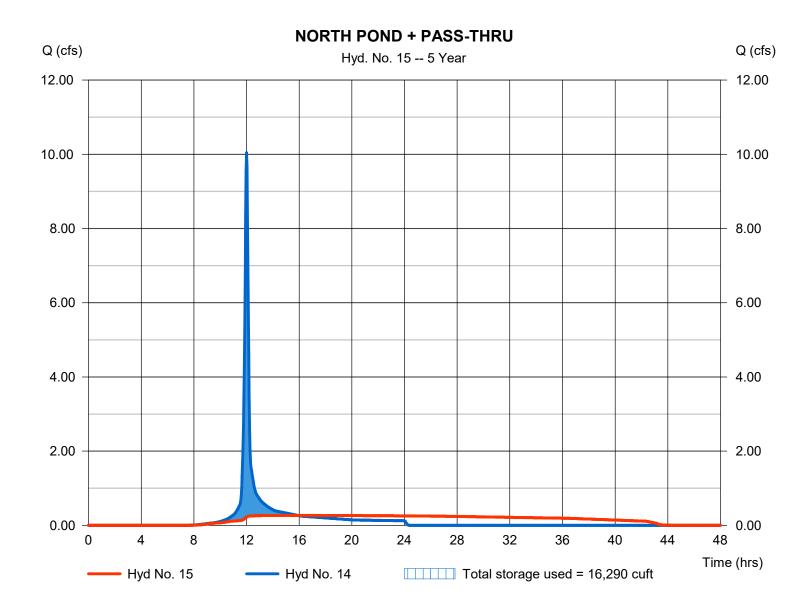
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Monday, 09 / 27 / 2021

Hyd. No. 15

NORTH POND + PASS-THRU

Hydrograph type Peak discharge = 0.267 cfs= Reservoir Storm frequency = 5 yrsTime to peak $= 15.90 \, hrs$ Time interval = 2 min Hyd. volume = 26,040 cuftInflow hyd. No. = 14 - NORTH DA + PASS-THR Max. Elevation = 941.03 ft= NORTH POND = 16,290 cuft Reservoir name Max. Storage



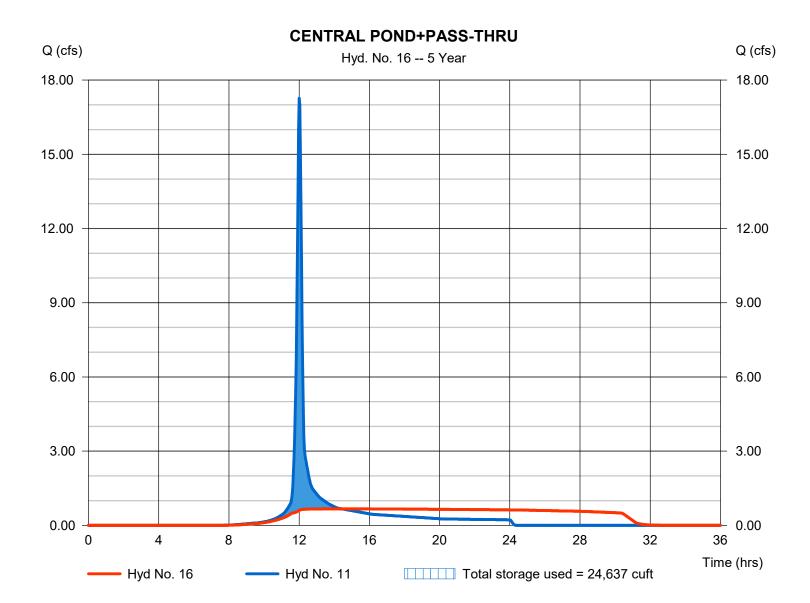
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Hyd. No. 16

CENTRAL POND+PASS-THRU

Hydrograph type Peak discharge = 0.667 cfs= Reservoir Storm frequency = 5 yrsTime to peak $= 14.43 \, hrs$ Time interval = 2 min Hyd. volume = 44,965 cuft Inflow hyd. No. = 11 - CENTRAL DA + PASS-THARAUX. Elevation = 949.80 ft= CENTRAL POND Reservoir name Max. Storage = 24,637 cuft



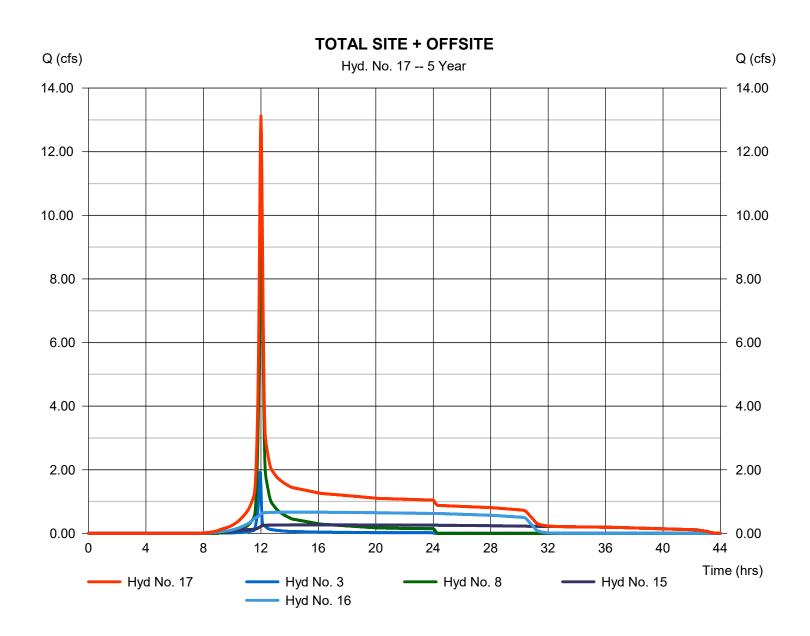
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Monday, 09 / 27 / 2021

Hyd. No. 17

TOTAL SITE + OFFSITE

Hydrograph type = Combine Peak discharge = 13.13 cfsStorm frequency = 5 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 102,962 cuft Inflow hyds. = 3, 8, 15, 16 Contrib. drain. area = 4.680 ac



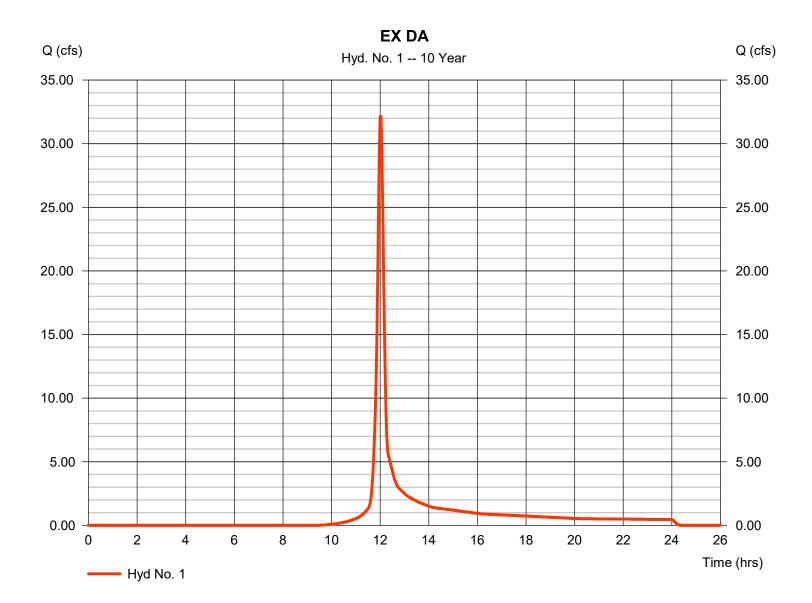
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Monday, 09 / 27 / 2021

Hyd. No. 1

EX DA

Hydrograph type = SCS Runoff Peak discharge = 32.15 cfsStorm frequency = 10 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 84,023 cuft Drainage area = 11.560 ac Curve number = 74 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) = 12.60 min = User Total precip. = 4.46 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



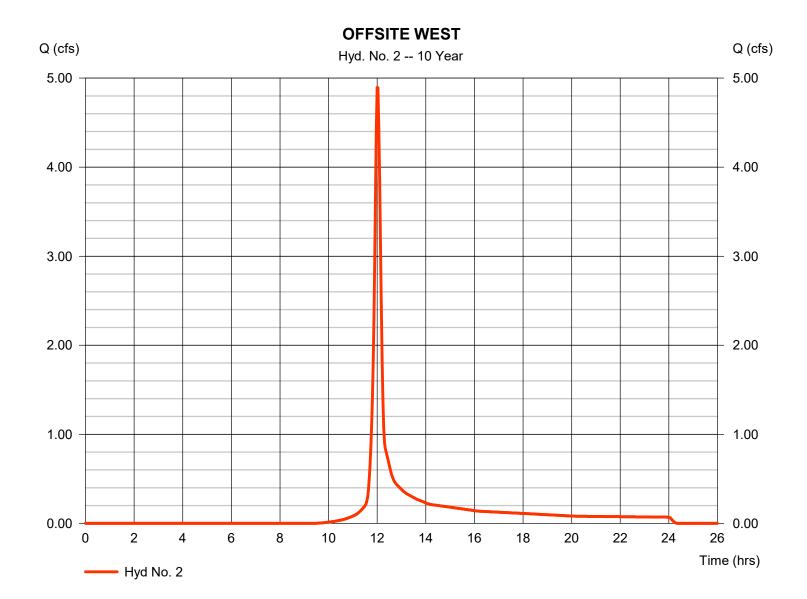
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Monday, 09 / 27 / 2021

Hyd. No. 2

OFFSITE WEST

Hydrograph type = SCS Runoff Peak discharge = 4.895 cfsStorm frequency = 10 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 12,792 cuft Drainage area = 1.760 acCurve number = 74 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 10.10 min = User Total precip. = 4.46 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



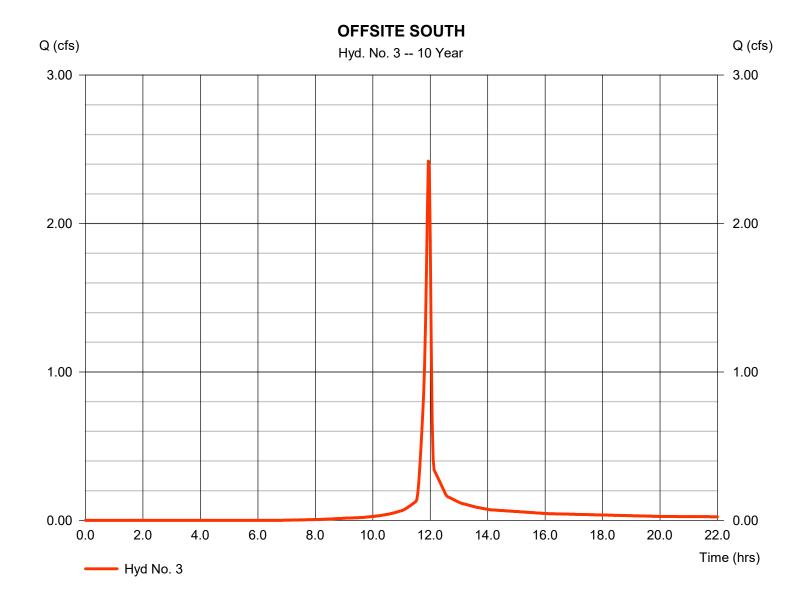
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Monday, 09 / 27 / 2021

Hyd. No. 3

OFFSITE SOUTH

= SCS Runoff Hydrograph type Peak discharge = 2.421 cfsStorm frequency = 10 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 4,943 cuft Drainage area Curve number = 0.540 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 4.46 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



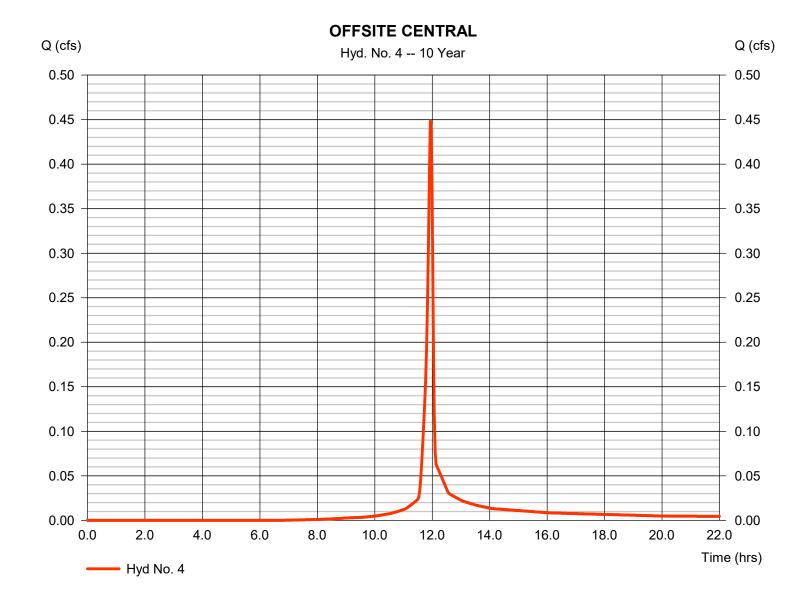
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Hyd. No. 4

OFFSITE CENTRAL

Hydrograph type = SCS Runoff Peak discharge = 0.448 cfsStorm frequency = 10 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 915 cuft Drainage area Curve number = 0.100 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 4.46 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



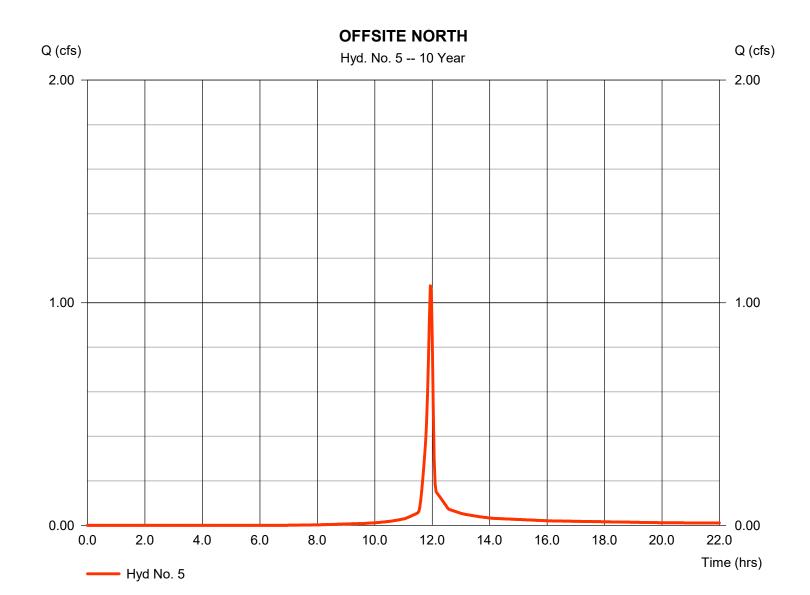
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Monday, 09 / 27 / 2021

Hyd. No. 5

OFFSITE NORTH

= SCS Runoff Hydrograph type Peak discharge = 1.076 cfsStorm frequency = 10 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 2,197 cuftDrainage area = 0.240 acCurve number = 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 4.46 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



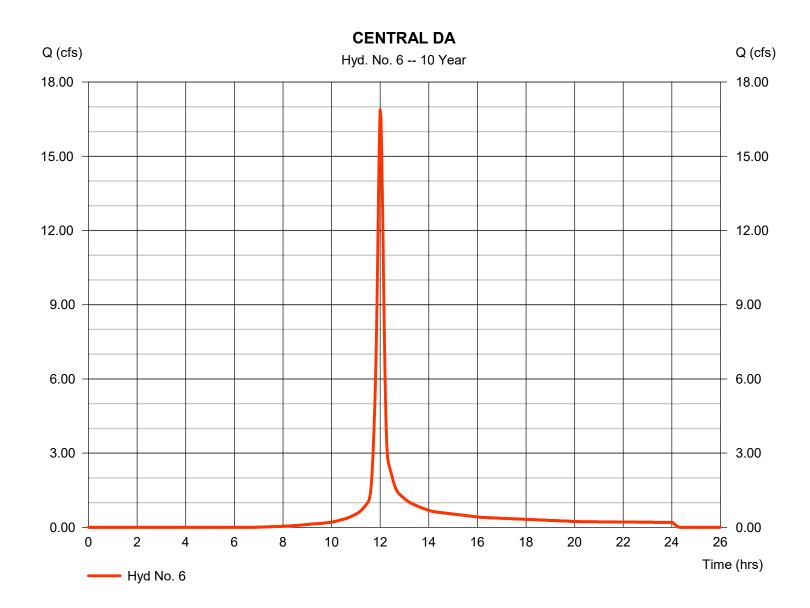
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Monday, 09 / 27 / 2021

Hyd. No. 6

CENTRAL DA

Hydrograph type = SCS Runoff Peak discharge = 16.88 cfsStorm frequency = 10 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 43,905 cuft Drainage area = 4.360 acCurve number = 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.00 min = User Total precip. = 4.46 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



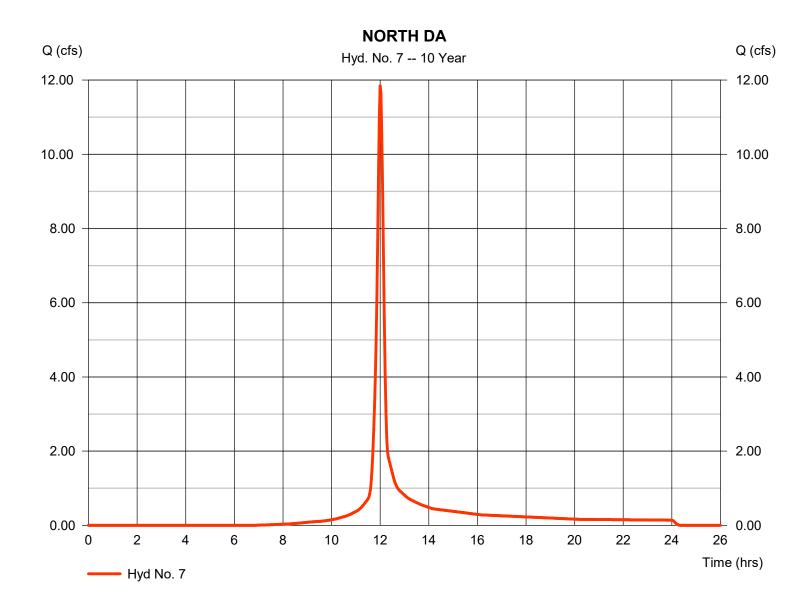
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Monday, 09 / 27 / 2021

Hyd. No. 7

NORTH DA

Hydrograph type = SCS Runoff Peak discharge = 11.85 cfsStorm frequency = 10 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 30,814 cuftDrainage area = 3.060 acCurve number = 83 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 10.00 min = User Total precip. = 4.46 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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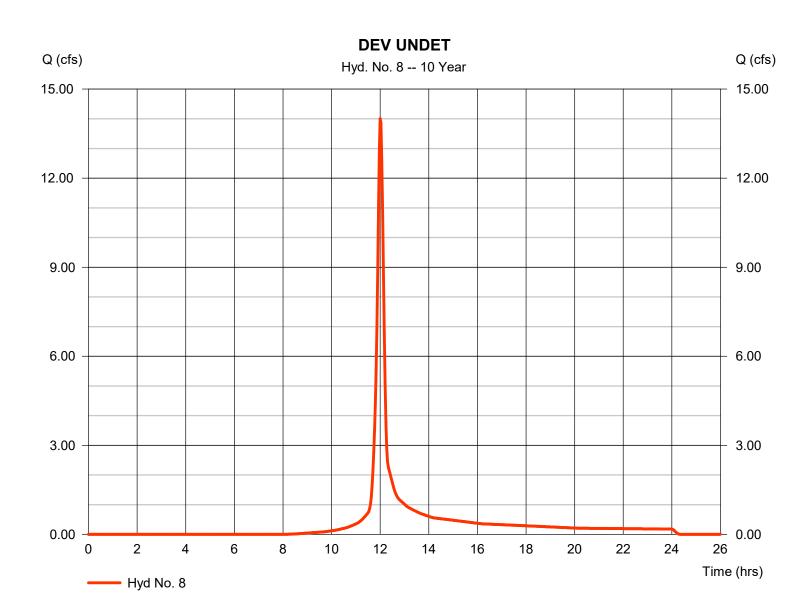
Monday, 09 / 27 / 2021

Hyd. No. 8

DEV UNDET

Hydrograph type = SCS Runoff Peak discharge = 14.01 cfsStorm frequency = 10 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 36,310 cuftDrainage area = 4.140 acCurve number = 79* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.00 min = User Total precip. = 4.46 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(2.460 x 79) + (1.680 x 80)] / 4.140



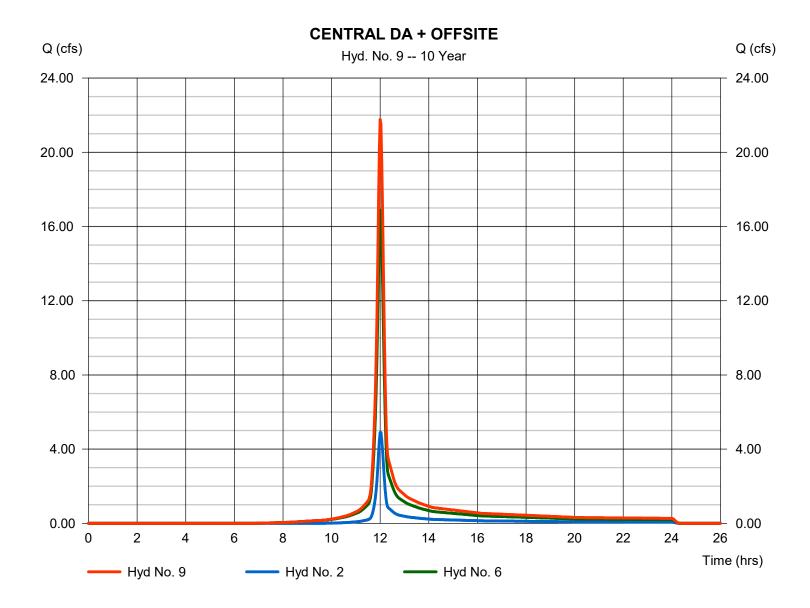
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Hyd. No. 9

CENTRAL DA + OFFSITE

Hydrograph type = Combine Peak discharge = 21.77 cfsStorm frequency Time to peak = 10 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 56,698 cuft Inflow hyds. = 2,6 Contrib. drain. area = 6.120 ac



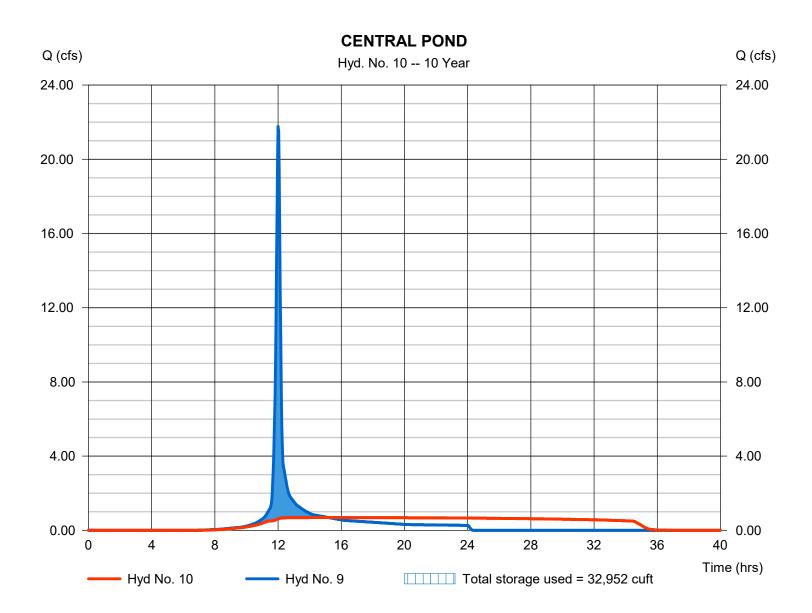
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Hyd. No. 10

CENTRAL POND

Hydrograph type Peak discharge = 0.688 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 15.20 \, hrs$ Time interval = 2 min Hyd. volume = 56,696 cuft Inflow hyd. No. = 9 - CENTRAL DA + OFFSITE Max. Elevation = 950.68 ft= CENTRAL POND Reservoir name Max. Storage = 32,952 cuft



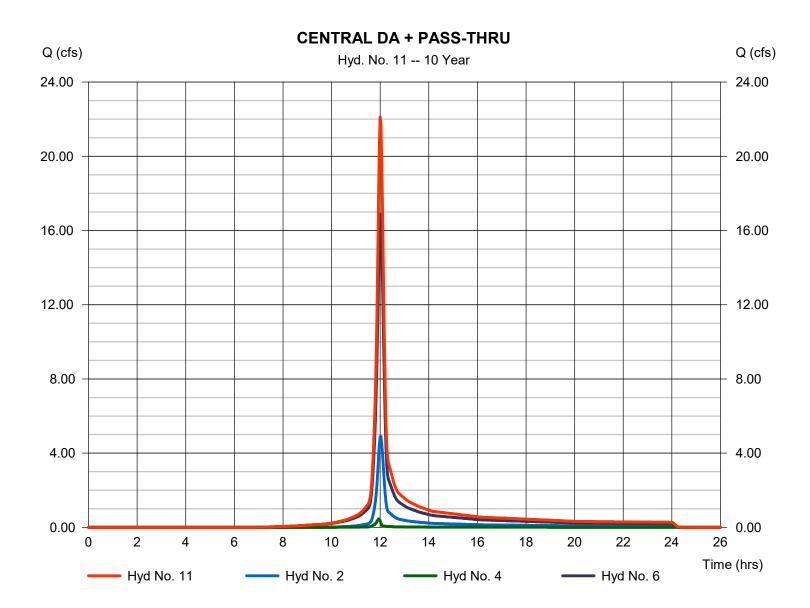
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Hyd. No. 11

CENTRAL DA + PASS-THRU

Hydrograph type = Combine Peak discharge = 22.12 cfsStorm frequency Time to peak = 10 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 57,613 cuftInflow hyds. = 2, 4, 6Contrib. drain. area = 6.220 ac



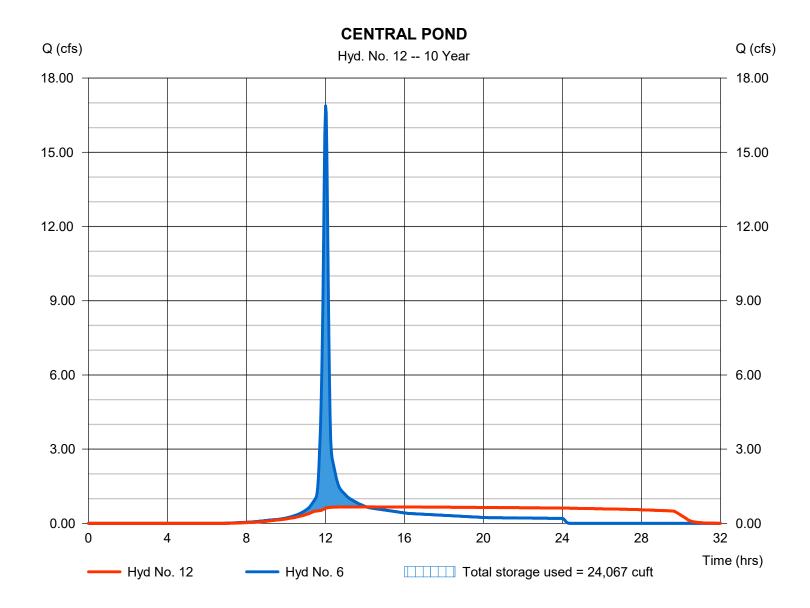
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Hyd. No. 12

CENTRAL POND

Hydrograph type Peak discharge = 0.664 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 14.07 \, hrs$ Time interval = 2 min Hyd. volume = 43,904 cuft Inflow hyd. No. Max. Elevation = 6 - CENTRAL DA $= 949.71 \, \text{ft}$ = CENTRAL POND Reservoir name Max. Storage = 24,067 cuft



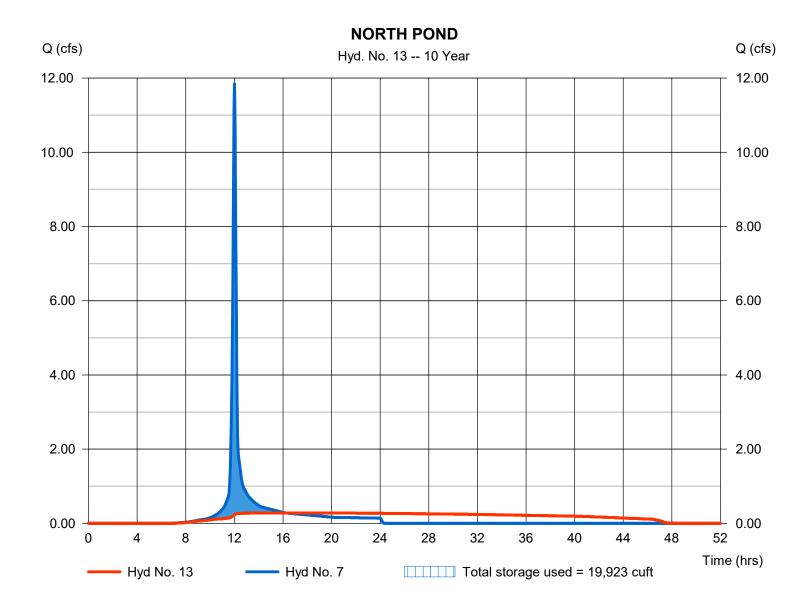
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Hyd. No. 13

NORTH POND

Hydrograph type Peak discharge = 0.281 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 16.23 \, hrs$ Time interval = 2 min Hyd. volume = 30,813 cuftInflow hyd. No. = 7 - NORTH DA Max. Elevation = 941.68 ft= NORTH POND Reservoir name Max. Storage = 19,923 cuft



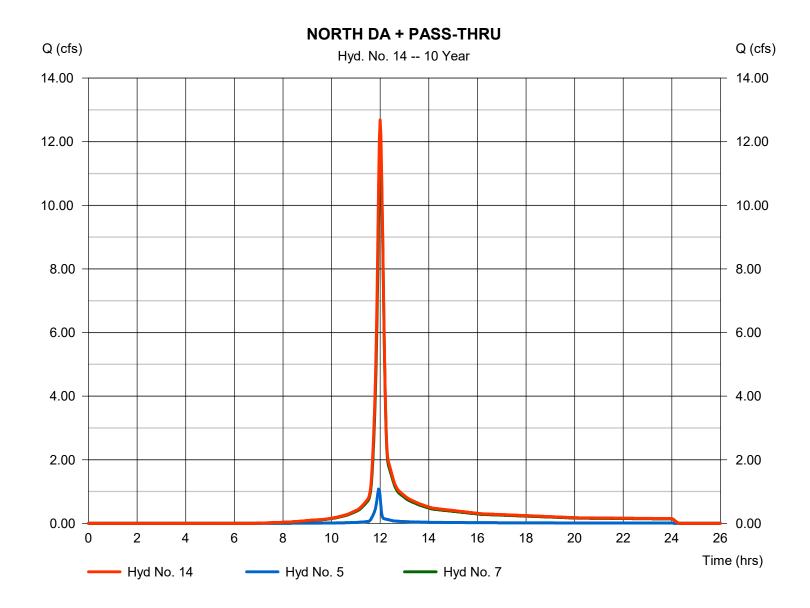
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Hyd. No. 14

NORTH DA + PASS-THRU

Hydrograph type = Combine Peak discharge = 12.68 cfsStorm frequency = 10 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 33,011 cuft Inflow hyds. = 5, 7 Contrib. drain. area = 3.300 ac



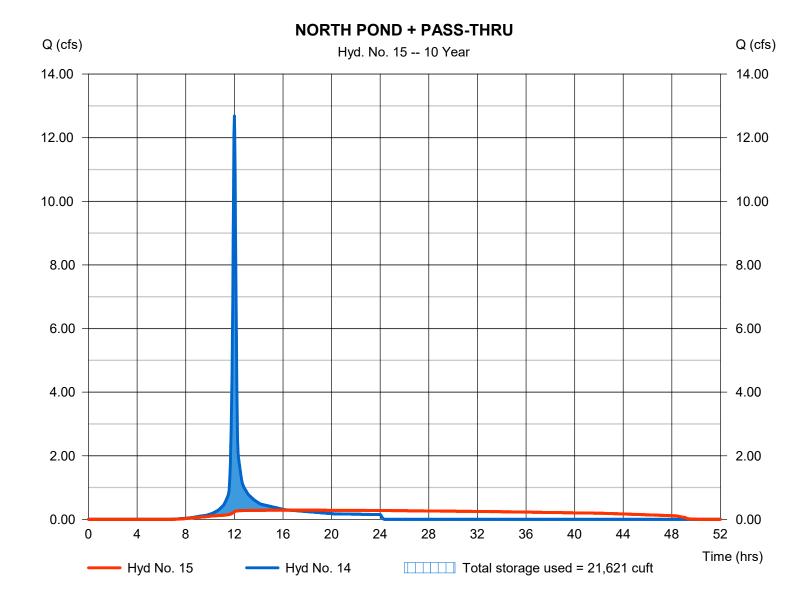
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Hyd. No. 15

NORTH POND + PASS-THRU

Hydrograph type Peak discharge = 0.287 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 16.63 \, hrs$ Time interval = 2 min Hyd. volume = 33,010 cuftInflow hyd. No. = 14 - NORTH DA + PASS-THR Max. Elevation = 941.98 ft= NORTH POND Reservoir name Max. Storage = 21,621 cuft



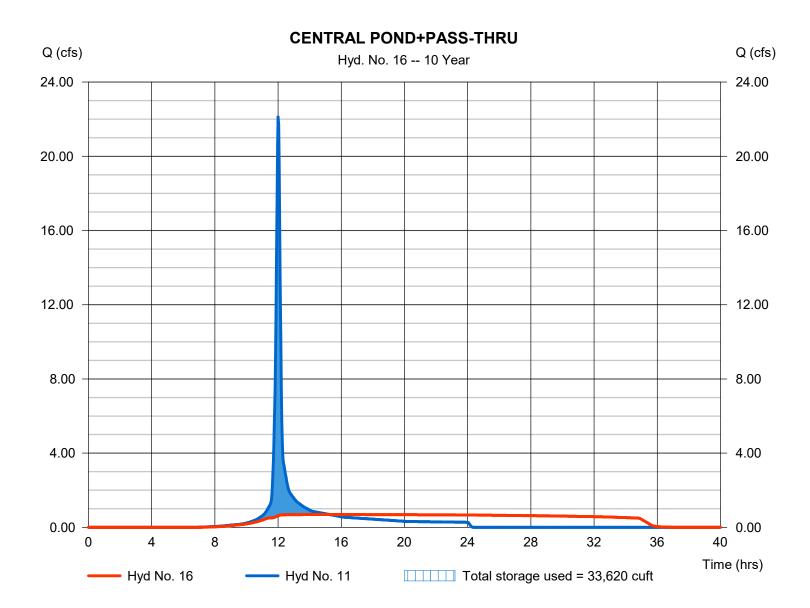
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Hyd. No. 16

CENTRAL POND+PASS-THRU

Hydrograph type Peak discharge = 0.690 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 15.27 \, hrs$ Time interval = 2 min Hyd. volume = 57,612 cuftInflow hyd. No. = 11 - CENTRAL DA + PASS-THARAUX. Elevation = 950.75 ft= CENTRAL POND Reservoir name Max. Storage = 33,620 cuft



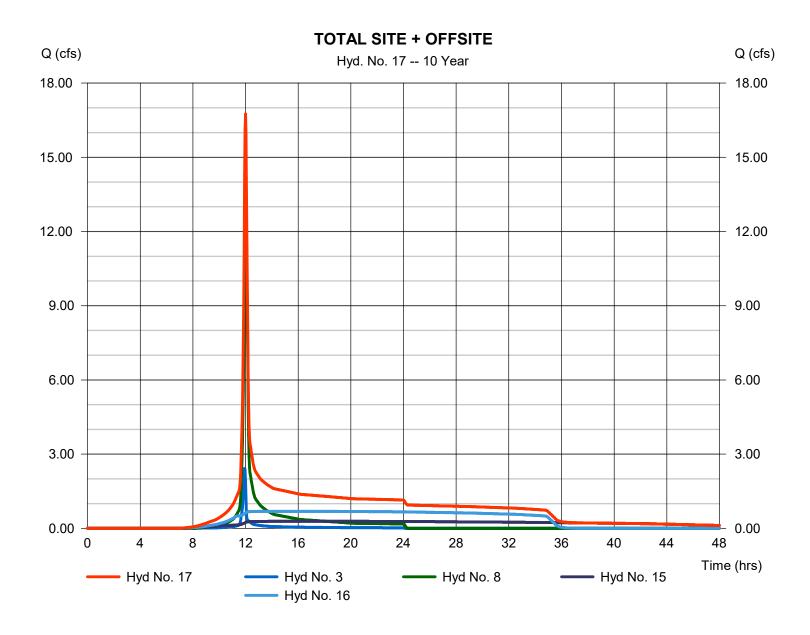
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Hyd. No. 17

TOTAL SITE + OFFSITE

Hydrograph type = Combine Peak discharge = 16.76 cfsStorm frequency Time to peak = 10 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 131,876 cuft Inflow hyds. = 3, 8, 15, 16 Contrib. drain. area = 4.680 ac



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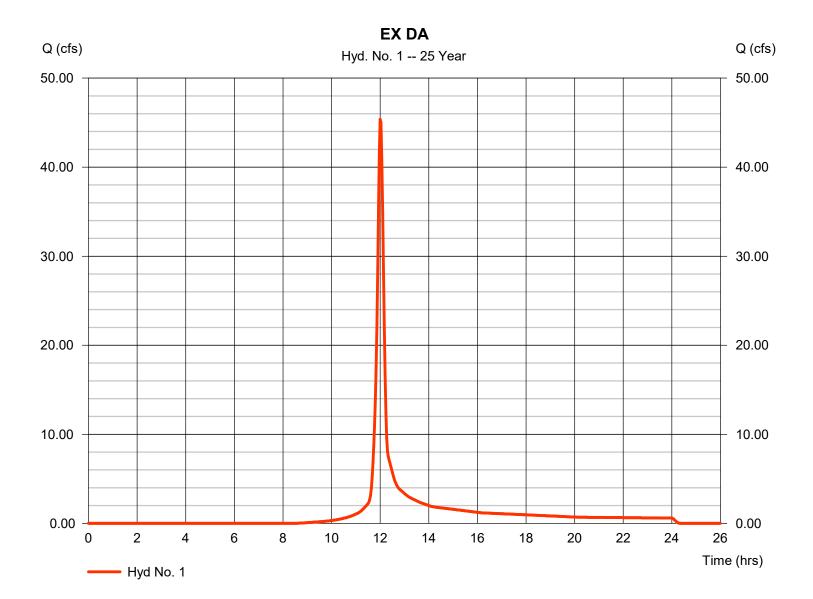
Monday, 09 / 27 / 2021

Hyd. No. 1

EX DA

Hydrograph type = SCS Runoff Peak discharge = 45.37 cfsStorm frequency = 25 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 117,704 cuft Drainage area = 11.560 ac Curve number = 74 = 0 ftBasin Slope = 0.0 %Hydraulic length

Tc method = User Time of conc. (Tc) = 12.60 min
Total precip. = 5.44 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



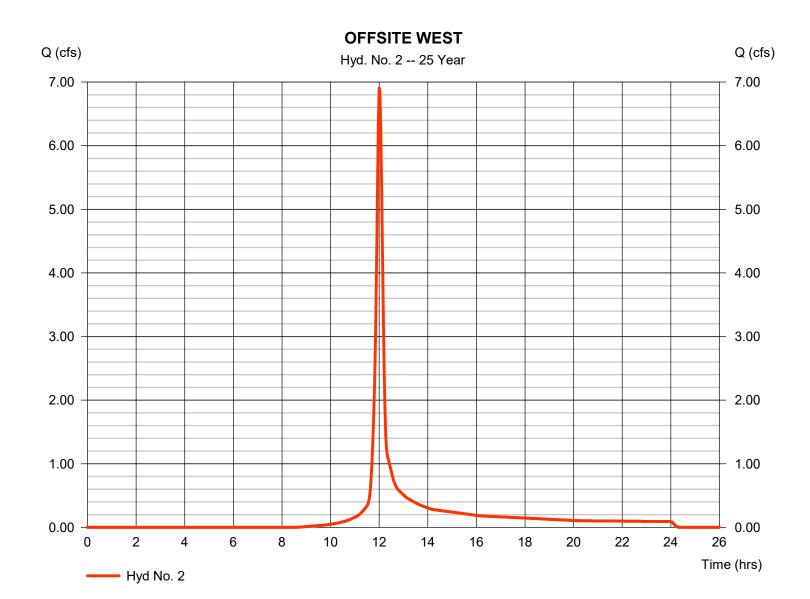
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Hyd. No. 2

OFFSITE WEST

Hydrograph type = SCS Runoff Peak discharge = 6.907 cfsStorm frequency = 25 yrs Time to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 17,920 cuftDrainage area = 1.760 acCurve number = 74 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 10.10 min = User Total precip. = 5.44 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



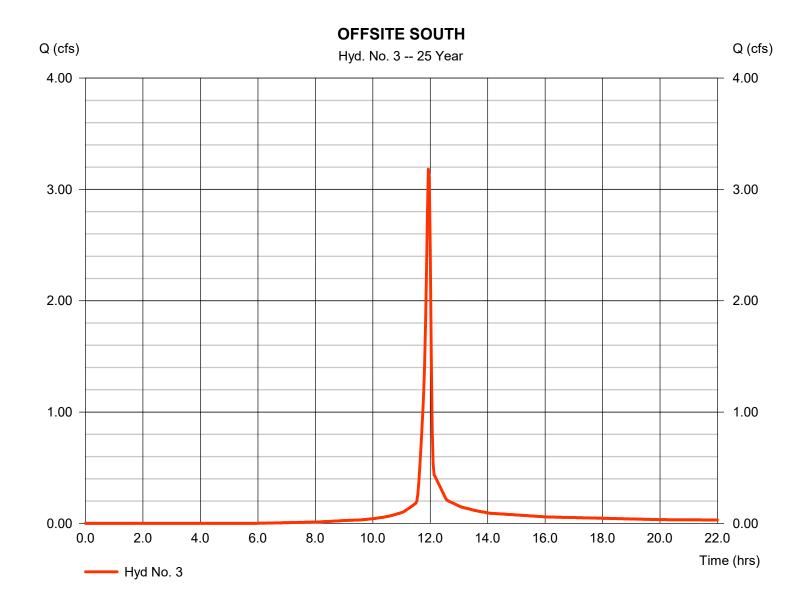
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Hyd. No. 3

OFFSITE SOUTH

= SCS Runoff Hydrograph type Peak discharge = 3.181 cfsStorm frequency = 25 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 6,569 cuftDrainage area = 0.540 acCurve number = 83 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.44 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



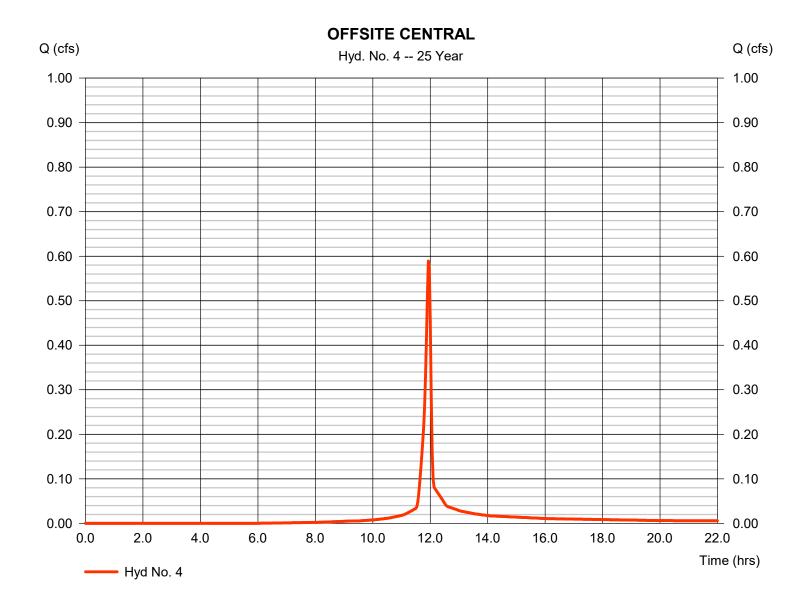
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Hyd. No. 4

OFFSITE CENTRAL

Hydrograph type = SCS Runoff Peak discharge = 0.589 cfsStorm frequency = 25 yrs Time to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 1.217 cuft Drainage area Curve number = 0.100 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.44 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



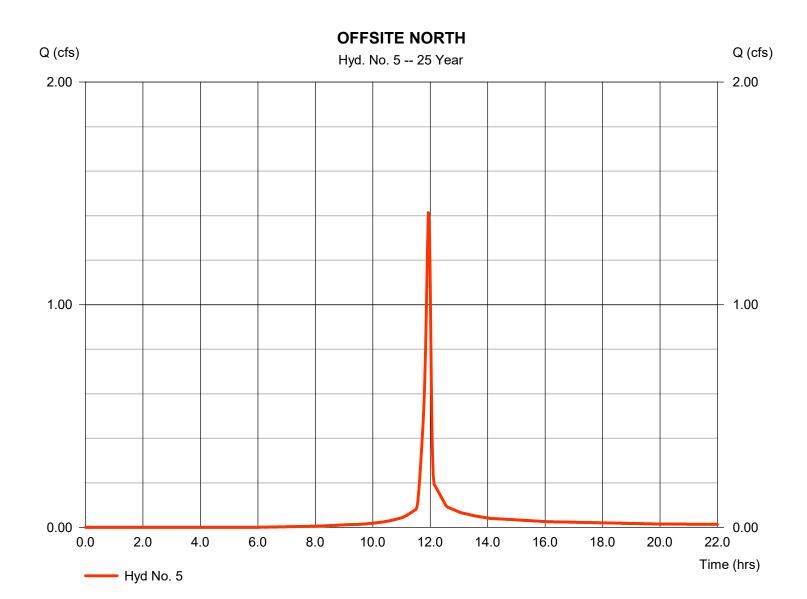
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Monday, 09 / 27 / 2021

Hyd. No. 5

OFFSITE NORTH

= SCS Runoff Hydrograph type Peak discharge = 1.414 cfsStorm frequency = 25 yrs Time to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 2,920 cuftDrainage area = 0.240 acCurve number = 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.44 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



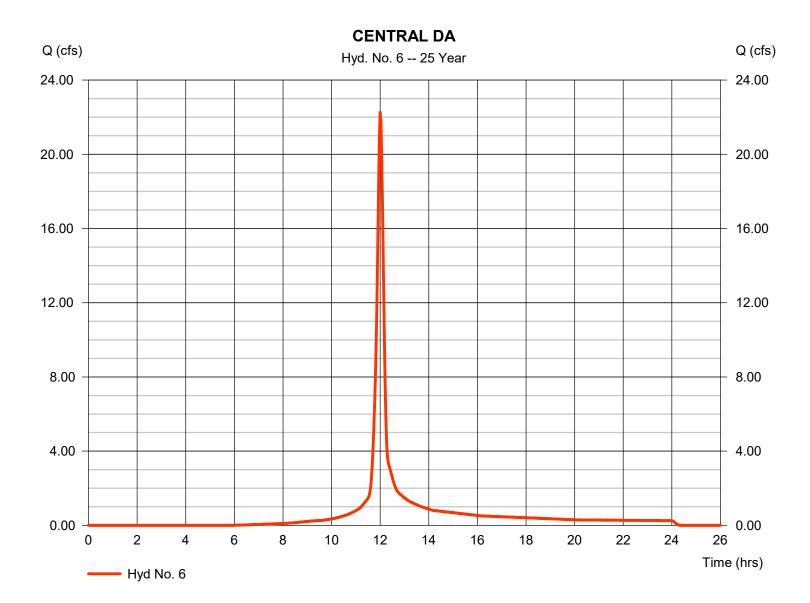
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Monday, 09 / 27 / 2021

Hyd. No. 6

CENTRAL DA

= 22.27 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency = 25 yrs Time to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 58,346 cuft Drainage area = 4.360 acCurve number = 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.00 min = User Total precip. = 5.44 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



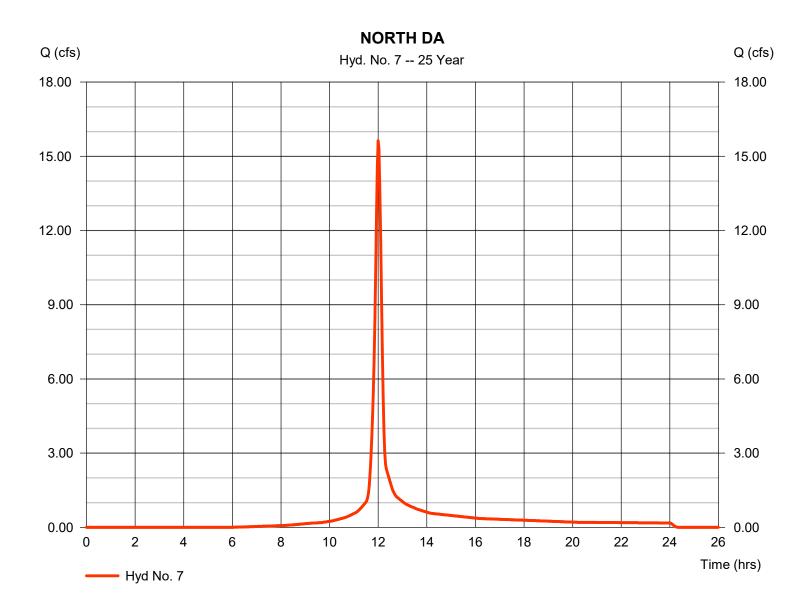
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Hyd. No. 7

NORTH DA

Hydrograph type = SCS Runoff Peak discharge = 15.63 cfsStorm frequency = 25 yrs Time to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 40,949 cuftDrainage area = 3.060 acCurve number = 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.00 min = User Total precip. = 5.44 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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Hyd. No. 8

DEV UNDET

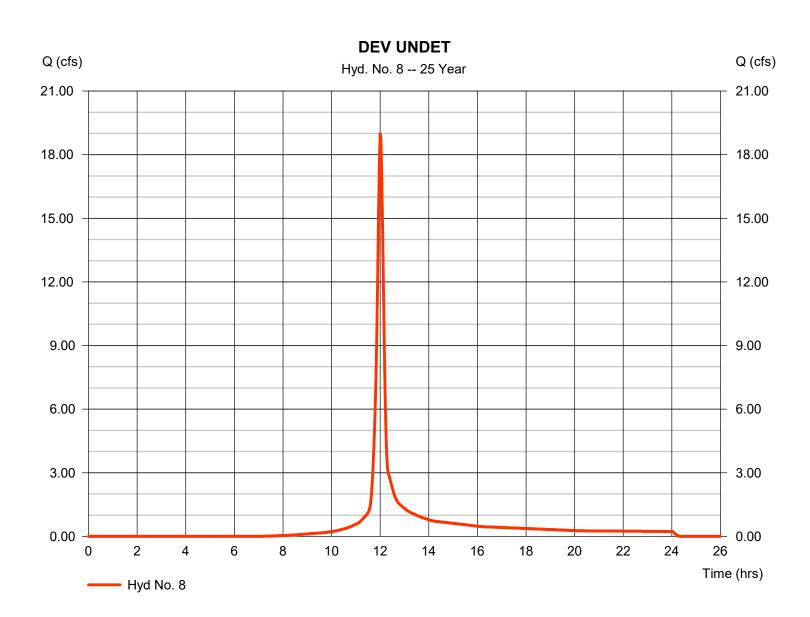
Hydrograph type = SCS Runoff Peak discharge = 19.00 cfsStorm frequency = 25 yrs Time to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 49,345 cuftDrainage area = 4.140 acCurve number = 79* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.00 min = User

Tc method = User Time of conc. (Tc) = 10.00 mir

Total precip. = 5.44 in Distribution = Type II

Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(2.460 x 79) + (1.680 x 80)] / 4.140



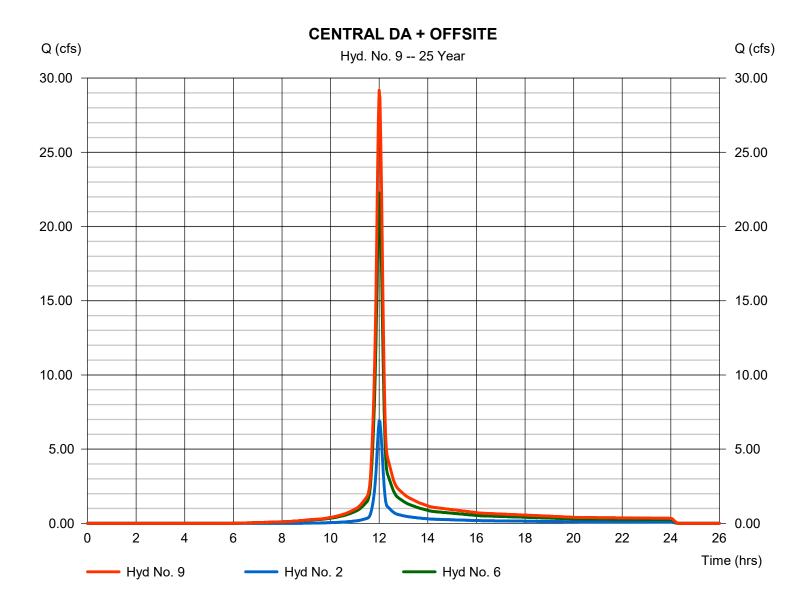
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Hyd. No. 9

CENTRAL DA + OFFSITE

Hydrograph type = Combine Peak discharge = 29.17 cfsStorm frequency = 25 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 76,266 cuft Inflow hyds. = 2,6 Contrib. drain. area = 6.120 ac



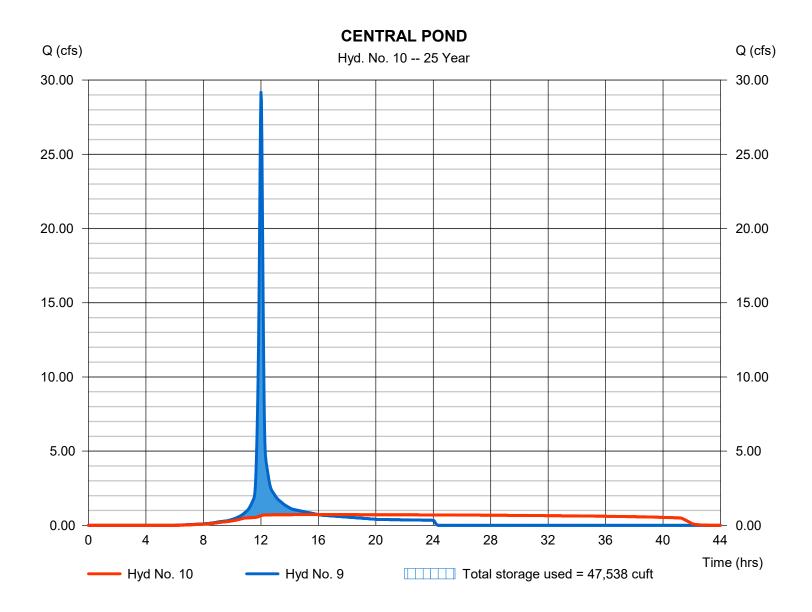
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Monday, 09 / 27 / 2021

Hyd. No. 10

CENTRAL POND

Hydrograph type = Reservoir Peak discharge = 0.721 cfsStorm frequency = 25 yrsTime to peak $= 16.00 \, hrs$ Time interval = 2 min Hyd. volume = 76,265 cuft Inflow hyd. No. = 9 - CENTRAL DA + OFFSITE Max. Elevation = 952.07 ft= CENTRAL POND Reservoir name Max. Storage = 47,538 cuft



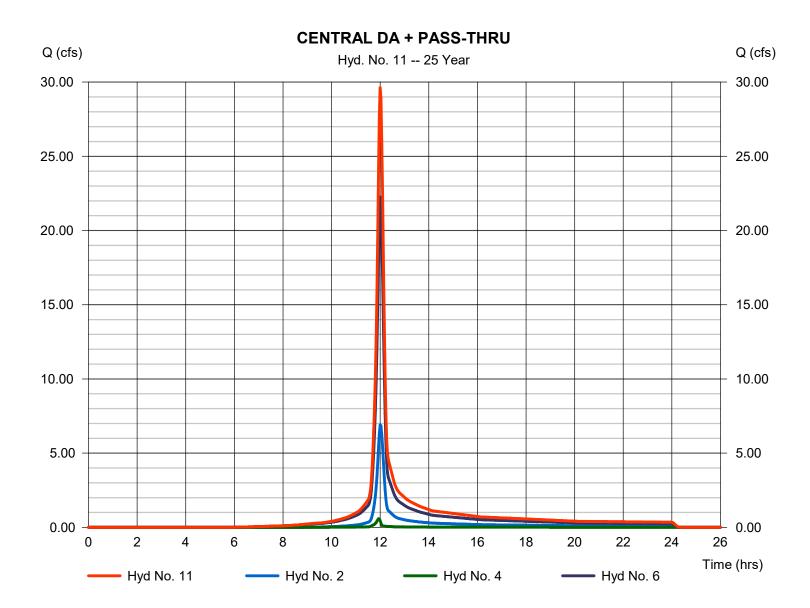
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Hyd. No. 11

CENTRAL DA + PASS-THRU

Hydrograph type = Combine Peak discharge = 29.63 cfsStorm frequency Time to peak = 25 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 77,483 cuft Inflow hyds. = 2, 4, 6Contrib. drain. area = 6.220 ac



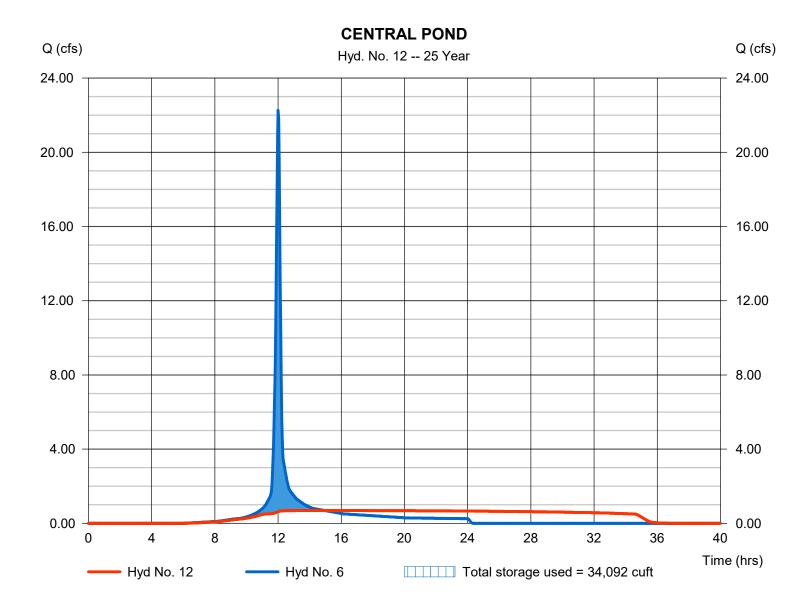
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Monday, 09 / 27 / 2021

Hyd. No. 12

CENTRAL POND

Hydrograph type = Reservoir Peak discharge = 0.691 cfsStorm frequency = 25 yrsTime to peak $= 14.97 \, hrs$ Time interval = 2 min Hyd. volume = 58,344 cuft Inflow hyd. No. Max. Elevation = 6 - CENTRAL DA = 950.79 ft= CENTRAL POND Reservoir name Max. Storage = 34,092 cuft



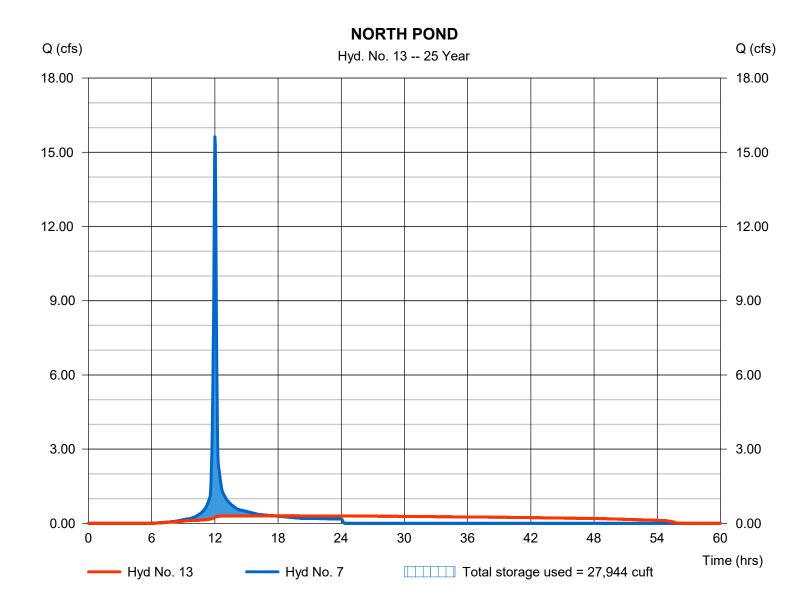
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Monday, 09 / 27 / 2021

Hyd. No. 13

NORTH POND

Hydrograph type = Reservoir Peak discharge = 0.303 cfsStorm frequency = 25 yrsTime to peak $= 17.60 \, hrs$ Time interval = 2 min Hyd. volume = 40,948 cuft Inflow hyd. No. = 7 - NORTH DA Max. Elevation = 942.79 ft= NORTH POND = 27,944 cuft Reservoir name Max. Storage



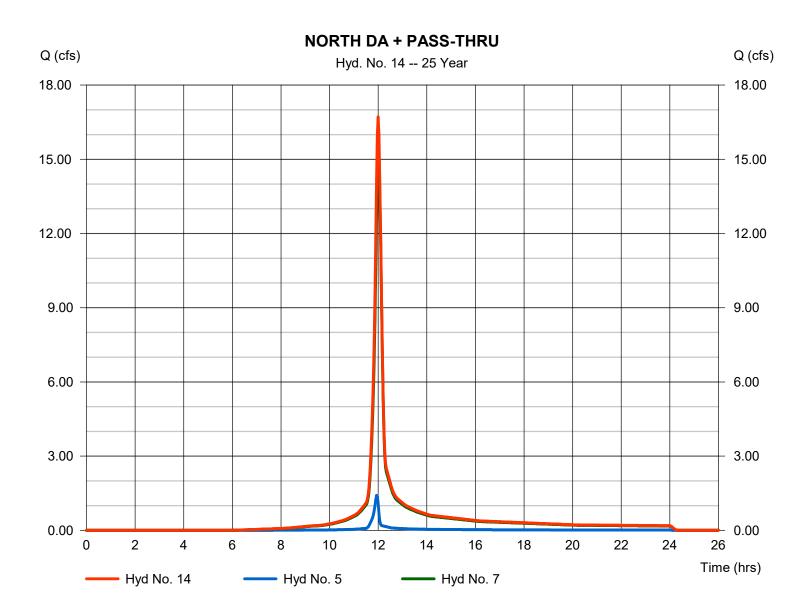
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Monday, 09 / 27 / 2021

Hyd. No. 14

NORTH DA + PASS-THRU

Hydrograph type = Combine Peak discharge = 16.72 cfsStorm frequency = 25 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 43,869 cuft Inflow hyds. = 3.300 ac= 5, 7 Contrib. drain. area



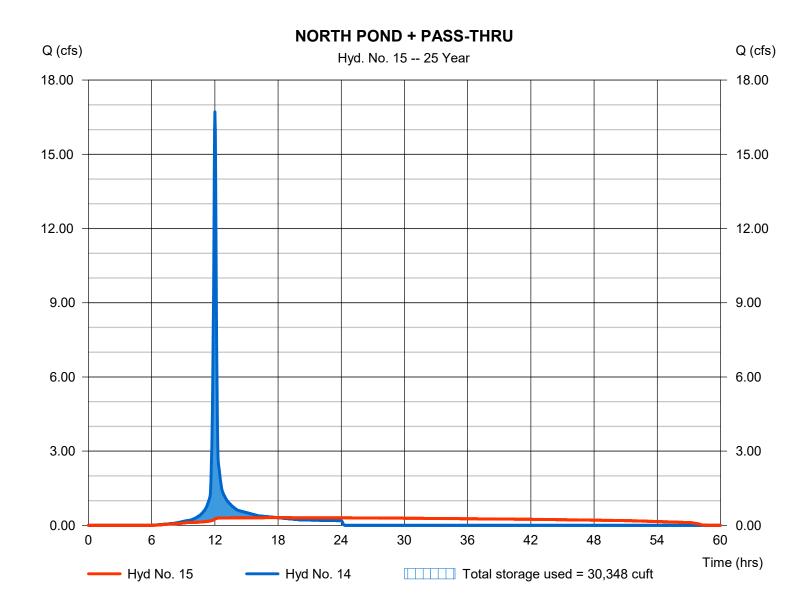
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Monday, 09 / 27 / 2021

Hyd. No. 15

NORTH POND + PASS-THRU

Hydrograph type Peak discharge = 0.309 cfs= Reservoir Storm frequency = 25 yrsTime to peak $= 17.97 \, hrs$ Time interval = 2 min Hyd. volume = 43.867 cuft Inflow hyd. No. = 14 - NORTH DA + PASS-THR Max. Elevation = 943.09 ft= NORTH POND Max. Storage Reservoir name = 30,348 cuft



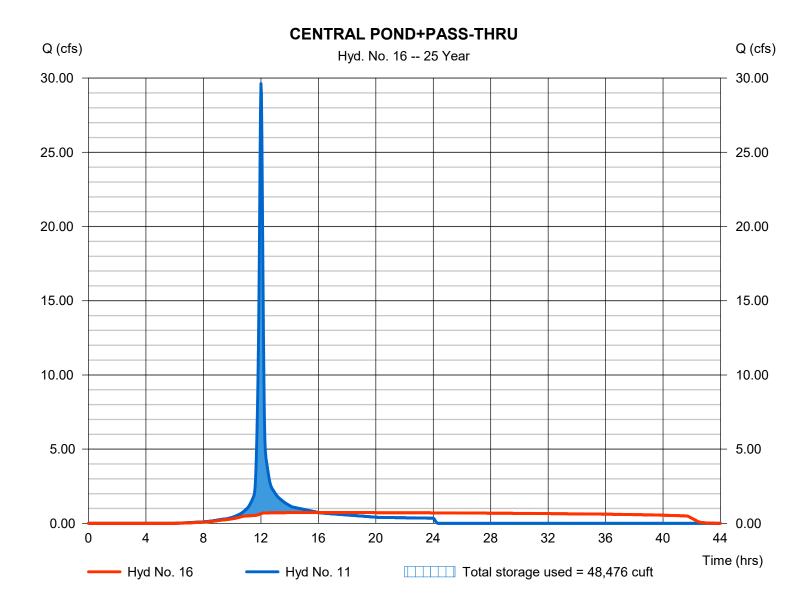
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Monday, 09 / 27 / 2021

Hyd. No. 16

CENTRAL POND+PASS-THRU

Hydrograph type Peak discharge = 0.722 cfs= Reservoir Storm frequency = 25 yrsTime to peak $= 16.03 \, hrs$ Time interval = 2 min Hyd. volume = 77,481 cuft Inflow hyd. No. = 11 - CENTRAL DA + PASS-THARAUX. Elevation = 952.13 ft= CENTRAL POND Reservoir name Max. Storage = 48,476 cuft



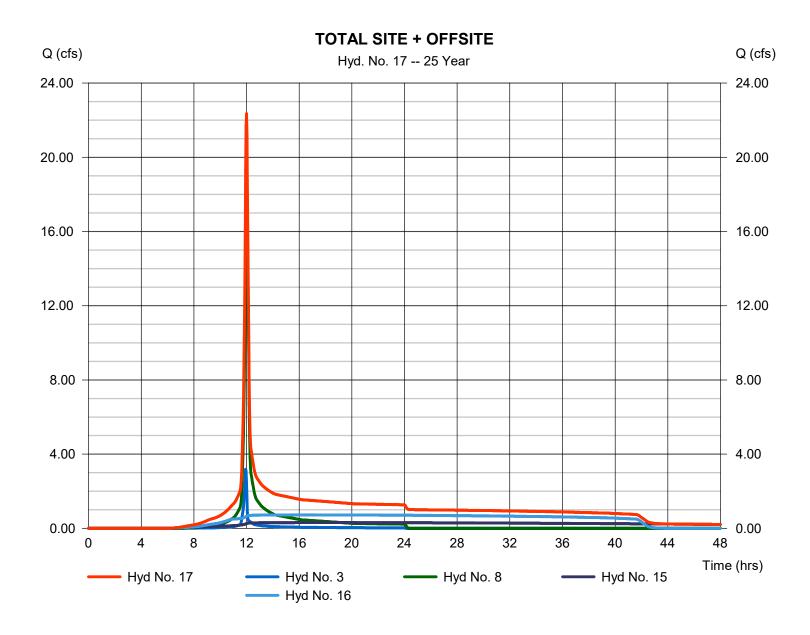
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Monday, 09 / 27 / 2021

Hyd. No. 17

TOTAL SITE + OFFSITE

Hydrograph type = Combine Peak discharge = 22.36 cfsStorm frequency Time to peak = 25 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 177,263 cuft Inflow hyds. = 3, 8, 15, 16 Contrib. drain. area = 4.680 ac



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Monday, 09 / 27 / 2021

Hyd. No. 1

EX DA

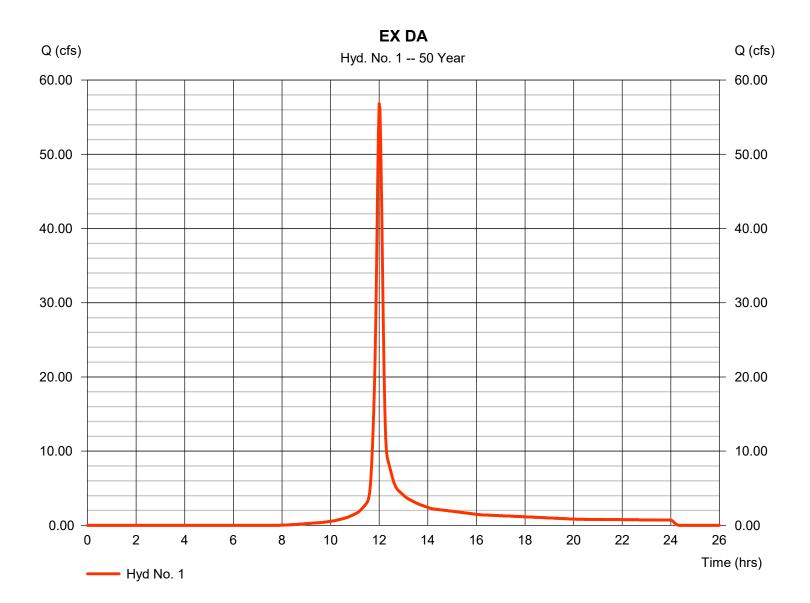
Hydrograph type = SCS Runoff Peak discharge = 56.83 cfsStorm frequency = 50 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 147,336 cuft Drainage area = 11.560 ac Curve number = 74

Basin Slope = 0.0 % Curve number = 74

Hydraulic length = 0 ft

To method = User Time of conc. (Tc) = 12.6

Tc method = User Time of conc. (Tc) = 12.60 min
Total precip. = 6.26 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



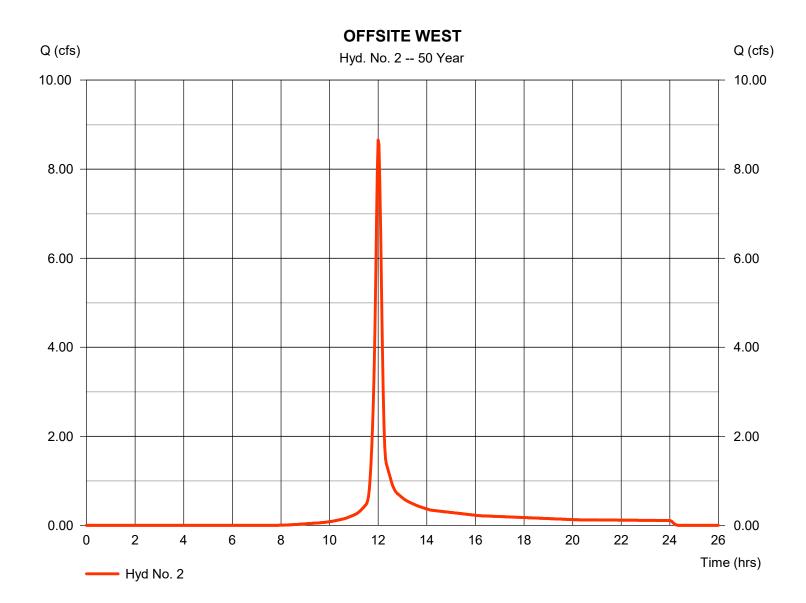
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Monday, 09 / 27 / 2021

Hyd. No. 2

OFFSITE WEST

= SCS Runoff Hydrograph type Peak discharge = 8.652 cfsStorm frequency = 50 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 22,432 cuft Drainage area = 1.760 acCurve number = 74 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) = 10.10 min = User Total precip. = 6.26 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



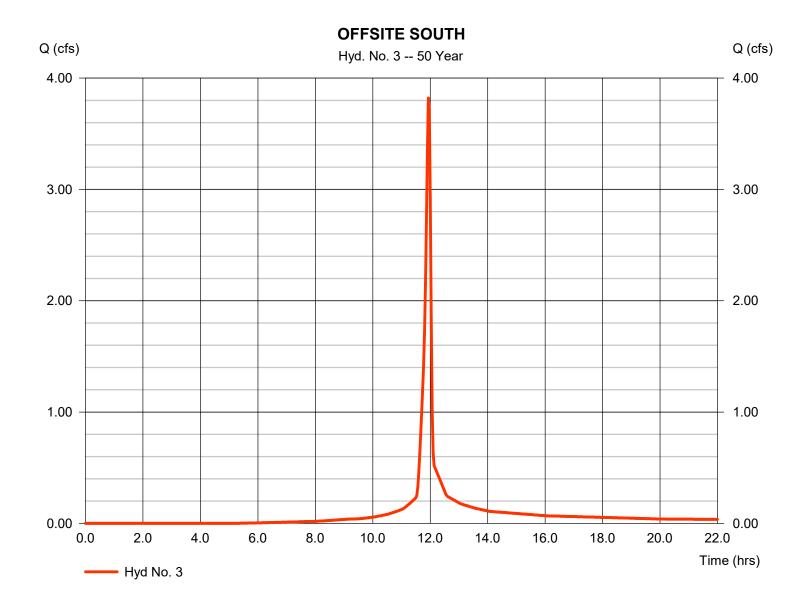
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Monday, 09 / 27 / 2021

Hyd. No. 3

OFFSITE SOUTH

= SCS Runoff Hydrograph type Peak discharge = 3.821 cfsStorm frequency = 50 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 7,963 cuft Drainage area = 0.540 acCurve number = 83 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 6.26 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



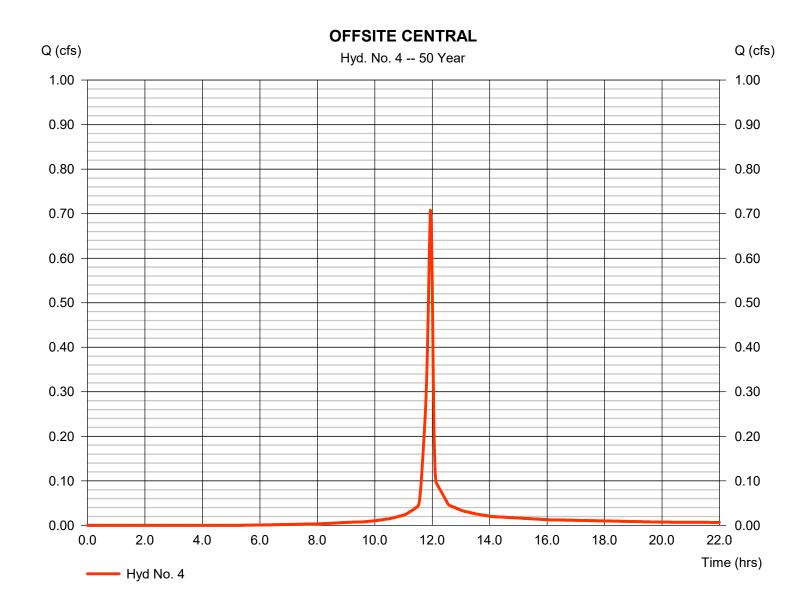
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Monday, 09 / 27 / 2021

Hyd. No. 4

OFFSITE CENTRAL

Hydrograph type = SCS Runoff Peak discharge = 0.708 cfsStorm frequency = 50 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 1,475 cuftDrainage area Curve number = 0.100 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 6.26 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



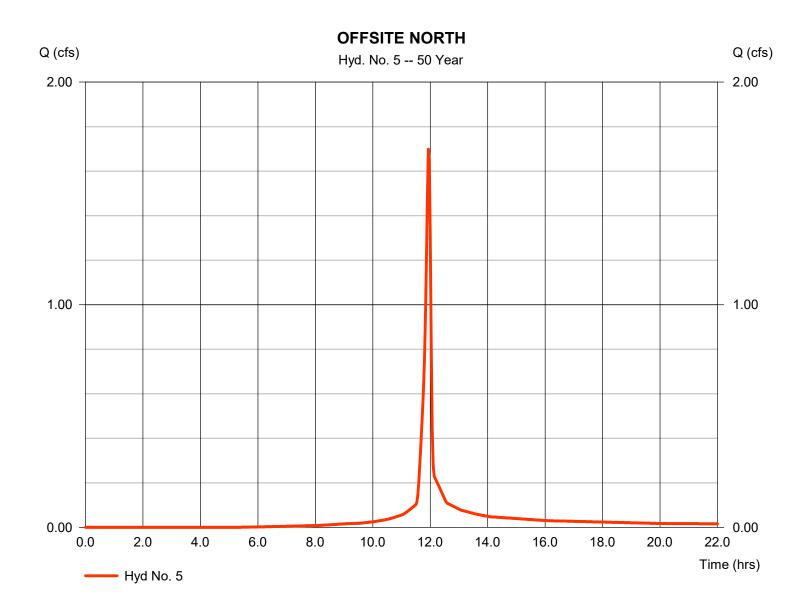
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Monday, 09 / 27 / 2021

Hyd. No. 5

OFFSITE NORTH

= SCS Runoff Hydrograph type Peak discharge = 1.698 cfsStorm frequency = 50 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 3,539 cuftDrainage area = 0.240 acCurve number = 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 6.26 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



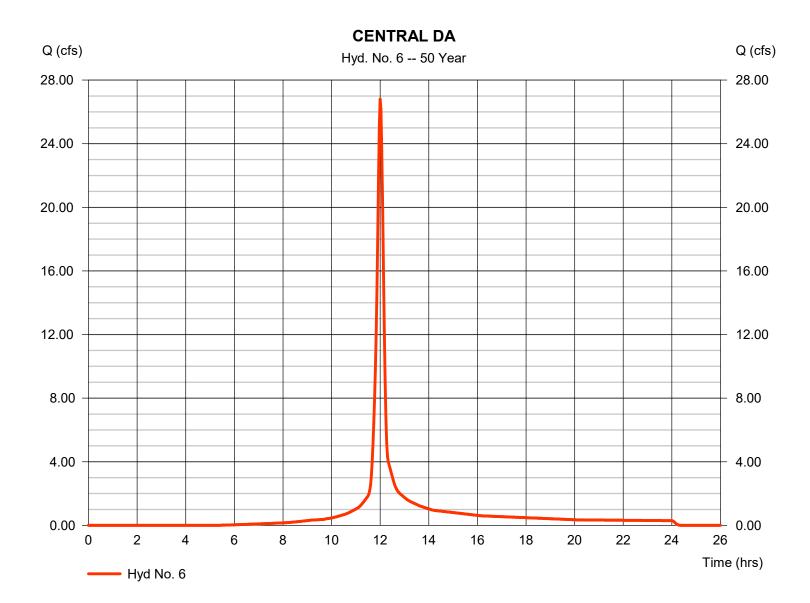
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Monday, 09 / 27 / 2021

Hyd. No. 6

CENTRAL DA

Hydrograph type = SCS Runoff Peak discharge = 26.80 cfsStorm frequency = 50 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 70,725 cuftDrainage area = 4.360 acCurve number = 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 6.26 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



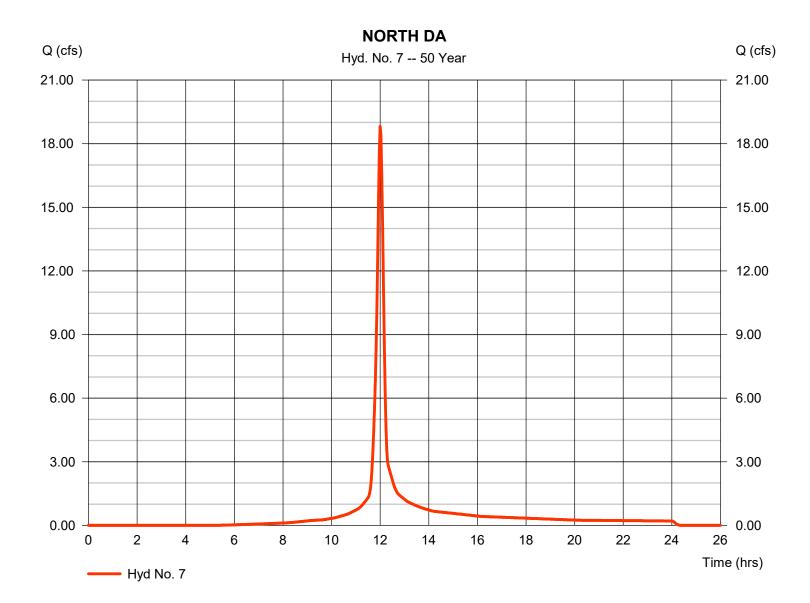
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Monday, 09 / 27 / 2021

Hyd. No. 7

NORTH DA

Hydrograph type = SCS Runoff Peak discharge = 18.81 cfsStorm frequency = 50 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 49,637 cuftDrainage area = 3.060 acCurve number = 83 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 6.26 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

= 24 hrs

Monday, 09 / 27 / 2021

= 484

Hyd. No. 8

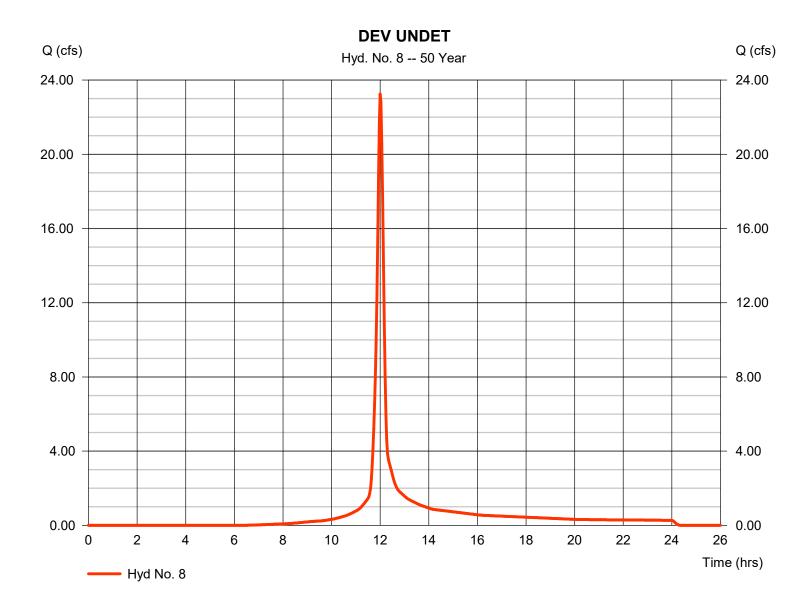
DEV UNDET

Storm duration

Hydrograph type = SCS Runoff Peak discharge = 23.25 cfsStorm frequency = 50 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 60.638 cuft Drainage area = 4.140 acCurve number = 79* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 6.26 inDistribution = Type II

Shape factor

^{*} Composite (Area/CN) = [(2.460 x 79) + (1.680 x 80)] / 4.140



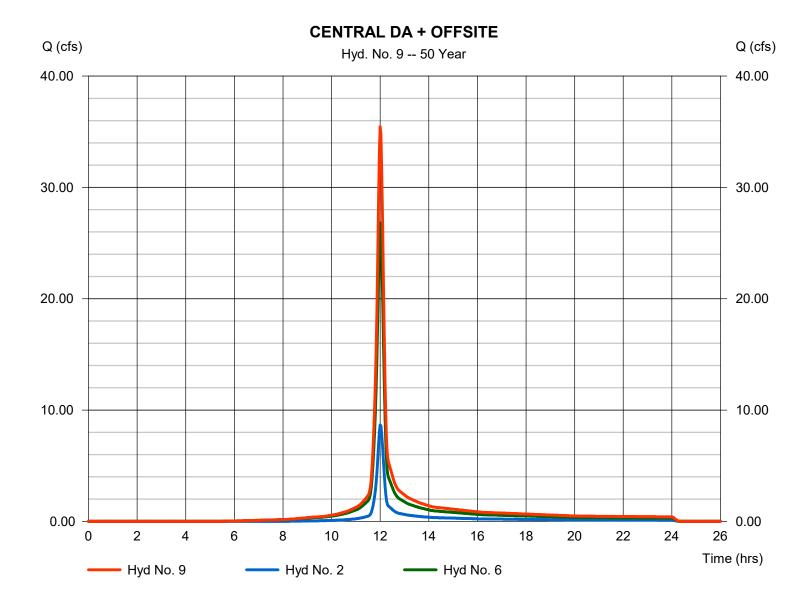
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Hyd. No. 9

CENTRAL DA + OFFSITE

Hydrograph type = Combine Peak discharge = 35.46 cfsStorm frequency = 50 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 93,157 cuft Inflow hyds. = 2,6 Contrib. drain. area = 6.120 ac



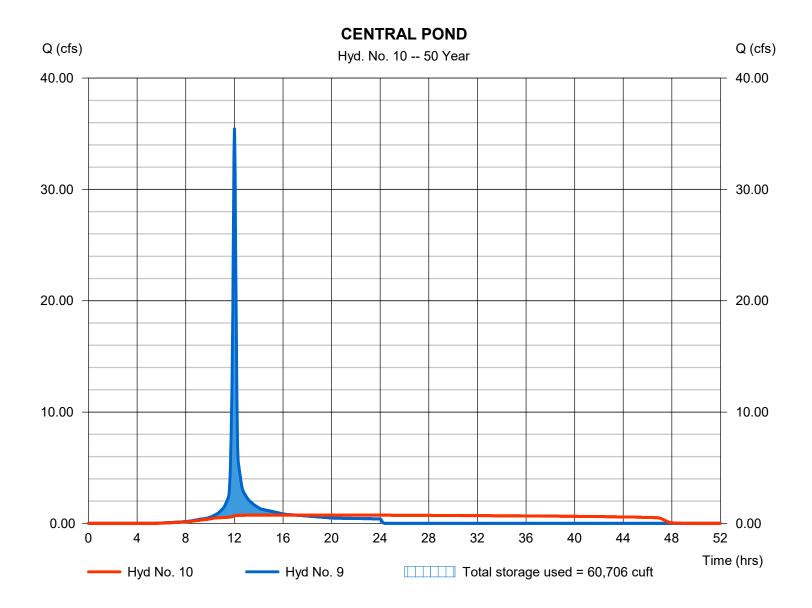
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Monday, 09 / 27 / 2021

Hyd. No. 10

CENTRAL POND

Hydrograph type = Reservoir Peak discharge = 0.740 cfsStorm frequency = 50 yrsTime to peak $= 17.03 \, hrs$ Time interval = 2 min Hyd. volume = 93,156 cuft Inflow hyd. No. = 9 - CENTRAL DA + OFFSITE Max. Elevation = 952.93 ft= CENTRAL POND Reservoir name Max. Storage = 60,706 cuft



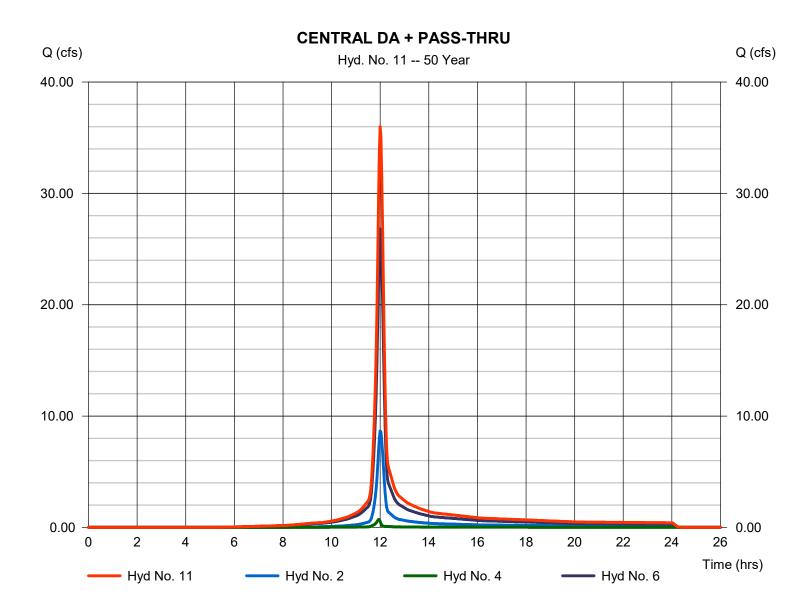
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Monday, 09 / 27 / 2021

Hyd. No. 11

CENTRAL DA + PASS-THRU

Hydrograph type = Combine Peak discharge = 36.00 cfsStorm frequency Time to peak = 50 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 94,632 cuft Inflow hyds. = 2, 4, 6Contrib. drain. area = 6.220 ac



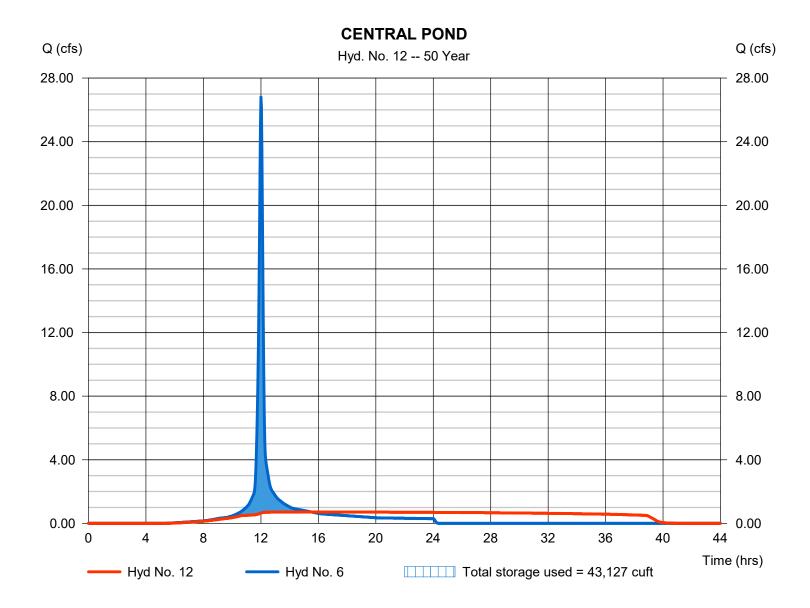
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Hyd. No. 12

CENTRAL POND

Hydrograph type Peak discharge = 0.712 cfs= Reservoir Storm frequency = 50 yrsTime to peak $= 15.53 \, hrs$ Time interval = 2 min Hyd. volume = 70,724 cuftInflow hyd. No. Max. Elevation = 6 - CENTRAL DA = 951.68 ft= CENTRAL POND Reservoir name Max. Storage = 43,127 cuft



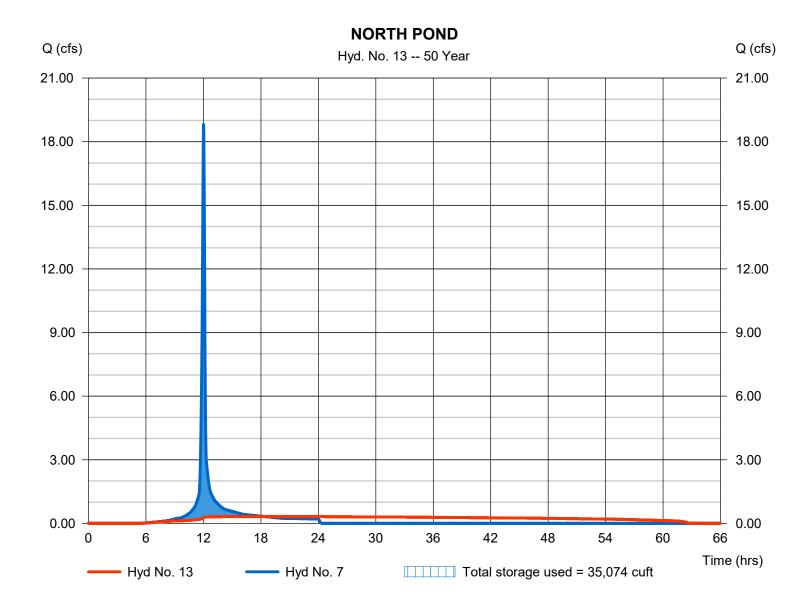
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Monday, 09 / 27 / 2021

Hyd. No. 13

NORTH POND

Hydrograph type = Reservoir Peak discharge = 0.320 cfsStorm frequency = 50 yrsTime to peak $= 18.40 \, hrs$ Time interval = 2 min Hyd. volume = 49,636 cuft Inflow hyd. No. = 7 - NORTH DA Max. Elevation $= 943.69 \, \text{ft}$ = NORTH POND Reservoir name Max. Storage = 35,074 cuft



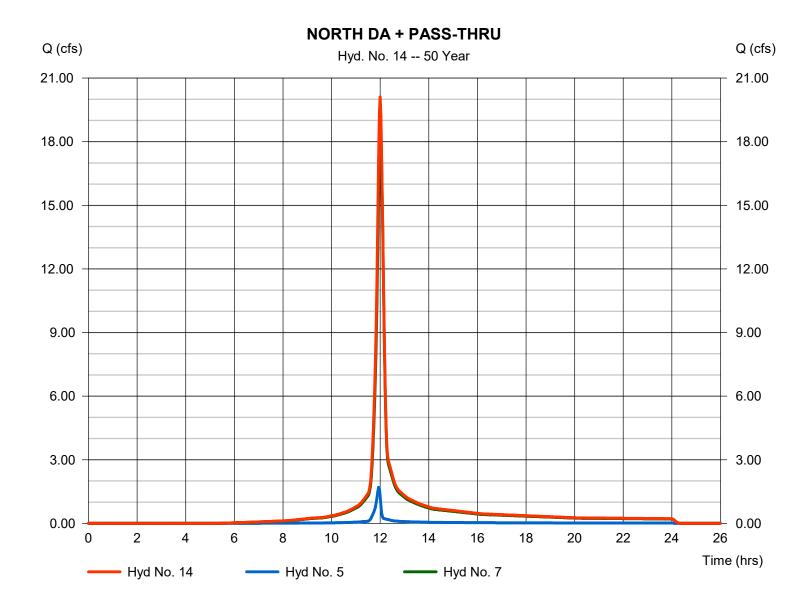
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Monday, 09 / 27 / 2021

Hyd. No. 14

NORTH DA + PASS-THRU

Hydrograph type = Combine Peak discharge = 20.11 cfsStorm frequency Time to peak = 50 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 53,177 cuft Inflow hyds. = 5, 7 Contrib. drain. area = 3.300 ac



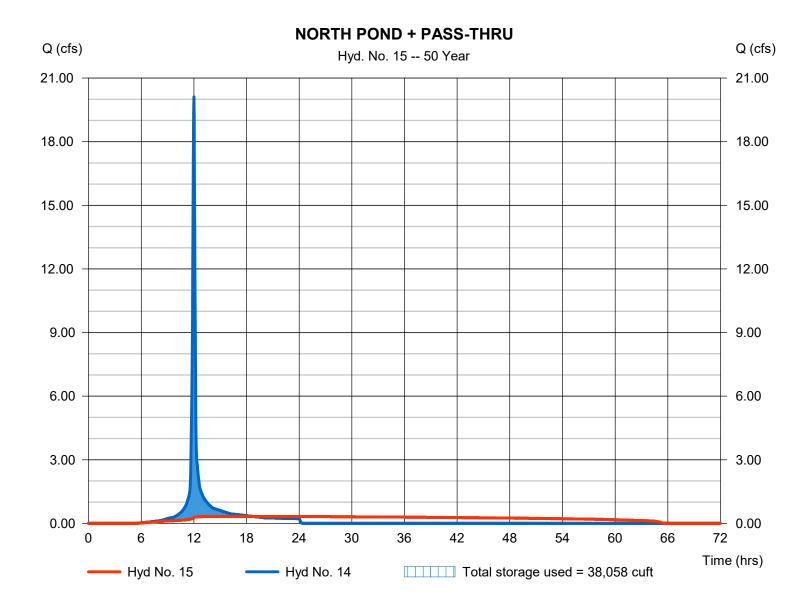
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Monday, 09 / 27 / 2021

Hyd. No. 15

NORTH POND + PASS-THRU

Hydrograph type Peak discharge = 0.326 cfs= Reservoir Storm frequency = 50 yrsTime to peak $= 18.73 \, hrs$ Time interval = 2 min Hyd. volume = 53,175 cuftInflow hyd. No. = 14 - NORTH DA + PASS-THR Max. Elevation $= 944.05 \, \text{ft}$ = NORTH POND Reservoir name Max. Storage = 38,058 cuft



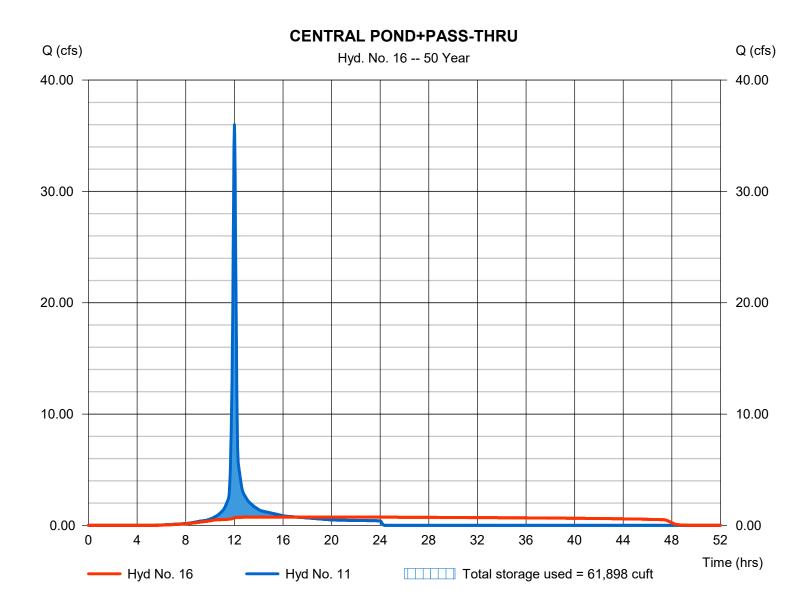
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Monday, 09 / 27 / 2021

Hyd. No. 16

CENTRAL POND+PASS-THRU

Hydrograph type Peak discharge = 0.742 cfs= Reservoir Storm frequency = 50 yrsTime to peak $= 17.13 \, hrs$ Time interval = 2 min Hyd. volume = 94,630 cuftInflow hyd. No. = 11 - CENTRAL DA + PASS-THARAUX. Elevation $= 953.01 \, \text{ft}$ = CENTRAL POND Reservoir name Max. Storage = 61,898 cuft



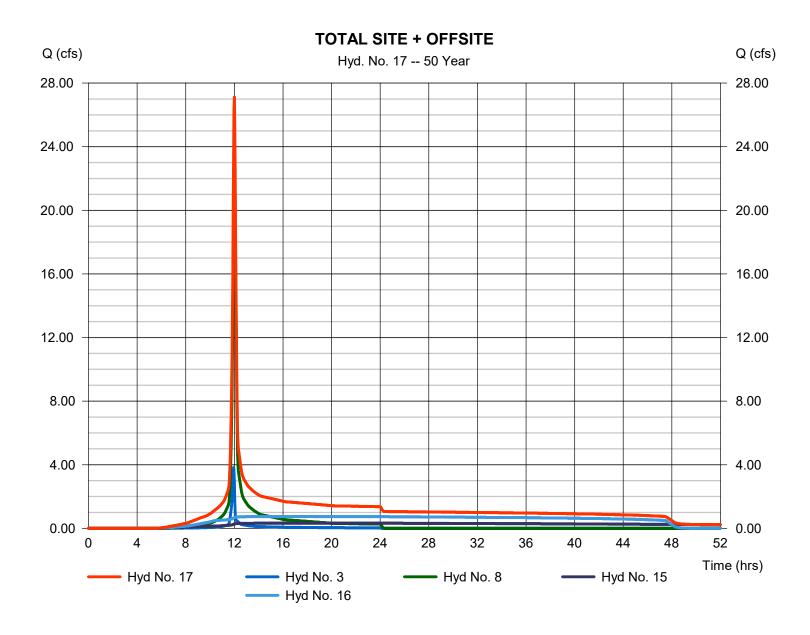
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Monday, 09 / 27 / 2021

Hyd. No. 17

TOTAL SITE + OFFSITE

Hydrograph type = Combine Peak discharge = 27.12 cfsStorm frequency Time to peak = 50 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 216,407 cuft Inflow hyds. Contrib. drain. area = 4.680 ac= 3, 8, 15, 16



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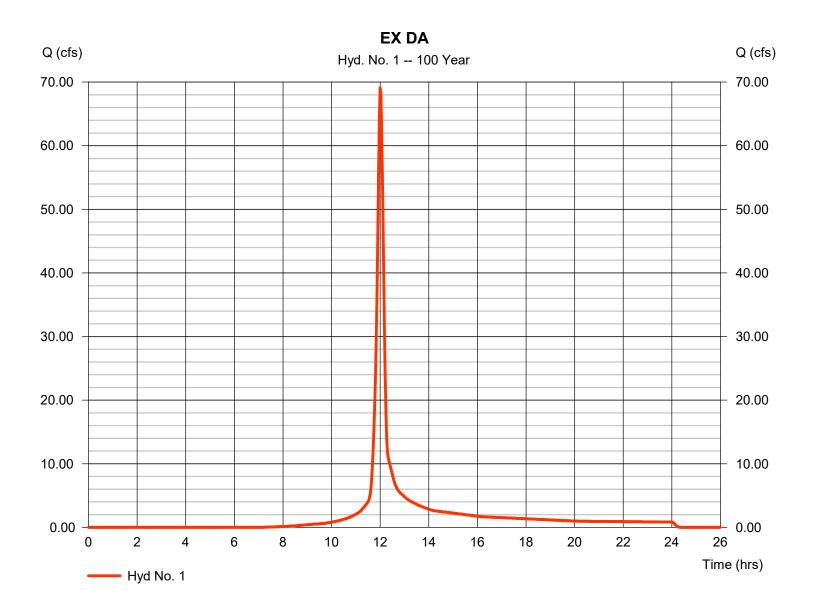
Hyd. No. 1

EX DA

Hydrograph type = SCS Runoff Peak discharge = 69.10 cfsStorm frequency = 100 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 179,452 cuft Drainage area = 11.560 ac Curve number = 74

Basin Slope = 0.0 % Hydraulic length = 0 ft
Tc method = User Time of conc. (Tc) = 12.60 min

Total precip. = 7.12 in Distribution = Type II Storm duration = 24 hrs Shape factor = 484



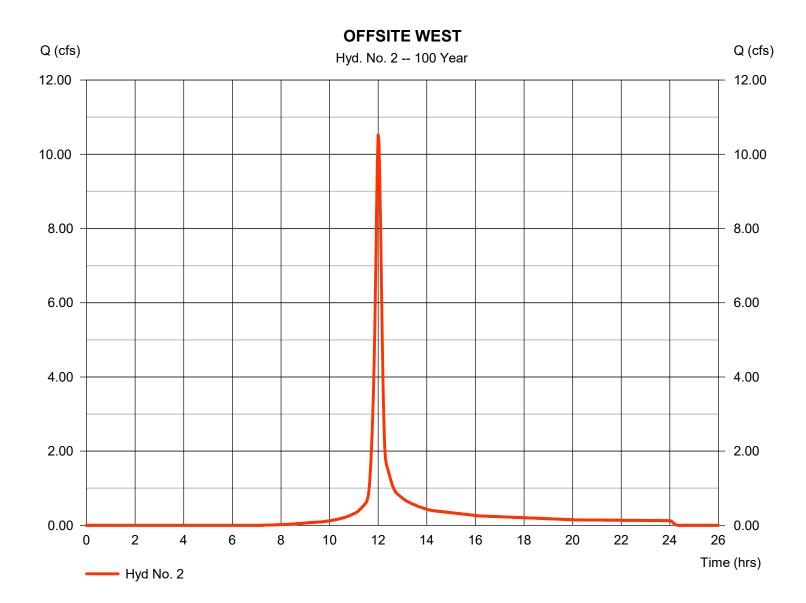
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Monday, 09 / 27 / 2021

Hyd. No. 2

OFFSITE WEST

Hydrograph type = SCS Runoff Peak discharge = 10.52 cfsStorm frequency = 100 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 27,321 cuftDrainage area = 1.760 acCurve number = 74 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 10.10 min = User Total precip. = 7.12 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



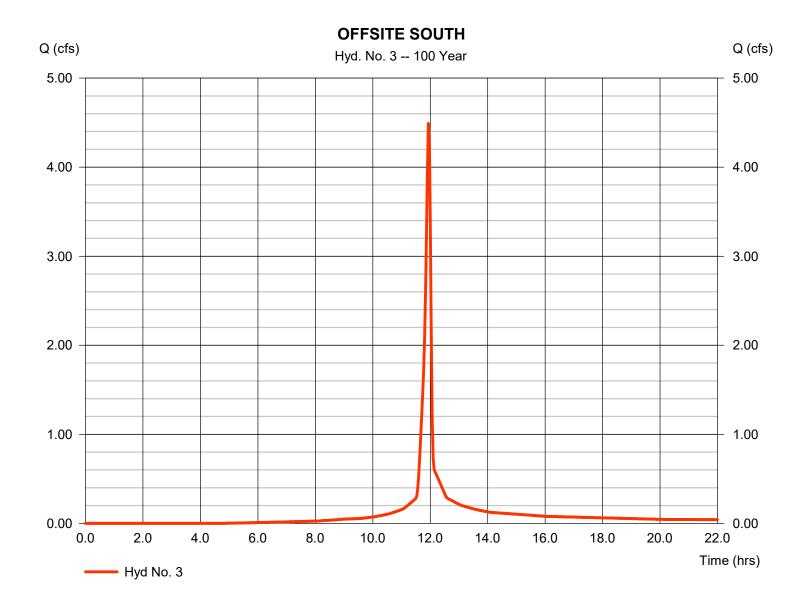
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Monday, 09 / 27 / 2021

Hyd. No. 3

OFFSITE SOUTH

Hydrograph type = SCS Runoff Peak discharge = 4.491 cfsStorm frequency = 100 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 9.448 cuft Drainage area Curve number = 83 = 0.540 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 7.12 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



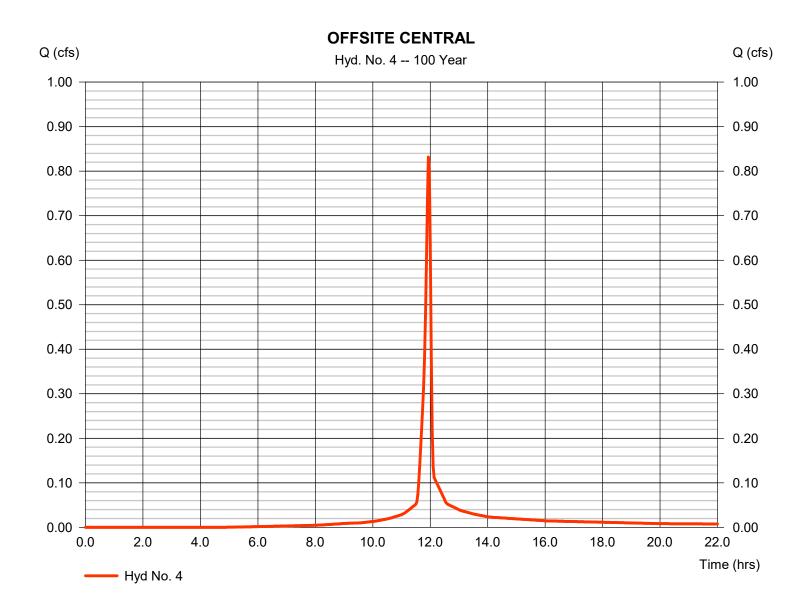
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Monday, 09 / 27 / 2021

Hyd. No. 4

OFFSITE CENTRAL

Hydrograph type = SCS Runoff Peak discharge = 0.832 cfsStorm frequency = 100 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 1,750 cuftDrainage area Curve number = 0.100 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 7.12 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



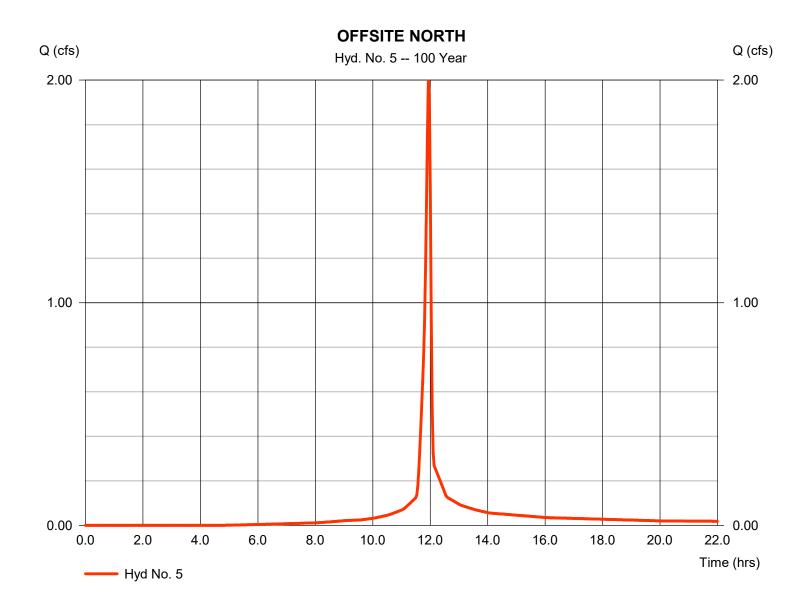
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Monday, 09 / 27 / 2021

Hyd. No. 5

OFFSITE NORTH

= SCS Runoff Hydrograph type Peak discharge = 1.996 cfsStorm frequency = 100 yrsTime to peak $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 4,199 cuftDrainage area = 0.240 acCurve number = 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 7.12 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



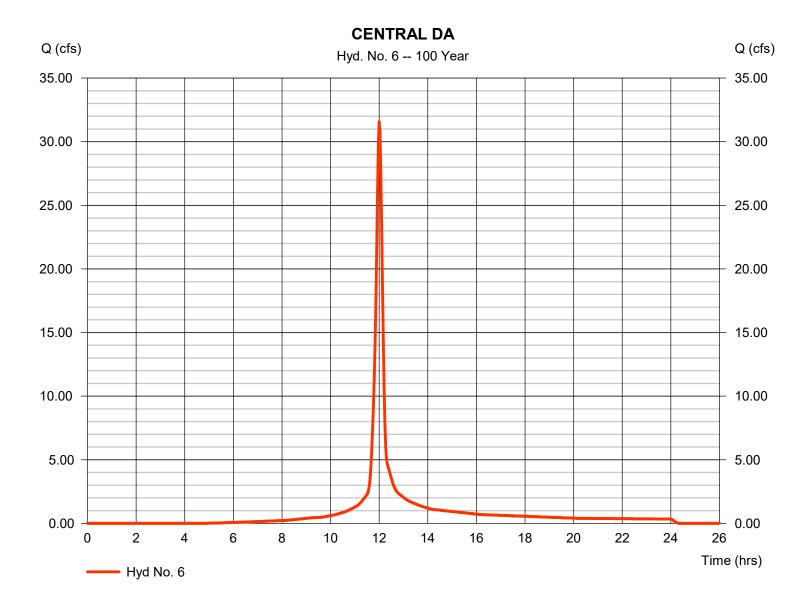
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Monday, 09 / 27 / 2021

Hyd. No. 6

CENTRAL DA

Hydrograph type = SCS Runoff Peak discharge = 31.57 cfsStorm frequency = 100 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 83,911 cuft Drainage area = 4.360 acCurve number = 83 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 7.12 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



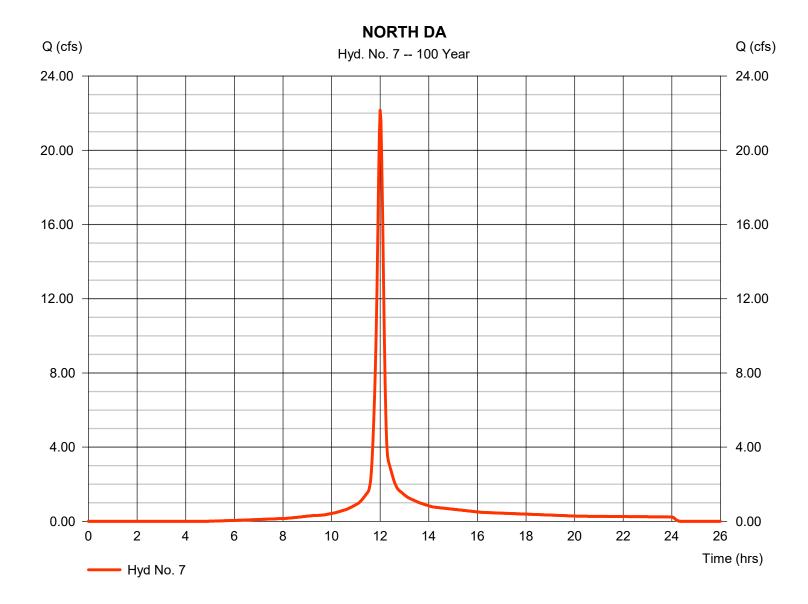
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Monday, 09 / 27 / 2021

Hyd. No. 7

NORTH DA

Hydrograph type = SCS Runoff Peak discharge = 22.16 cfsStorm frequency = 100 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 58,891 cuftDrainage area Curve number = 3.060 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 7.12 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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Monday, 09 / 27 / 2021

Hyd. No. 8

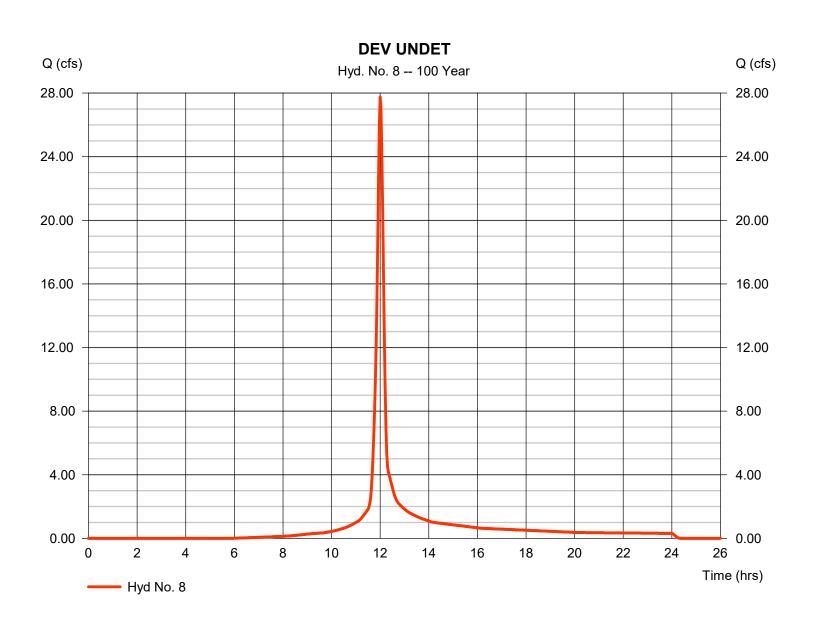
DEV UNDET

Hydrograph type = SCS Runoff Peak discharge = 27.75 cfsStorm frequency = 100 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 72,752 cuft = 4.140 acCurve number Drainage area = 79* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.00 min = User

Total precip. = 7.12 in Distribution = Type II

Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(2.460 x 79) + (1.680 x 80)] / 4.140



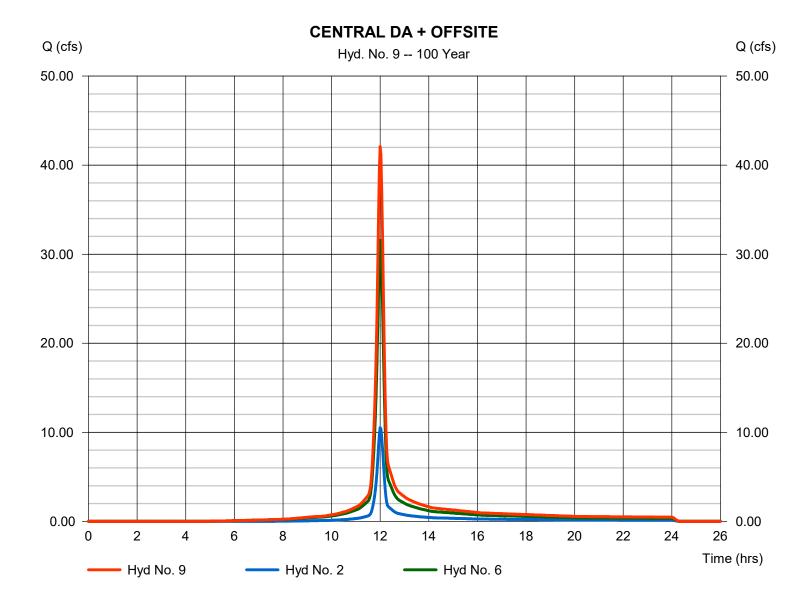
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Hyd. No. 9

CENTRAL DA + OFFSITE

Hydrograph type = Combine Peak discharge = 42.09 cfsStorm frequency Time to peak = 100 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 111,232 cuft Inflow hyds. = 2,6 Contrib. drain. area = 6.120 ac



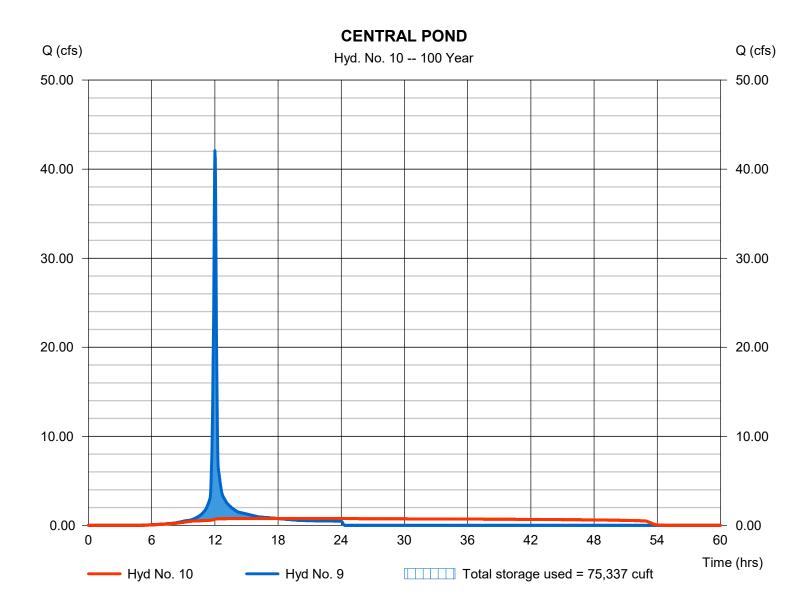
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Monday, 09 / 27 / 2021

Hyd. No. 10

CENTRAL POND

= Reservoir Hydrograph type Peak discharge = 0.761 cfsStorm frequency = 100 yrsTime to peak $= 18.00 \, hrs$ Time interval = 2 min Hyd. volume = 111,230 cuft Inflow hyd. No. = 9 - CENTRAL DA + OFFSITE Max. Elevation = 953.88 ft = 75,337 cuft Reservoir name = CENTRAL POND Max. Storage



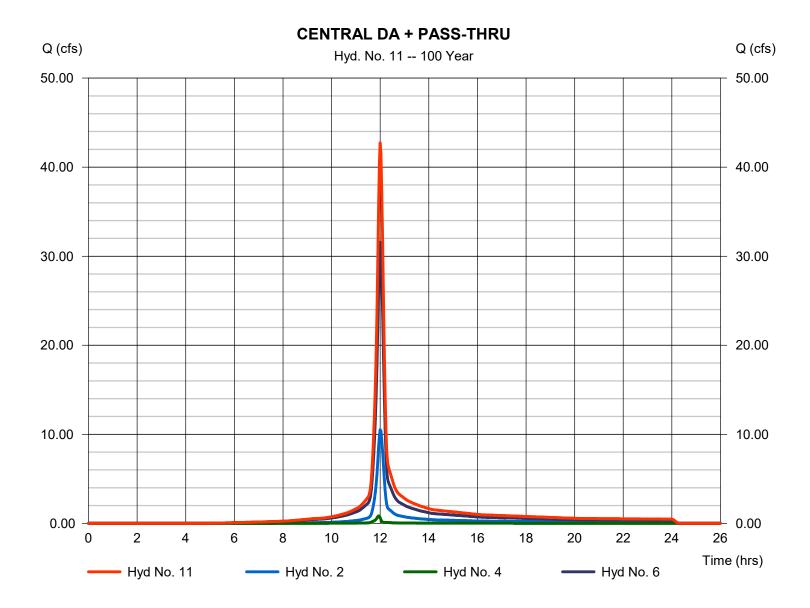
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

Hyd. No. 11

CENTRAL DA + PASS-THRU

= 42.73 cfsHydrograph type = Combine Peak discharge Storm frequency Time to peak = 100 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 112,981 cuft Inflow hyds. = 2, 4, 6= 6.220 ac Contrib. drain. area



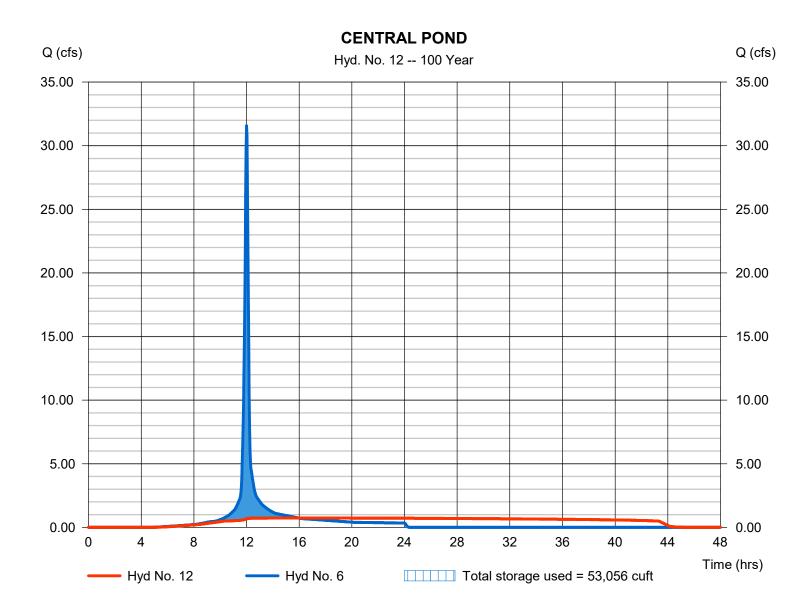
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Monday, 09 / 27 / 2021

Hyd. No. 12

CENTRAL POND

Hydrograph type = Reservoir Peak discharge = 0.729 cfsStorm frequency = 100 yrsTime to peak $= 15.97 \, hrs$ Time interval = 2 min Hyd. volume = 83,909 cuft Inflow hyd. No. Max. Elevation = 6 - CENTRAL DA = 952.43 ft= CENTRAL POND Reservoir name Max. Storage = 53,056 cuft



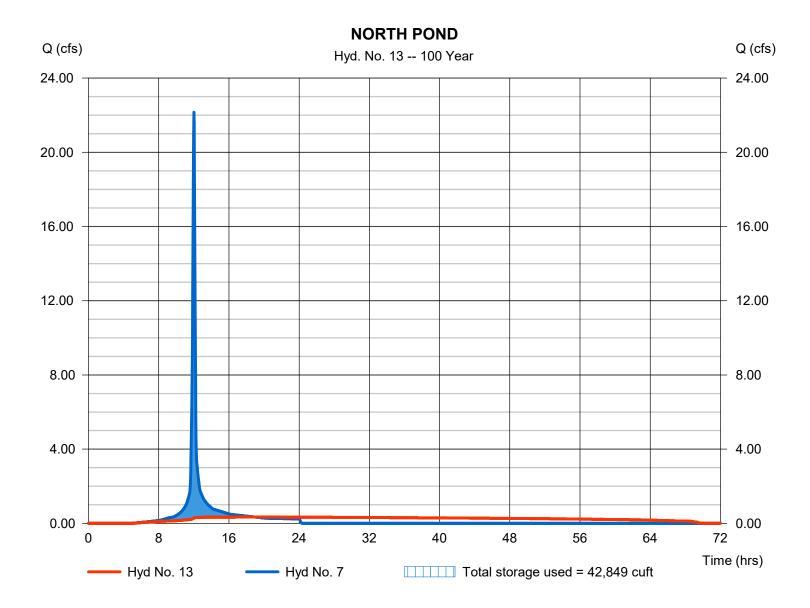
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Monday, 09 / 27 / 2021

Hyd. No. 13

NORTH POND

Hydrograph type Peak discharge = 0.334 cfs= Reservoir Storm frequency = 100 yrsTime to peak $= 19.07 \, hrs$ Time interval = 2 min Hyd. volume = 58,890 cuftInflow hyd. No. Max. Elevation = 7 - NORTH DA $= 944.50 \, \text{ft}$ Reservoir name = NORTH POND Max. Storage = 42,849 cuft



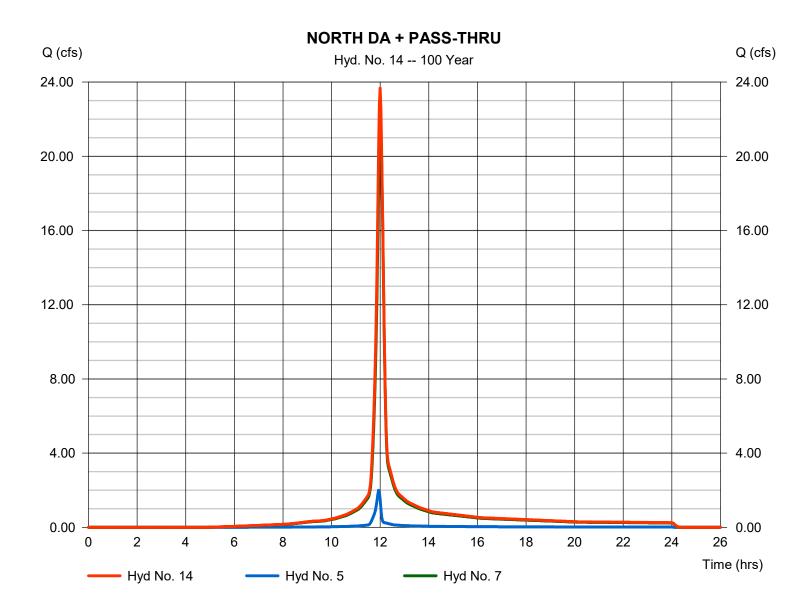
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Monday, 09 / 27 / 2021

Hyd. No. 14

NORTH DA + PASS-THRU

Hydrograph type = Combine Peak discharge = 23.68 cfsStorm frequency Time to peak = 100 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 63,090 cuftInflow hyds. = 3.300 ac= 5, 7 Contrib. drain. area



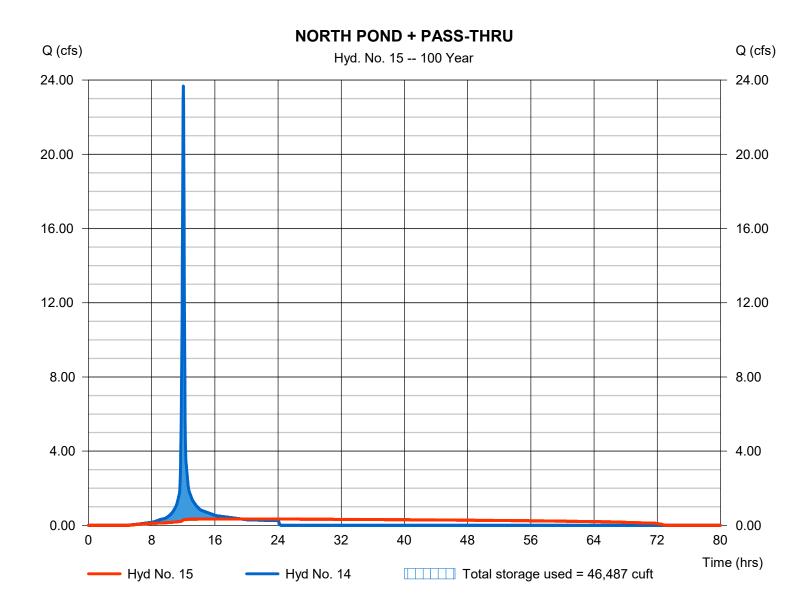
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Monday, 09 / 27 / 2021

Hyd. No. 15

NORTH POND + PASS-THRU

Hydrograph type Peak discharge = 0.341 cfs= Reservoir Storm frequency = 100 yrsTime to peak $= 19.37 \, hrs$ Time interval = 2 min Hyd. volume = 63,089 cuftInflow hyd. No. = 14 - NORTH DA + PASS-THR Max. Elevation = 944.85 ft= NORTH POND Reservoir name Max. Storage = 46,487 cuft



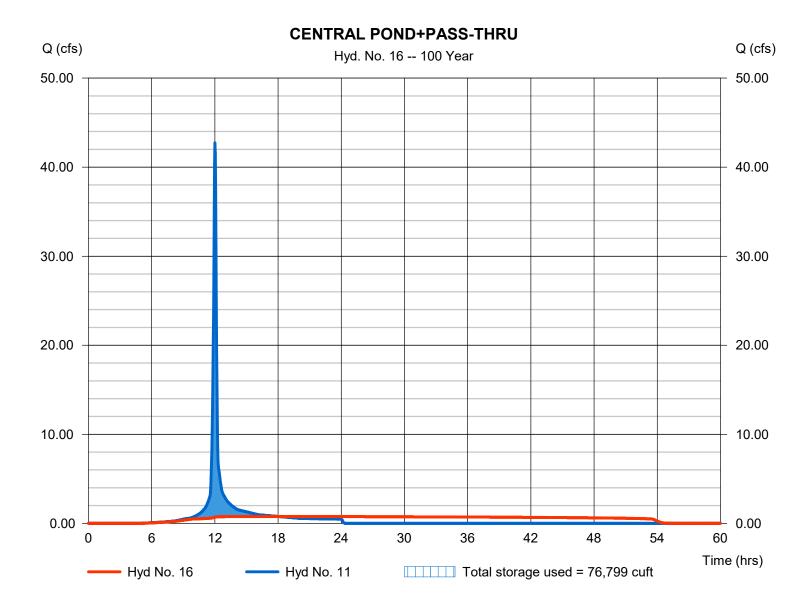
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Monday, 09 / 27 / 2021

Hyd. No. 16

CENTRAL POND+PASS-THRU

Hydrograph type Peak discharge = 0.763 cfs= Reservoir Storm frequency = 100 yrsTime to peak $= 18.10 \, hrs$ Time interval = 2 min Hyd. volume = 112,980 cuftInflow hyd. No. = 11 - CENTRAL DA + PASS-THARAUX. Elevation = 953.98 ft= CENTRAL POND = 76,799 cuft Reservoir name Max. Storage



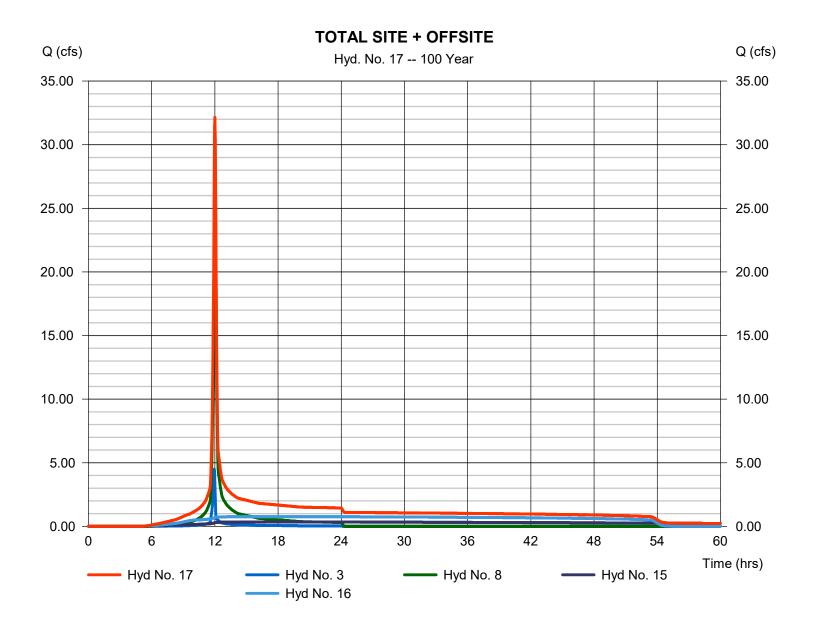
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Monday, 09 / 27 / 2021

Hyd. No. 17

TOTAL SITE + OFFSITE

Hydrograph type = Combine Peak discharge = 32.15 cfsStorm frequency Time to peak = 100 yrs $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 258,269 cuft Inflow hyds. Contrib. drain. area = 3, 8, 15, 16 = 4.680 ac



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

Monday, 09 / 27 / 2021

| Return Period | Intensity-Duration-Frequency Equation Coefficients (FHA) | | | | | | | |
|------------------|--|---------|--------|-------|--|--|--|--|
| (Yrs) | В | D | E | (N/A) | | | | |
| 1 | 66.7390 | 18.4000 | 0.9371 | | | | | |
| 2 | 101.8674 | 20.8000 | 0.9811 | | | | | |
| 3 | 0.0000 | 0.0000 | 0.0000 | | | | | |
| 5 | 124.8469 | 20.4000 | 0.9780 | | | | | |
| 10 | 145.4638 | 20.8000 | 0.9749 | | | | | |
| 25 | 181.9707 | 20.8000 | 0.9836 | | | | | |
| 50 | 201.7299 | 20.9000 | 0.9769 | | | | | |
| 100 | 239.1196 | 21.3001 | 0.9873 | | | | | |

File name: WDM-Figure3-5.IDF

Intensity = B / (Tc + D)^E

| Return | Intensity Values (in/hr) | | | | | | | | | | | |
|-----------------|--------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Period (Yrs) | 5 min | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 |
| 1 | 3.48 | 2.90 | 2.49 | 2.19 | 1.95 | 1.76 | 1.61 | 1.48 | 1.37 | 1.27 | 1.19 | 1.12 |
| 2 | 4.20 | 3.53 | 3.04 | 2.68 | 2.39 | 2.16 | 1.97 | 1.81 | 1.68 | 1.56 | 1.46 | 1.37 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5 | 5.28 | 4.43 | 3.81 | 3.35 | 2.99 | 2.70 | 2.46 | 2.26 | 2.09 | 1.95 | 1.82 | 1.71 |
| 10 | 6.12 | 5.15 | 4.44 | 3.91 | 3.50 | 3.16 | 2.88 | 2.65 | 2.46 | 2.29 | 2.14 | 2.01 |
| 25 | 7.44 | 6.25 | 5.39 | 4.74 | 4.23 | 3.82 | 3.48 | 3.20 | 2.96 | 2.76 | 2.58 | 2.42 |
| 50 | 8.40 | 7.07 | 6.10 | 5.37 | 4.80 | 4.34 | 3.96 | 3.64 | 3.37 | 3.14 | 2.94 | 2.76 |
| 100 | 9.48 | 7.98 | 6.89 | 6.07 | 5.42 | 4.90 | 4.47 | 4.11 | 3.80 | 3.54 | 3.31 | 3.11 |

Tc = time in minutes. Values may exceed 60.

 $\label{lem:precip_file} \begin{tabular}{ll} Precip_file name: Q:\A-FILES\A-1800\A1846\Docs\Stormwater\ Management\ Plan\Hydroflow\WDM-Figure 3-5.PCP \end{tabular}$

| | Rainfall Precipitation Table (in) | | | | | | | | |
|-----------------------|-----------------------------------|------|------|------|-------|-------|-------|--------|--|
| Storm Distribution | 1-yr | 2-yr | 3-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | |
| SCS 24-hour | 2.67 | 3.08 | 0.00 | 3.81 | 4.46 | 5.44 | 6.26 | 7.12 | |
| SCS 6-Hr | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Huff-1st | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Huff-2nd | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Huff-3rd | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Huff-4th | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Huff-Indy | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Custom | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

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